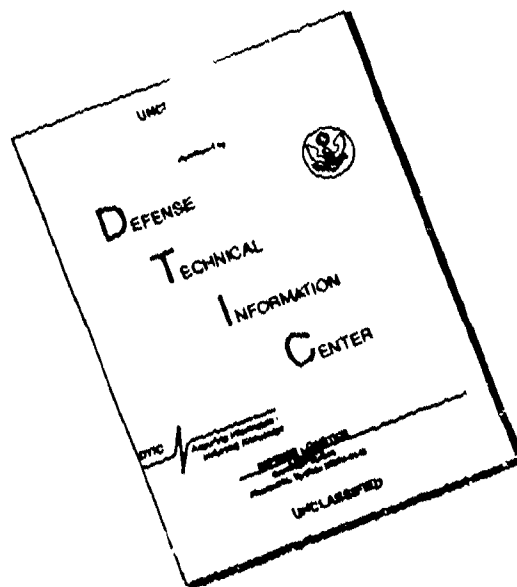


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TECHNICAL REPORT BRL-TR-2829

IBHVG2 -- A USER'S GUIDE

RONALD D. ANDERSON
KURT D. FICKIE

JULY 1987



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Errata Sheet for BRL-TR-2829, "IBHVG2 -- A USER'S GUIDE"

Page	Description
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41	After equation (A.14), reference to 'Figure 6' should be 'Figure 7'
----	---

43	Section C, first paragraph, last sentence: "...tube-based frame of reference (Figure 6), where $z_p \approx x_p + x_r$, is as follows."
----	--

49	Equation (D.18) should be:
----	----------------------------

$$A_w = \left[\frac{V_c}{A_b} \right] \pi D_b + 2A_b + \pi D_b [z_p - z_p(0)]$$

Equation (D.21) should be:

$$\bar{v} = \frac{\dot{z}_p}{2}$$

50	Section E, third paragraph, second sentence: "These codes solve for surface area and unburned volume for the different grain types..."
----	--

55	Subscript definitions, last line should have " 0 " (zero) instead of " ϕ " (phi)
----	---

58	Graph at bottom of page should have following axis labels: <div style="display: flex; justify-content: space-between; margin-left: 100px;"> <div>Horizontal axis</div> <div>"Depth Burned (in)"</div> </div> <div style="display: flex; justify-content: space-between; margin-left: 100px;"> <div>Vertical axis</div> <div>"Surface Area (in²)"</div> </div>
----	---

61	Appendix D, first paragraph, end of third sentence: "...integration step size (DELT in the \$INFO deck)."
----	---

62	Appendix E, third paragraph, second sentence: "...case 5 took more time to compute on the Cray and the PC than..."
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73	Test Case 2, second paragraph, end of fourth sentence: "...\$TRAJ, and \$INFO decks, and the graph at the end of Appendix B.)"
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SECURITY CLASSIFICATION OF THIS PAGE

REPORT DOCUMENTATION PAGE				Form Approved OMB No 0704-0188 Exp. Date Jun 30, 1986	
1a. REPORT SECURITY CLASSIFICATION Unclassified			1b. RESTRICTIVE MARKINGS		
2a. SECURITY CLASSIFICATION AUTHORITY			3. DISTRIBUTION/AVAILABILITY OF REPORT		
2b. DECLASSIFICATION/DOWNGRADING SCHEDULE					
4. PERFORMING ORGANIZATION REPORT NUMBER(S) BRL-TR-2829			5. MONITORING ORGANIZATION REPORT NUMBER(S)		
6a. NAME OF PERFORMING ORGANIZATION Ballistic Research Laboratory		6b. OFFICE SYMBOL (If applicable) SLCBR-IB-A	7a. NAME OF MONITORING ORGANIZATION		
6c. ADDRESS (City, State, and ZIP Code) Aberdeen Proving Ground, MD 21005-5066			7b. ADDRESS (City, State, and ZIP Code)		
8a. NAME OF FUNDING/SPONSORING ORGANIZATION		8b. OFFICE SYMBOL (If applicable)	9. PROCUREMENT INSTRUMENT IDENTIFICATION NUMBER		
8c. ADDRESS (City, State, and ZIP Code)			10. SOURCE OF FUNDING NUMBERS		
			PROGRAM ELEMENT NO. 61102A	PROJECT NO. 1L161102A	TASK NO. 43 00
					WORK UNIT ACCESSION NO. 00
11. TITLE (Include Security Classification) IBHVG2 -- A User's Guide					
12. PERSONAL AUTHOR(S) Ronald D. Anderson and Kurt D. Fickie					
13a. TYPE OF REPORT Technical Report		13b. TIME COVERED FROM Jan 83 TO Jan 87		14. DATE OF REPORT (Year, Month, Day)	
15. PAGE COUNT					
16. SUPPLEMENTARY NOTATION					
17. COSATI CODES			18. SUBJECT TERMS (Continue on reverse if necessary and identify by block number)		
FIELD	GROUP	SUB-GROUP			
19	01				
21	02		Interior Ballistics, Guns, High Velocity, Propellants		
19. ABSTRACT (Continue on reverse if necessary and identify by block number) IBHVG2, which stands for 'Interior Ballistics of High Velocity Guns, version 2,' is a lumped-parameter, interior ballistic computer code. The code, which was developed at the BRL, is an updated version of the classic Baer-Frankle interior ballistic code. IBHVG2 is used for calculation of interior ballistic trajectories, including gas pressure, projectile displacement and projectile velocity as a function of time. The code treats both regular and dented propellants. It contains powerful variational and searching capabilities, so that it can, for example, search and find the 'best' propellant dimensions, given the maximum allowable gas pressure. This report thoroughly documents IBHVG2, so that all of its many features can be used effectively. The report contains a detailed description of the range of possible user input and a description of both the algorithms embodied along with the FORTRAN subroutines which implement them. There are also complete examples of input and output from the code. Although the code has been written to be as generally applicable as possible, the report has a short section describing modifications that are necessary to enable the code to run on various computers and compiler combinations. A machine-readable copy of the code can be obtained by contacting the authors of this report.					
20. DISTRIBUTION/AVAILABILITY OF ABSTRACT <input checked="" type="checkbox"/> UNCLASSIFIED/UNLIMITED <input type="checkbox"/> SAME AS RPT <input type="checkbox"/> DTIC USERS			21. ABSTRACT SECURITY CLASSIFICATION Unclassified		
22a. NAME OF RESPONSIBLE INDIVIDUAL Ronald D. Anderson			22b. TELEPHONE (Include Area Code) (301) 278-6102		22c. OFFICE SYMBOL SLCBR-IB-A

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I. INTRODUCTION

The efficient design of large caliber guns and their corresponding charges requires an accurate simulation of the interior ballistic cycle. Simple lumped-parameter models are usually sufficient to predict the gross ballistic variables such as chamber pressure and projectile velocity to precision rivaling experimental capabilities. This accomplishment allows ballisticians to focus on experiments which either validate the models or are used to extend the modeling effort. Since computer simulation is very inexpensive in relation to experimental testing, once it has been established that the model corresponds to actual firings, the designer can try out many different ideas under a variety of circumstances. The net result is a superior round at minimum cost.

This report describes one such code which is widely used in the interior ballistics community. IBHVG2, which stands for "Interior Ballistics of High Velocity Guns, version 2", was developed by describing the ballistic events as a set of ordinary differential equations which are solved by marching forward in time. One feature which has helped to popularize the code is its flexible method of inputting user options, allowing the designer to focus his energies on the ballistics instead of the computer programming aspects. Past experience suggests that IBHVG2 is general enough to investigate most gun/charge scenarios without any modifications to the computer algorithms.

Most useful computer codes are the product of evolution and IBHVG2 is no exception. The basic principles are described in the well-known Baer-Frankle report[1]. IBHVG1, which was written by Robert Deas of BRL, is essentially the Baer-Frankle methodology written in FORTRAN with an improved user-interface. Some ideas were also borrowed from MPRGUN written by Paul Baer, also of BRL. In 1981, mission requirements dictated that a new code be written which would properly model deterred propellants and provide a better description of heat transfer to the gun tube. Franz Lynn was the sole author of the coding efforts, although numerous discussions among the scientists in the Interior Ballistic Division of BRL helped shape the final form and goals. Development ceased after his untimely death in 1983.

The basic operation of the code is quite simple. From a sufficient description of the gun system and its propelling charge, IBHVG2 can simulate the burning of the primer and propellant while computing the time trace of a variety of variables to include: mean gas pressure and temperature of the gun chamber, acceleration and velocity of the projectile, and the mass fraction of each unburned propellant. One of the advanced features of the code is the ability to automatically vary its inputs for a new simulation in an iterative fashion. This is very useful for charge design work. As an illustration, the ballisticians could fix the maximum allowable gun tube pressure and require the code to vary some characteristic of a specific propellant (say, the grain web size) until the goal is attained. Such iterations can, in turn, be nested. Extending our example, one may desire to meet the target pressure while optimizing on the exit velocity of the projectile by varying another propellant characteristic. Detailed examples are included in Appendix E to serve as a guide to the reader and to demonstrate the versatility of the code.

Figures 1 and 2 are included to demonstrate the correspondence between range firing data and IBHVG2 simulations. The data come from a series of experiments investigating short, slotted sticks (25-mm) fired in a 155-mm howitzer (see reference [2]). They are representative of results one would expect for granular charges in a large caliber weapon. The input for computer simulation is based on propellant data obtained from closed-bomb experiments and

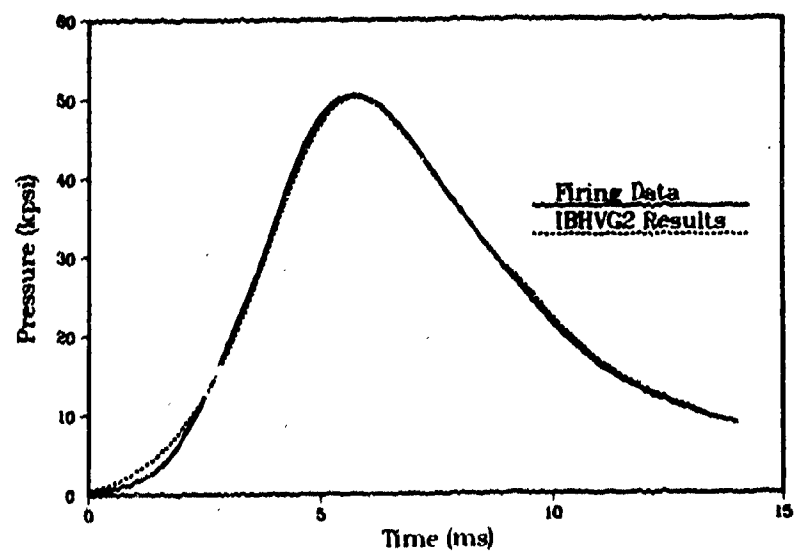


Figure 1. Comparison of Pressure Histories

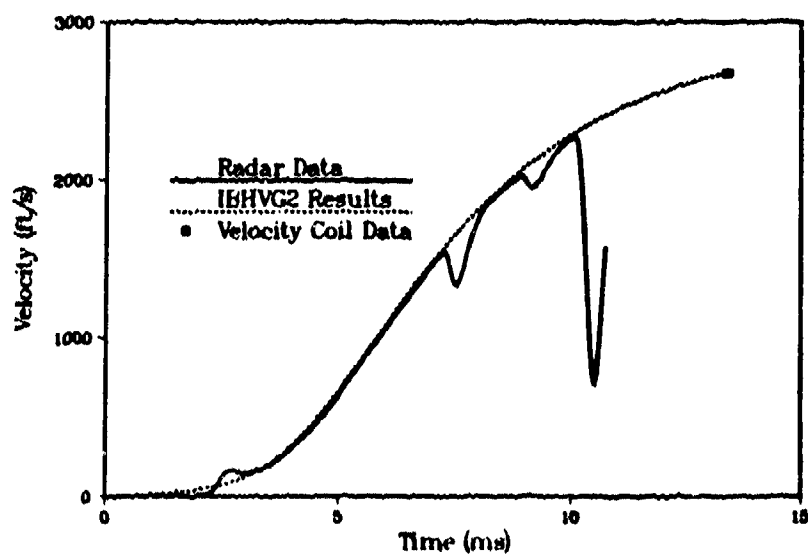


Figure 2. Comparison of Velocity Histories

the projectile resistance profile corresponds to previously recorded measurements for a M101 projectile. That is to say, there was no curve fitting since there are no free parameters; all input data either involved direct physical measurements or were obtained by independent experiments.

As one can see, the comparison of range data with an IBHVG2 simulation is reasonably good. Both the pressure and velocity histories appear to be within the experimental error of the measurements. This point is worth some elaboration. In these firings there are two sets of measurement records to estimate variance. One consists of time traces from redundant transducers of the same event such as two pressure gages at the same axial distance of the gun tube. The other involves measurements from repeated, but equivalent, firings. Both sets are useful for different reasons. The former gives quantitative information about transducer and measurement error, while the latter provides insight about reproducibility of the experiment.

One should note that the time origin for the firing data is arbitrary; therefore, to aid in the comparison, the origin of the data is adjusted such that the maximum pressure occurs at the same time as the simulation. Using this technique, the pressure simulation falls within the experimental uncertainty of the range data (pooled standard deviation of about 0.4 kpsi) with the exception of the first 2.5 ms. This region is of interest because it describes the portion of the interior ballistic event least understood.

There is a strong temptation to explain the disparity to the fact that IBHVG2 simulates the propellant burning uniformly, whereas, experiments have demonstrated that flamespreading is neither complete nor instantaneous immediately after ignition. Presumably, this would cause the pressure to initially lag behind the computed result. Examination of various transducer channels suggest another factor to be considered. It is common to observe two separate channels with results in excellent agreement everywhere except the first millisecond or so. This behavior could be attributed to slight variations in the individual pressure ports (sometimes described as "plugging") or it could be a manifestation of the finite dynamic response of the transducers. Pressure transducers for the study of ballistics are calibrated and chosen based on accuracy from static tests and linearity over the range; frequency response is of secondary importance. In summary, it is not clear which plays the most significant role, but it is obvious that this region contains the most uncertainty. The key point is that for early times IBHVG2 pressures tend to exceed those recorded on the firing range.

The velocity comparison shows two independent measurements from the range. The solid curve is obtained from Doppler radar where the time origin is the same as obtained for the pressure comparison described above. The oscillation exhibited prior to projectile exit is an artifact of the technique. The signal appears to have been severely attenuated, probably because this round had some blow-by gases which were absorbing the radiation. The bump at 2.5 ms should also be disregarded. This is typical of Doppler measurements due to the difficulty of discerning a velocity of a slow moving object. The star marks the velocity recorded independently via velocity coils near the gun muzzle. The time coordinate is arbitrary, but the velocity value is precise to within 0.2 percent (based on the pooled variance of 12 shots). The IBHVG2 estimate for muzzle velocity falls inside this bound.

While writing this report, we expected just to include a comparison from any former experiment. To our surprise, it appears that experimental curves are seldom compared to IBHVG2 simulations, although virtually all gun firings are preceded by some lumped-parameter calculation. Most investigations just compare the maximum pressure and the muzzle velocity. In the hands of an experienced ballisticians this may be sufficient. However, the primary reason for not comparing the curves is due to the difficulty of getting the range data and the

simulation results in a suitable format and on the same computer. It is the sincere hope of the authors that this will no longer be an obstacle. The code is now sufficiently portable to be run on most any computer with a FORTRAN compiler. As demonstrated in Appendix E, a single simulation can be executed on a microcomputer on the order of a minute. Therefore, it would be reasonable to run the code on the same computer which does the data acquisition. Then a comparison can be established immediately after the firing. It is clear that the best time to reconcile or verify a discrepancy is soon after the experiment when all the details are fresh.

Such an arrangement could have advantages beyond convenience. If the curves match as well as the one shown in this report over a wide range of ammunition, the simulation could almost be used as a quality control mechanism. Any significant deviations would signal a serious problem with either the experiment or what the user perceives as correct input. If, on the other hand, the curves do not match as well with some rounds as others, then we will have identified some new research issues. Documenting problem cases would, at the very minimum, aid future simulation efforts. Regardless, we predict a synergistic effect if some modeling is shifted to those who actually do the firing.

This report is designed to be both an introduction and a user's guide to IBHVG2. The first section is a complete reference manual for the construction of the user input decks. It is followed by a short description of each FORTRAN subroutine found in the code. The third section describes the ordinary differential equations and the constitutive relations used to create the code. Both the physics and the mathematical assumptions are briefly discussed. The remainder of the report describes issues about executing the code to include some examples.

This documentation is essentially an attempt to pull together much of the information known about the IBHVG2 code and put it in one place for the convenience of the user. The fact that both authors are novices at using the code probably served as an advantage. More times than we care to recount, one of us had to seek out an advanced user to understand something about the folklore or discover some fact which was "common knowledge" in using the code. Undoubtedly, in the process we have absorbed some information which now makes sense to us, but is not clearly stated in this report. Familiarity has a tendency to obscure subtle understandings. When the reader uncovers such failures, we would appreciate hearing from you so it can be corrected for a future guide. Comments about useful additions or omissions are also encouraged.

II. DESCRIPTION OF INPUT DECKS

A. Syntax Rules

Input data stream for IBHVG2 consists of a series of "decks." The start of each deck is demarcated by a line starting with a "\$" in the first column and followed by a four letter mnemonic. All lines of input data between decks should in principle be closely related ballistic parameters.

Inputs are free format in that more than one can be included per line. Comments may be incorporated by preceding them with a "\$" in any column other than the first. The formats are

variable = value

for ordinary unsubscripted variables and

variable (sub) = value₁, ..., value_n

for subscripted variables, with commas and/or blanks between consecutive variable/value constructs. Integer and real formats are legal for all numerical values. Character strings must be delimited with either apostrophes or quotes. All keywords, to include deck cards and variable names, must be in uppercase.

The first blank between consecutive variable/value fields is the legal delimiter; any additional ones are ignored. Blanks embedded in variable names, subscripts, or numeric values are significant but illegal. Leading blanks in character strings are squeezed out.

An omitted "(sub)" in a subscripted variable is taken to be 1. Consecutive values fill locations sub, sub+1, sub+2, etc., while pairs of commas with nothing or blanks between them advance to the next subscript (i.e., a subscript is skipped over). All character variables default to blank strings while numerical variables default to either zero or a convenient value listed below. If a variable is multiply-defined, the last input overrides all previous ones. All syntax errors are flagged. A list of all valid deck names follows as well as descriptions of all variables within each deck.

B. Decks

SCOMM

All cards between a \$COMM and the next deck card are ignored to allow the tagging of a data input file with user comments.

SEND

This control card signifies end-of-input for the current case. IBHVG2 will then execute. Afterwards, it will start reading the next card, if any. This is to allow the processing of other runs or for the code itself to generate runs internally. An end-of-input condition for a user's input deck is processed as if the \$END card was read in. *A frequent mistake by novice users is to include the \$END and follow it by a blank line. The code assumes this is another run and proceeds to produce errors due to insufficient information.*

\$FIND

For inputs to a general variation-and-search utilizing function minimization techniques (see reference [6] for algorithm). Up to six \$FIND decks may be submitted in one run allowing a variation in six dimensions. A list of additional option variables for outputting is found at the end of this section.

VARY	name of parameter including any subscript
DECK	name of deck containing parameter; 4 characters max; may not be PARA, PDIS, FIND, PMAX, or TDIS
NTH	number of deck if there are several with same name (default = 1)
FROM	initial value of parameter in proper units
EPS	error tolerance
OUTV	name of desired output variable from run completion variables (see end of this section)
CODE	0 to achieve desired value of OUTV variable 1 to maximize OUTV variable
VAL	desired value if CODE is 0, else ignored
MULT	multiplier for function-minimizer residual (default = 1.0)
MIN	min allowable value of VARY parameter (default = 0.0)
MAX	max allowable value of VARY parameter (default = 1.0E+10)

\$GUN

For variables related to gun-tube geometry, namely:

NAME TYPE	name of gun; 28 characters max
CHAM CV CVOL	chamber volume [<i>in</i> ³]
GRVE	groove diameter [<i>in</i>]
LAND	land diameter [<i>in</i>]
TRAV LENG	travel to shot-exit [<i>in</i>]
G/L	ratio of groove to land surface area; smooth-bore if G/L=0 [default]
TWST	rifling twist [<i>calibers /turn</i>]
LOPT	0 [default] to ignore LDEN 1 to calculate CHAM from total charge weight and LDEN 2 to calculate total charge weight from CHAM and LDEN; primer & charge weights must be specified; they are scaled proportionally to sum to required total charge weight
LDEN	ratio total charge weight/chamber volume [<i>g /cm</i> ³]; used when LOPT = 1 or 2 [default = 0.2] <i>CAUTION: LDEN calculations are done after C/M (which may have altered charge weights) used.</i>
CLEN	effective chamber length [<i>in</i>] for scaling in-chamber pressure gauge locations [default = CV/bore area]
NGAG	number of gauge locations [default = 0 <i>or</i> 30]
GLOC	gauge location array of size NGAG [<i>in</i>] [default = 0.0]. Dis- tance is measured (+) downtube from the breech or (-) into chamber from the initial position of the projectile base. <i>CAUTION: IBHVG2 will discard duplicate or out-of-range values and will rearrange distances in ascending order, if neces- sary. This should be kept in mind when using, for example, a \$SAVE deck--the position you reference may not be the one the computer code decided upon.</i>

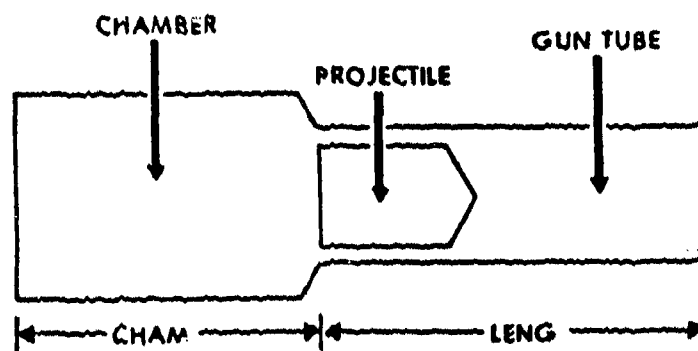
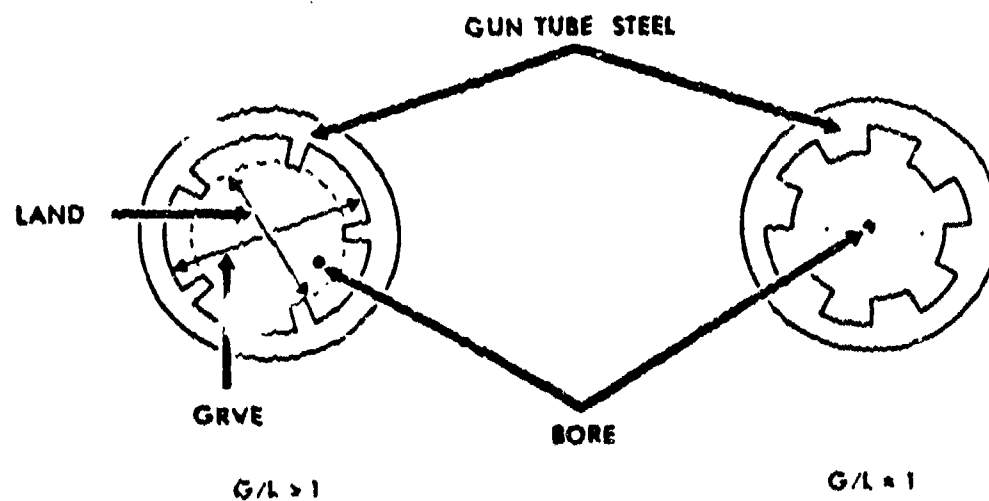


Figure 3 Gun Parameters

SHEAT

For heat-loss-related variables, namely:

TSHL	tube shell thickness for heat sink [in] [default = 0.004]
CSHL	shell specific heat [$\text{in-lb}_f/\text{lb}_m\text{-}^\circ\text{K}$] covering a broad range of steels [default = 1848.0]
RSHL	shell material density [lb_m/in^3] [default = 0.284]
TWAL	initial wall temperature [$^\circ\text{K}$] [default = 293.0]
H0	free convective heat transfer coefficient for air in the tube [$\text{in-lb}_f/\text{in}^2\text{-sec-}^\circ\text{K}$] [default = 0.0648]
HL	0 to ignore heat losses in energy balance 1 [default] to include heat losses

SINFO

For run-related inputs. The variables are:

DELT	max integration time step [sec] [default = 0.0001]
DLPU	1 [default] for DELP in units of time [sec] 2 for DELP in units of projectile travel [in]
DELP	integrator logout & print step [sec] or [in]; reset to DELT if DLPU = 1 and DELP < DELT
SOPT	0 to suppress file storage of run output [default] 1 to write trajectory data for each run into output file STORE for post-processing 2 to write only single-line summaries for each parametric run into file STORE; ignored if non-parametric runs are being conducted
GRAD	1 for Lagrange gradient [default] 2 for Pidduck-Kent gradient
UNIT	unit system for output; not implemented yet, but will be a choice between 0 for SI and 1 for English

POPT	print option array of size 6 [all defaults = 1]. Detailed descriptions given below between the double bars:
POPT(1)	0 to suppress 1 to print input echo
POPT(2)	0 to suppress trajectory print 1 to print default trajectory variables 2 to print user-specified \$TDIS variables
POPT(3)	0 to suppress 1 to print IB summary
POPT(4)	0 to suppress blowdown calculation 1 to print blowdown phase (see reference [5], chapter 9) to include tube recoil when the recoil option is in effect (see \$RECO)
POPT(5)	0 to honor above print options for every run of parametric variation 1 to honor above print options for first run of parametric variation and print a single-line summary thereafter 2 like 1, but summary print variables supplied via \$PDIS specifications
POPT(6)	is currently unused
RUN TITL	run title on output pages; 48 character* max
EPS	max error for integrator time-step adjustment and transition tolerances [default = 0.002]
CONP	0 for usual non-constant-pressure run [default] 1 for run with constant pressure maintained by varying the burning rate of the single charge 2 for run with constant pressure maintained by varying the surface area of the single charge
PRES	desired constant breach pressure [psi] when CONP option is 1 or 2
TOL	error tolerance [psi] for PRES [default = 1.0]

\$PARA

For parametric variations; up to four \$PARA decks per run permit a four dimensional matrix to be systematically tried. The DECK must contain a nominal value of the variable to be VARY'd.

VARY	name of parametric variable including any subscript
DECK	name of deck containing variable; 4 chars max; may not be PARA, PDIS, FIND, PMAX, or TDIS
NTH	deck number if there is more than one (default = 1)
FROM	initial value of variable
TO	final value of variable
BY	increment/decrement value

\$PDIS

Each deck defines one variable to be printed in lieu of the default set for each line of the parametric summary print. There can be up to 11 \$PDIS decks in effect: one for each variable printed for the interior ballistic cycle. Be sure to include the line POPT(5)=2 (print option) in the \$INFO deck. To write the summary information to a file attached to UNIT=7, include the line SOPT=2 in the \$INFO deck. (\$PDIS is similar to the \$TDIS deck). A list of additional option variables for outputting is found at the end of this section.

SHOW	name of variable to print; 4 chars max
DECK	name of deck containing the desired variable; any deck may be named except PARA, PDIS, FIND, and PMAX
NTH	number of deck if more than one (default = 1)
MULT	number to multiply data value by (default = 1.0)
DIV	number to divide data value by (default = 1.0)
REMI REMK	20 character remark string for titles and file STORE

SPMAX

For variation of charge weight or web to achieve a desired maximum breech pressure. If web is varied, grain ratios rather than gr.in dimensions may be the better choices in the \$PROP deck concerned. The \$PROP deck must contain a nominal value of charge weight and web, even though one or the other will be varied in the \$PMAX operation. Note that a DECK='PROP' card is not needed in a \$PMAX; the program knows that it must be varying some propellant characteristic. If you include DECK='PROP', the program will complain but will still do the proper things.

VARY	variable name in a \$PROP deck including any subscript
NTH	number of \$PROP deck (default = 1)
TRY1	first value of VARY to try
TRY2	second value of VARY to try; third and subsequent guesses are based on interpolation. NOTE: the last two guesses from the previous run are employed as the first two guesses in second and subsequent \$PARA runs
PMAX	maximum breech pressure [psi] sought
EPS	error tolerance [psi] for PMAX; (default = 1.0).
LOOP	max number of tries before quitting (default = 20)
MIN	minimum allowable value of VARY parameter (default = 0.0)
MAX	maximum allowable value of VARY parameter (default = 1.0E+10)
NPMX	0 (default) if PMAX refers to the max breech pressure ever achieved during the run n where $n \in (1, 2, \dots, 5)$ if PMAX refers to the NPMX-th local breech pressure maximum achieved

SPRIM

For primer data. The "primer" is considered completely burned at the start of integration. For this reason, it is considered wise to include only enough primer to reach sufficient pressurization to ignite the propelling charge. Real primers are usually modelled with IBHVG2 by simulating the function with both a \$PRIM and a \$PROP deck. A typical correspondence is 10% by weight for the \$PRIM and 90% as a \$PROP. Constant-pressure runs may include or exclude a primer. A primer is mandatory for conventional simulations.

NAME	name of primer; 28 characters max
TYPE	
GAMA	specific heat ratio
FORC	force [$\text{ft} \cdot \text{lb}_f / \text{lb}_m$]
COV	covolume [$\text{in}^3 / \text{lb}_m$]
TEMP	flame temperature [K]
CHWT	weight [lb_m]
WT	
CHGW	
C	
CW	

SPROJ

For projectile-related variables.

NAME TYPE	projectile designation; 28 characters max
PRWT WT	projectile weight [lb_m]
COPT	0 [default] to ignore C/M 1 to calculate PRWT from total charge weight & C/M 2 to calculate total charge weight from PRWT & C/M; primer and all charge weights must be specified, but they will be scaled proportionally to sum to the required total charge weight
C/M	used when COPT=1 or 2; ratio of total charge weight and projectile weight [default = 1.0]
SOPT	0 [default] bypass PRWT calculation based on subprojectile parameters and sabot formula 1 find PRWT based on projectile weight estimation formula of Burns (see Reference [3]) 2 find PRWT based on same weight estimation formula using coefficients yielding 15% lighter sabot
WTSP	subprojectile weight [lb_m]
LSP	subprojectile length [in]
DSP	subprojectile diameter [in]
PDES	max design pressure [psi] for sabot projectile
SABO	sabot weight [lb_m]; not input—set by IBHVG2

SPROP

Defines a main propelling charge element. IBHVG2 will recognize up to five such decks and considers them independently (i.e., order is unimportant). The following are basic input variables most useful for describing homogeneous, undeterred grains:

NAME TYPE	name of propellant; 28 chars max
RHO DENS	density [lb_m/in^3]
GAMA	specific heat ratio
FORC	force [$lbf \sim lb_f / lb_m$]
COV	covolume [in^3/lb_m]
TEMP	flame temperature [K]
CHWT WT CHGW C CW	weight [lb_m]
ALPH	burning rate $= \beta P^\alpha$ (in/s) where P is mean pressure [psi]
BETA	burning rate exponent, α
EROS	erosive burning coefficient, empirical factor multiplied by projectile velocity (in/s) to add to burning rate [default = 0.0]
GRAN FORM	granulation code chosen from 7PF (or 7P), 1PF (1P), CORD, RECT (SLAB), SPHR (BALL), SLOT, 37HX (37H), 19HX (19H), 19PF (19P), GEN, PIE (STAR), GHEX (HEX), MONO (see Appendix B)

WI WIN	inner web for cylindrical/hexagonal grains [<i>in</i>]
WO WOUT	outer web for cylindrical/hexagonal grains [<i>in</i>]
WM WMID	middle web for cylindrical/hexagonal grains [<i>in</i>]
WEB WB	common value of all inner, middle, and outer webs [<i>in</i>]; also resets WI/O
D DIAM GDIA	grain diameter, if applicable [<i>in</i>]
PD DP PDIA	perf diameter, if applicable [<i>in</i>] [default = 0]
SLOT	slot width in SLOT and PIE grains [<i>in</i>]
NSLT	number of diametral slots in PIE grain ≥ 2
NRNG	number of concentric rings of perfs around central perf in HEX grains; ≥ 0 [default = 2]
L GL LEN GLEN	grain length, if applicable [<i>in</i>]
WIDTH	grain width in RECT grains [<i>in</i>]
THCK	grain thickness in RECT grains [<i>in</i>]
NSUR	number of depth/surface pairs for GEN grain [default = 1, max = 10]
DEPB	depths-burned array [<i>in</i>] for GEN grains; ignored if NSUR = 1
SURF	surface area array [<i>in</i> ²] for GEN grains
IGNC	code specifying charge ignition: 0 to ignite at start of integration [default] 1 to ignite at some time [<i>s</i>] 2 to ignite at some projectile travel [<i>in</i>] 3 to ignite at some mean pressure [<i>psi</i>] 4 to ignite at some Z (mass fraction burned) of the charge described by the previous SPROP deck

THRC	threshold value for ignition if IGNC > 0
IGNS	array of size 3 specifying ignition codes for the perf, end, and lateral grain surfaces, respectively; same codes as IGNC; ignored if IGNC > 0.0
THRS	array of threshold values for surface ignition
PA-B	0 [default] for standard treatment of charge; set automatically if grain has no perfs or if run has either constant-pressure option set 1 for perf-augmented burning of charge until grain fracture
DSCF	Robbins-Horst discharge coefficient in weight flux computation for perf-augmented burning model [default = 1.0] (see Reference [4])
FRAC	0 [default] for no user-defined grain fracture criterion of charge with PA-B = 1. <i>NOTE: web burn-through turns off perf-augmented burning.</i> 1 to specify pressure-difference grain fracture threshold for charge with PA-B = 1. <i>NOTE: web burn-through triggers fracture.</i>
NFRG	number of fragments when 1PF grain fractures ≥ 1
THRF	absolute value of difference between chamber and perf pressures for grain fracture [psi]; ignored if FRAC = 0 [default = 0.0]

IBHVG2 will calculate grain dimensions if given either actual measurements, or alternatively, a single measurement combined with ratio specifications. This latter technique is quite useful when the code is used to optimize a charge design. For example, a CORD grain can be defined by D and L, or by L and the ratio L/D. For a 7-perforated grain, WI and DP together with WI/O, D/DP, and L/D will completely specify the grain geometry. The slot width of a SLOT or PIE grain will be calculated given SW/D and D. Care must be taken to avoid over-specified or inconsistent information since the computer program may make arbitrary or poor decisions. IBHVG2 prints the grain dimensions prior to ballistic calculations; experienced users of the code always scrutinize this portion of the output for any surprises.

L/D	grain length/grain diameter
L/DP L/PD	grain length/perf diameter
D/DP D/PD	grain diameter/perf diameter

L/WD	grain length/grain width
WD/T	grain width/grain thickness
SW/D	slot width/grain diameter
WI/O	inner web/outer web for multiperforated grains; web eccentricity for single perf grains [default = 1.0]

For dettered grains, further (or replacement) inputs to handle variable thermochemistry and burning rates are necessary. Visualize each grain having, in general, three disjoint surfaces:

Surface	Description
P	perf (includes the slot, if any)
E	end
L	lateral

Extending inward from each surface are layers 1, 2, 3, and 4 (the innermost or "core"), and any or all of the first three may be of zero thickness (nonexistent) on one or more of the P, E, or L surfaces. The core layer is always present and its properties, unlike those of the outer layers, are independent of depth. As there is only one common 4th layer, L-specifications for the core override all others to prevent conflicts. All depth-varying properties are consecutively defined at the outer surface of each layer from the outside in so each of the following is an array of size 4. Linear interpolation is performed by IBHVG2 when intermediate values are required.

RHOP	density [lb_m/in^3]	on P surfaces
RHOE		on E surfaces
RHOL		on L surfaces
GAMP	specific heat ratio	on P surfaces
GAME		on E surfaces
GAML		on L surfaces
FRCP	force [$ft-lb_f/lb_m$]	on P surfaces
FRCE		on E surfaces
FRCL		on L surfaces
COVP	covolume [in^3/lb_m]	on P surfaces
COVE		on E surfaces
COVL		on L surfaces
TMPP	flame temperature [K]	on P surfaces
TMPE		on E surfaces
TMPL		on L surfaces

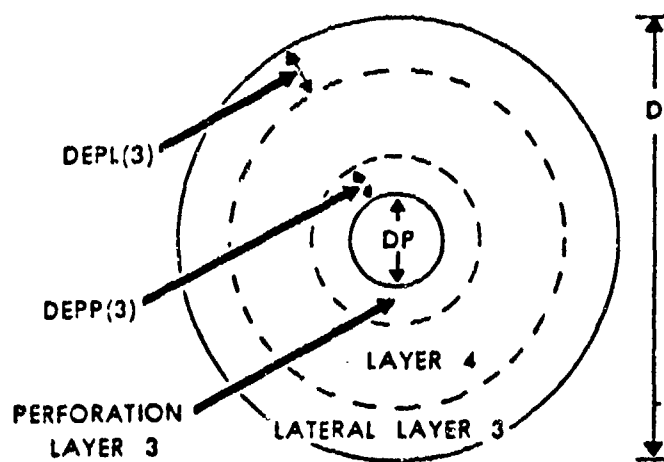


Figure 4. Two-Layer, Single-Perf Grain (end-view)

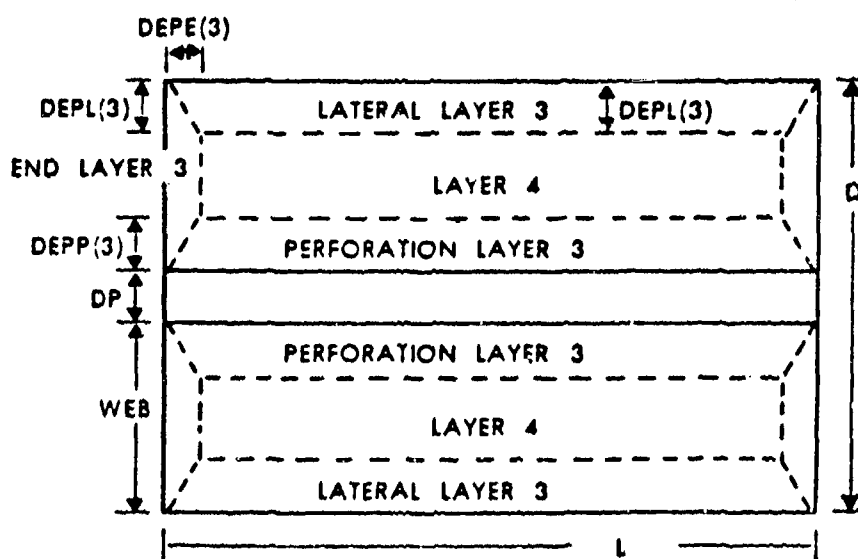


Figure 5. Two-Layer, Single-Perf Grain (lateral-view)

Arrays of size 3 specify the transition depths [in] between the first and second, the second and third, and the third and fourth layers, respectively, for each surface.

DEPP	transition depths	on P surfaces
DEPE		on E surfaces
DEPL		on L surfaces
	[defaults = 0.0]	

Transition depths will be calculated by IBHVG2 if positive ratios specifying transition depths as fractions of surface-to-surface distance are input. Arrays of size 3 store the ratios [the default for all values is 0.0].

DP/S	ratios of transition depths on P surfaces to WI; used for perforated grains only
DE/S	ratios of transition depths on E surfaces to: <ul style="list-style-type: none"> • min(GL,WIDTH) for RECT • GL for perforated & CORD grains
DL/S	ratios of transition depths on L surfaces to: <ul style="list-style-type: none"> • D for CORD & SPHR grains • THCK for RECT grains • WI for perforated grains
FP/L	ratios of DP/S to DL/S; DP/S values will be found given FP/L and DL/S; useful for defining a relation between transition depths on P and L surfaces

Finally, burning rate data for the outer surface of each layer may be incorporated via several alternative methods. It should be noted that interpolation is linear for depths and betas, but logarithmic for alphas and tables of pressure versus burning rates.

NTBL	method of specifying burning rate inputs ... absolute value is number of table entries on every surface layer; range of values: -10 to +10 <ul style="list-style-type: none"> < 0 to specify betas and alphas as tabular functions of mean pressure [psi], NTBL triples in all = 0 to define one beta/alpha pair [default] > 0 to specify burning rates [in/sec] as tabular functions of mean pressure [psi], NTBL pairs in all. <i>NOTE: if NTBL = 1, burning rate is constant so corresponding pressure value, if any, is ignored.</i>
PR1L	pressures [psi] on outside of layer 1, L surface. PR2L, PR3L, PR4L, PR1E, PR2E, PR3E, PR4E, PR1P, PR2P, PR3P, PR4P are defined similarly.

BR1L	burning rates (<i>in/sec</i>) on outside of layer 1, L surface. BR2L, BR3L, BR4L, BR1E, BR2E, BR3E, BR4E, BR1P, BR2P, BR3P, BR4P are defined similarly.
CF1L	burning rate coefficients (betas) on outside of layer 1, L surface. CF2L, CF3L, CF4L, CF1P, CF2P, CF3P, CF4P are defined similarly.
EX1L	burning rate exponents (alphas) on outside of layer 1, L surface. EX2L, EX3L, EX4L, EX1E, EX2E, EX3E, EX4E, EX1P, EX2P, EX3P, EX4P are defined similarly

\$RECO

For recoil data. In the model currently available, the gun tube freely recoils under the influence of breech pressure less resistance pressure. In IBHVG2 Version 400, this option has not been fully tested and should not be considered reliable.

RECO	0 for fixed tube, no recoil (default) 1 to employ recoil option
RCWT WT	weight (<i>lb</i>) of tube and recoiling parts
NAME TYPE	name of recoil system; 28 characters max

\$RESI

This precedes resistance pressure inputs. The variables are:

NPTS	number of travel/pressure pairs (min = 0, max = 20)
TRAV	projectile travel array of size 20 (<i>in</i>)
PRES	resistance pressure array of size 20 (<i>psi</i>)
AIR	0 to suppress adding in air resistance 1 to include air resistance [default]
HTFR	fraction of work done to overcome barrel resistance which is used to pre-heat tube wall; $0.0 \leq \text{HTFR} \leq 1.0$ [default = 0.0]

SSAVE

Actually, not a deck card, but a control card. If it is the first card in a run after an \$END card, the values of all input variables are retained, so that succeeding decks need only update selected variables. If an \$END card is not followed by a \$SAVE card, all input variables must be reinitialized. See test cases 3, 4, and 5 in Appendix B for examples.

STDIS

Each deck defines one variable to be printed in lieu of the default set for each line of the trajectory print. There can be up to 11 \$TDIS decks in effect: one for each variable printed for the interior ballistic cycle. Be sure to include the line POPT(2)=2 (print option) in the \$INFO deck. To write the trajectory information to a file attached to UNIT=7, include the line SOPT=2 in the \$INFO deck. (\$TDIS is similar to the \$PDIS deck). The list of option variables available for use is found at the end of this section.

SHOW	name of variable to print from deck TRAJ; 4 characters max
MULT	number to multiply data value by [default = 1.0]
DIV	number to divide data value by [default = 1.0]
REMI REMK	20 character remark string for titles and file STORE

Trajectory Variables

Below is a list of keyword variables which can be used in conjunction with the \$TDIS, \$FIND, and \$PDIS decks to reference quantities other than the default set. To use them with \$PDIS and \$FIND, one must include the line DECK="TRAJ"; a reference within \$TDIS assumes the keyword will come from the following list. Test cases 3 demonstrates the use of \$TDIS to change the trajectory display printed during the ballistic cycle.

MEAN	mean gas pressure in chamber [psi]
PRFP	array of size 5 of mean gas pressure in perfs [psi] of each charge; equal to MEAN if no perf-augmented burning in that charge at current time step
GAGE	array of size 30 of gage pressures [psi]
BRCH	breech pressure [psi]
BASE	pressure at projectile base [psi]
PDOT	$d(\text{mean chamber pressure})/dt$ [kpsi/mz]

PDTP	array of size 5 of $d(\text{mean perf pressure})/dt$ [kpsi/ms], one for each charge
TBAR	mean gas temperature in chamber [K]
PRFT	array of size 5 of mean gas temperature in perfs [K] of each charge; equal to TBAR if no perf-augmented burning in that charge at current time step
FRCR	bore-friction resistance pressure [psi]
AIRR	air resistance pressure [psi]
TOTR	sum of FRCR and AIRR
TWAL	temperature of tube wall shell [K]
WTB	array of size 5 of weight burned of each charge [lb _m]; reference by subscript
WTBR	array of size 5 of weight-burning rate of each charge [lb _m /sec]; reference by subscript
WTBT	total weight of gas in chamber [lb _m]
PRJE	projectile translational kinetic energy [in-lb _f]
PRJ%	$PRJE * 100 / TOTE$
PRPE	propellant and gas kinetic energy [in-lb _f]
PRP%	$PRPE * 100 / TOTE$
ROTE	projectile rotational kinetic energy [in-lb _f]
ROT%	$ROTE * 100 / TOTE$
FRTE	barrel-frictional work to tube [in-lb _f]
FRT%	$FRCE * 100 / TOTE$
FREE	barrel-frictional work not absorbed as heat to the tube wall [in-lb _f]
FRE%	$FREE * 100 / TOTE$
DRGE	work done against air in barrel [in-lb _f]
DRG%	$DRGE * 100 / TOTE$
RECE	kinetic energy of recoiling tube [in-lb _f]

REC%	$RECE * 100 / TOTE$
HETE	energy lost as heat convected to tube wall [<i>in-lb_f</i>]
HET%	$HETE * 100 / TOTE$
LOSE	sum of all energy losses [<i>in-lb_f</i>]
LOS%	$LOSE * 100 / TOTE$
TOTE	total chemical energy released by combustion [<i>in-lb_f</i>]
EDOT	$d(TOTE)/dt$ [<i>in-lb_f/sec</i>]
GASE	internal energy of gas [<i>in-lb_f</i>], i.e., $TOTE - LOSE$
GAS%	$GASE * 100 / TOTE$
SRF	array of size 5 of burning-surface area of each charge [<i>in²</i>]; reference by subscript
SRFT	total surface area of all ignited charges [<i>in²</i>]
TIME	time [<i>ms</i>]
TRAV	projectile displacement from initial position [<i>in</i>]
VEL	ground-based projectile velocity [<i>ft/sec</i>]
ACCL	projectile acceleration [<i>G's</i>]
Z	array of size 5 of charge weight fractions burned; reference by subscript
DB-P	array of size 5 of depth burned into P surface of each charge [<i>in</i>]; reference by subscript
DB-E	same as above for E surfaces
DB-L	same as above for L surfaces
DB-F	same as above for F (fracture) surfaces
BR-P	array of size 5 of burning rate on P surface of each charge [<i>in/sec</i>]; reference by subscript
BR-E	same as above for E surfaces
BR-L	same as above for L surfaces
BR-F	same as above for F (fracture) surfaces

Run Completion Variables

These are output variables defined after a complete IBHVG2 run. Typically they represent some global extrema which can only be ascertained at the conclusion of ballistic computation. For example, a maximum pressure is determined after shot ejection, while there could be several local maxima during the pressure history. The variables may be referenced by name using \$PDIS (with DECK='OUT') as in test case 6, or by \$FIND as the value inserted for OUTV as shown in test case 5.

PMAX	max breech pressure [psi]
HUMP	array of size 5 of local breech pressure maxima [psi]
GMAX	array of size 30 of gauge pressure maxima [psi]
VMUZ	muzzle velocity [ft/s]
AMAX	max acceleration [g's]
BMAX	max base pressure [psi]
X@BO	array of size 5 of projectile position [in] at charge burnouts; reference by subscript
PMUZ	base pressure at shot exit [psi]
ZMUZ	array of size 5 of charge weight fractions burned at shot exit; reference by subscript
IMPL	final impulse (momentum) [lb _f -s]
LDEN	calculated loading density [g/cm ³]

III. SUBROUTINE DESCRIPTIONS

AUXGEN

check consistency of charge weight and densities specified for FRMGEN charge

AUXHEX

add to weight of core of nth grain the contributions from P, E, and L layers with linearly-varying density ... used for hexagonal or cylindrical grains with NPERFS(NTH) number of perfs

AUXMON

add to weight of core of nth grain the contributions from P, E, and L layers with linearly-varying density ... used for monolithic grains only

AUXSLT

add to weight of core of nth grain the contributions from P, E, and L layers with linearly-varying density ... used for slot grains only

AUXSTR

add to weight of core of nth grain the contributions from layers with linearly-varying density on IASUB-th surface ... used for rectangular grains only

BADBERN

determine if grain surfaces in 01p, slot, 07p, 19p, 19h, or 37h have burned beyond core of grain

BLDATA

define static parameters, including I/O device numbers, alphanumeric characters set, and version number of IBHVG2

BRNCMP

return a burning rate through BRNCMP

BRNRAT

lookup burning rates as function of pressure and interpolate linearly as function of depth burned

BULDEK

define input variables for projectile

CALPRJ

calculate projectile weight, if required, based on projectile weight estimation formula cited in ARBRL-TR-02364, p. 24, by Burns (See Reference [3])

COMDEK read through comment deck

CPRCHK error check input if constant pressure run

CPREDA store current values before and restore values after tentative integration step for constant pressure run

CRITIG return value of ignition-criterion variable for nth charge based on ignition code for comparison with threshold value

CRKLIN parse input line, crack and classify fields as numeric, string, or variable name, and flag syntax errors

CRKNUM stash numeric value in field number, NFIELD, or flag error

CRKSUB stash integer subscript in field number, NFIELD, or flag error

CRKTTT stash start and stop columns of string in field number, NFIELD

CRKVAR stash variable name and subscript, if any, in field number, NFIELD, or flag error

DATINP initialize input variables and call appropriate input routines

DEFPAG define number of lines/output page

DERIV1 calculate derivatives for ODE solver during 1B cycle

DERIV3 calculate derivatives for ODE solver during evacuation phase (treatment drawn from Corner, Chapter 9 of Reference [5])

DFQSET set up eqns for solver KUTMER

DODPDT calculate $d(\text{mean pressure})/dt$

DRIVER drive IB solver in selected modes

ECHOIN echo inputs

ECHOPR echo propellant input data

ENEQST calculate mean temperatures and pressures

EVPREP initialization and setup for evacuation cycle

FILLCB fill common blocks as input cards are interpreted

FINDEX define input variables driving automatic program search for desired conditions

FNEVAL compute residual as function value FBAR for FUNMIN

FORMFN calculate instantaneous grain surface areas and fractions burned for the grains in each charge

FRM01P	find surface areas for 01-perf cylindrical grain geometry
FRM07P	find surface areas for 07-perf cylindrical grain geometry
FRM19H	find surface areas for 19-perf hexagonal grain geometry
FRM19P	find surface areas for 19-perf cylindrical grain geometry
FRM37H	find surface areas for 37-perf hexagonal grain geometry
FRMADJ	return trial value of surface area in constant pressure run
FRMCRD	find surface areas for cord grain geometry
FRMGEN	find surface area for charge with user-specified values of surface area as function of depth burned
FRMHGX	find surface areas for general hexagonal grain geometry
FRMMON	find surface areas for monolithic, perforated, cylindrical grain geometry
FRMPIE	find surface areas for pie grain geometry
FRMSLT	find surface areas for slotted grain geometry

FRMSPH find surface areas for spherical grain geometry

FRMSTR find surface areas for strip (rectangular) grain geometry

FSTORE store parameter values determined by FUNMIN

FUNMIN finds the minimum of function of n variables based on method in BRL-TN-1677 by J.D. Wortman (See Reference [6])

GAGSET find and sort gage positions

GENISL finds the surface area-contributions due to inner slivers for a multiperforated propellant grain

GENOSL finds the surface area-contributions due to outer slivers for a multiperforated propellant grain

GRADNT calculate pressure at breech, projectile base, & gages

GUNDEK define input variables for gun tube

HDRSTO store descriptive information in file for post-run processing of detailed IB and evacuation cycles

HELPPR format and build output lines for ECHOPR

HETDEK define input variables used in heat loss calculations

HEXCOR

find surface area contribution from rounded corners of multiperforated hexagonal propellant grain

HEXOSL

find surface area contribution for outer slivers in multiperforated hexagonal propellant grain

HLRATE

calculate heat-loss rate from treatment of Black and Comenetz in Chap. 5, vol. 1 of NDRC hypervelocity report (See Reference [7])

IBHVG2

Interior Ballistics of High-Velocity Guns, 2nd version (main program unit)

IBPREP

initialization and setup for ballistic cycle

INFDEK

define miscellaneous input run variables

INITCP

calculate initial conditions for constant-pressure run

INITPR

define properties of air in chamber and initialize some integrals with primer information

INTBAL

initiate and control calculations for IB cycle and bore-evacuation phase

KMPAUX

print user-requested values in trajectory print form

KMPRN1

print details at current time step in interior ballistic cycle

KMPRN2

print details at current time step in evacuation phase

KMTERM1 establish values of variables representing the transition conditions checked by KUTMER in IB cycle

KMTERM2 establish values of variables representing the transition conditions checked by KUTMER in evacuation cycle

KUTMER 5-step Runge-Kutta ODE integrator with auto-adjustment of step size to achieve accumulation tolerances as well as transition and print conditions

LCHECK check layer depths for consistency and find initial current-layer-exposed for each surface of nth grain

LDEFIN calculate layer-transition depths bases on ratios

LIMITF check whether any values set by FUNMIN are out-of-range

MAXDER define input variables for maximum pressure search

MGRATE calculate mass-generation rates, energy-generation rate, and related derivatives in chamber and perfs

MINAUX print user-requested values in parametric print form

MINPET compressed print parametric runs

MXBRPR adjust single input variable to achieve desired maximum pressure

NEWEPS reset double-sided integrator tolerance EPSL

NEWFLG update flags and clean up after each print step

OUTDEK define program-accessible output variables

PACKER encode utility for input parsing routines

PAGCHK begin new output page with appropriate headings when necessary

PARDEK define input variables dealing with automatic parametric variation of desired run variables

PDSDEK define input variables dealing with user-selected printing on parametric compressed print summary

PICKDT compute maximum integration step size

POLYN compute the integral for mass of an object with a density changing linearly in coordinate x . For example, if the object had two dimensions L and W for planes 1 and 2 which are perpendicular to x , then the integral would be:

$$Mass = \int_{x_1}^{x_2} \left[L_1 + \frac{L_2 - L_1}{x_2 - x_1} (x - x_1) \right] \left[W_1 + \frac{W_2 - W_1}{x_2 - x_1} (x - x_1) \right] \left[\rho_1 + \frac{\rho_2 - \rho_1}{x_2 - x_1} (x - x_1) \right] dx.$$

PRIDEK define input variables for primer

PRPDEK define input variables for propellant description

PSTORE store parameter values from matrix

RATIOS

recalculate charge weights, projectile weight, or chamber volume based on input options and ratios

RDLINE

read input card-image

RECDEK

define input variables for gun recoil

REDOFF

accept last integration step for constant pressure run or prepare for restart of last step

RESDEK

define input variables for resistance profile

RESIST

compute resistance pressure to projectile motion

RUNDAT

define the machine precision limit; return a current date through DAYR and time thru TIMR (TIMR is highly system-dependent and has been commented out)

SAVDEK

process \$SAVE control cards

SETVAR

set a variable VNAME to number in VALUE for parametric variation and search routines or retrieves current contents

SHOTGO

set a shot-start flag based on initial chamber pressures and prepares for first search for maximum pressure

SPECIN

same purpose as POLYIN, but modified to accommodate a SLOT geometry

STASHD	move double precision number
STASHI	convert double precision to integer
STDPRP	set default propellant properties
STRTRD	define control cards, initialize page control, and common blocks
TDSDEK	define user-selectable trajectory print variables
THERMI	return thermodynamic information interpolated linearly on depth burned
TRJDEK	define program-accessible output variables
TRJSUM	print run summary through projectile exit
UPDATE	post-print-step update
UPDAUX	find current layer exposed for jth surface of ith grain
VENTPF	find dm/dt from perforations based on method of Robbins & Horst in ARBRL-MR-03295 (See Reference [4])
WRAPUP	is merely a program stub. Users may desire to include their own system clean-up commands, etc.

IV. ALGORITHM DESCRIPTIONS

A. Calculation of Mean Temperature and Pressure

By the First Law of Thermodynamics, we state the energy balance for the closed interior ballistic system at time t as

$$\text{initial energy of gases} = \text{internal energy of gases} + \text{losses}$$

where the loss term includes work done by and heat transferred from the system. In addition, we will assume the gaseous components always retain their identity and that they undergo no further reactions after being generated. Using average values of specific heats over the temperatures considered, we express this balance as

$$\sum_{i,j} m_{ij} c_{ui} T_{fij} + m_p c_p T_{f_p} = \left[\sum_{i,j} m_{ij} c_{ui} + m_p c_p \right] T_{\text{mean}} + L \quad (\text{A.01})$$

which we solve for mean temperature

$$T_{\text{mean}} = \frac{\sum_{i,j} m_{ij} c_{ui} T_{fij} + m_p c_p T_{f_p} - L}{\sum_{i,j} m_{ij} c_{ui} + m_p c_p} \quad (\text{A.02})$$

where the summations are taken over each surface j of every charge element i with the addition of a primer considered all burned at $t = 0$. From the definitions

$$\gamma \equiv c_p / c_u \quad (\text{A.03})$$

$$c_p - c_u = R \quad (\text{A.04})$$

$$F = RT_f \quad (\text{A.05})$$

it follows that

$$c_u = \frac{F}{(\gamma - 1)T_f} \quad (\text{A.06})$$

Substituting this result into (A.02) and simplifying our notation somewhat we get

$$T_{\text{mean}} = \frac{\sum_b \frac{F_b m_b}{\gamma_b - 1} + \frac{F_o m_o}{\gamma_o - 1} - L}{\sum_b \frac{F_b m_b}{(\gamma_b - 1) T_{f_b}} + \frac{F_o m_o}{(\gamma_o - 1) T_{f_o}}} \quad (\text{A.07})$$

which, in the limit, becomes

$$T_{\text{mean}} = \frac{\sum_b \int \frac{F_b}{\gamma_b - 1} dm_b + \frac{F_o m_o}{\gamma_o - 1} - L}{\sum_b \int \frac{F_b}{(\gamma_b - 1) T_{f_b}} dm_b + \frac{F_o m_o}{(\gamma_o - 1) T_{f_o}}} \quad (\text{A.08})$$

for differential weights burned, or

$$T_{\text{mean}}(t) = \frac{\sum_b \int \frac{F_b \dot{m}_b}{\gamma_b - 1} dt + \frac{F_o m_o}{\gamma_o - 1} - L(t)}{\sum_b \int \frac{F_b \dot{m}_b}{(\gamma_b - 1) T_{f_b}} dt + \frac{F_o m_o}{(\gamma_o - 1) T_{f_o}}} \quad (\text{A.09})$$

for instantaneous values of F , \dot{m} , γ , and T_f . The derivation of L is discussed in section III.D.

We assume Noble-Abel gases and mixtures, that is, a covolume correction applied to the ideal gas law so, at time t ,

$$P_{\text{mean}} \left[V_{f_{\text{res}}} - \sum_b m_b \eta_b - m_o \eta_o \right] = \left[\sum_b m_b R_b + m_o R_o \right] T_{\text{mean}} \quad (\text{A.10})$$

which, with the aid of (A.05), we solve for mean pressure,

$$P_{\text{mean}} = \frac{T_{\text{mean}} \left[\sum_b \frac{F_b m_b}{T_{f_b}} + \frac{F_o m_o}{T_{f_o}} \right]}{V_{f_{\text{res}}} - \sum_b m_b \eta_b - m_o \eta_o} \quad (\text{A.11})$$

which becomes

$$P_{\text{mean}} = \frac{T_{\text{mean}} \left[\sum_b \int \frac{F_b}{T_{f_b}} dm_b + \frac{F_o m_o}{T_{f_o}} \right]}{V_{f_{\text{res}}} - \sum_b \int \eta_b dm_b - \eta_o m_o} \quad (\text{A.12})$$

in the limit for differential weights burned. The free volume of the system is the volume behind the projectile less that occupied by unburned propellant, or

$$V_{free} = V_c + A_b [x_p + x_r] - \sum_i n_i V_i \quad (A.13)$$

so

$$P_{mean}(t) = \frac{T_{mean}(t) \left[\sum_h \int \frac{F_h \dot{m}_h}{T_{f_h}} dt + \frac{F_o m_o}{T_{f_o}} \right]}{V_c + A_b [x_p + x_r] - \sum_i n_i V_i - \sum_h \int \eta_h \dot{m}_h dt - \eta_o m_o} \quad (A.14)$$

for instantaneous values of x_p , x_r , η , F , \dot{m} , γ , and T_f . The gun coordinate system defining the displacements x_p and x_r is shown in Figure 6. How they are computed is taken up in section III.B.

The rate at which the weight of propellant i is converted into gas on its j th surface is given by

$$\dot{m}_{ij} = n_i \rho_{ij} S_{ij} r_{ij} \quad (A.15)$$

for instantaneous values of ρ and S where the burning rates are either tabulated experimental values or empirical functions of the form

$$r_{ij} = \beta_{ij} [P_{mean}]^{\alpha_{ij}} + \zeta_{ij} v_p \quad (A.16)$$

for known α , β , and ζ . The determination of the geometrical properties of individual propellant grains, V_i , S_{ij} , and n_i is taken up in section III.E.

B. Dynamic Relations

By Newton's Second Law, we express the acceleration of the projectile at any time t by

$$\text{projectile acceleration} = \frac{\text{net force on projectile}}{\text{projectile mass}}$$

where the propulsive force is supplied by the pressure of the propellant combustion gases on the base of the projectile and the retarding forces are provided by barrel resistance against the rotating band as well as air resistance against the nose as the air is compressed ahead of the projectile during its flight downtube. Hence we express projectile acceleration as

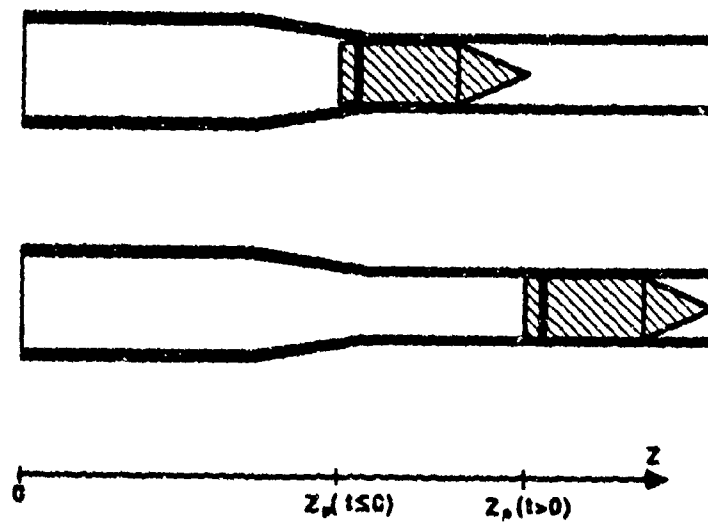


Figure 6. Gun Tube Reference Frame

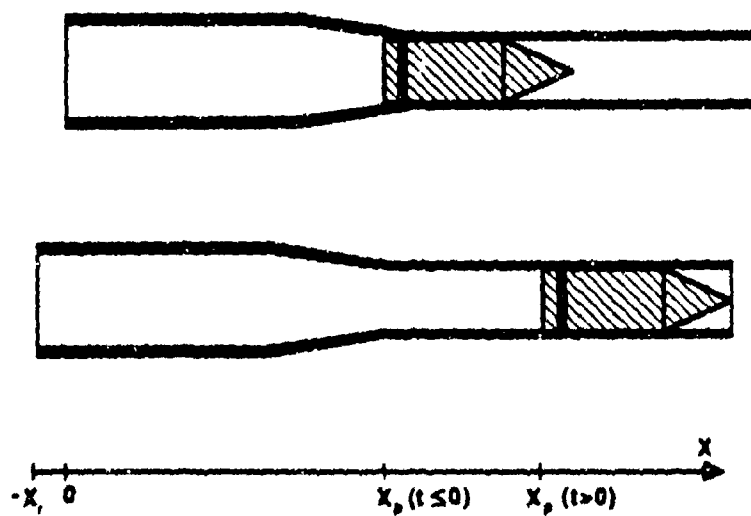


Figure 7. Ground Reference Frame

$$\ddot{x}_p = \frac{[P_{base} - P_{res} - P_{air}] A_b}{m_p/g} \quad (B.01)$$

for instantaneous values of P_{base} , P_{res} , and P_{air} . Similarly, the acceleration of the freely-recoiling barrel is

$$\ddot{x}_r = \frac{[P_{breach} - P_{res}] A_b}{m_r/g} \quad (B.02)$$

for instantaneous values of P_{breach} and P_{res} . One integration produces the ground-referenced projectile and recoil velocities \dot{x}_p and \dot{x}_r . A second integration yields the projectile and barrel displacements, x_p and x_r , measured from their respective initial positions. Calculations of breach and base pressure are taken up in section III.C. Resistance pressure due to engraving of the rotating band is interpolated from tabular resistance pressures as a function of the tube-referenced projectile displacement $x_p + x_r$.

C. Calculation of the Pressure Gradient

We will consider two ways of calculating the pressure gradient in the system from the breach to the projectile base. The first is the so-called Lagrange approximation with the added assumption that the introduction of recoil does not appreciably disturb the gradient so derived. The central assumptions of this model are that the entire charge may at any time be treated as gaseous—that is, all burned—and that the density of the gas is uniformly distributed along the gun tube at any given time. The derivation in a tube-based frame of reference is as follows ($z \equiv x_p + x_r$).

We use the one-dimensional, inviscid equations of continuity and momentum

$$0 = \frac{\partial \rho}{\partial t} + \frac{\partial}{\partial z}(\rho v), \quad 0 \leq z \leq z_p \quad (C.01)$$

$$-\frac{1}{\rho} \frac{\partial P}{\partial z} = \frac{\partial v}{\partial t} + v \frac{\partial v}{\partial z}, \quad 0 \leq z \leq z_p \quad (C.02)$$

together with the uniformity assumption

$$\frac{\partial \rho}{\partial z} = 0. \quad (C.03)$$

Then (C.01) and (C.03) imply

$$\frac{\partial v}{\partial z} = -\frac{1}{\rho} \frac{d\rho}{dt} \quad (C.04)$$

with the boundary conditions of

$$\begin{aligned} v(0, t) &= 0 \\ v(z_p, t) &= v_p \equiv \dot{z}_p \end{aligned} \quad (C.05)$$

where z_p and v_p denote position of the projectile base and projectile velocity, respectively. Integrating over z , produces the gas velocity distribution

$$v(z, t) = z \frac{\dot{z}_p(t)}{z_p(t)} \quad (C.06)$$

indicating a linear distribution from breech to base. Substituting (C.06) into (C.02) we find

$$-\frac{1}{\rho} \frac{\partial p}{\partial z} = z \frac{z_p \ddot{z}_p - \dot{z}_p \dot{z}_p}{z_p^2} + \left[z \frac{\dot{z}_p}{z_p} \right] \left[\frac{\dot{z}_p}{z_p} \right] \quad (C.07)$$

or

$$\frac{\partial p}{\partial z} = -\rho \frac{z}{z_p} \ddot{z}_p \quad (C.08)$$

Now the all-burnt assumption implies the (spatially uniform) density

$$\rho = \frac{\sum C_i / g}{A_b z_p} \quad (C.09)$$

Substituting both (C.09) and (B.01) rewritten in tube-based coordinates into (C.08), we find

$$\frac{\partial p}{\partial z} = -\frac{z}{z_p} \left[\frac{\sum C_i / g}{A_b z_p} \right] \frac{[P_{base} - P_{res} - P_{air}] A_b}{m_p / g} \quad (C.10)$$

so that

$$P(z, t) = \psi(t) - \frac{[P_{base} - P_{res} - P_{air}] \sum C_i}{2 m_p z_p^2} z^2 \quad (C.11)$$

The condition $P(0, t) = P_{breech}$ implies

$$\psi(t) = P_{breech} \quad (C.12)$$

so the requirement $P(z_p, t) = P_{base}$ forces

$$P_{breach} = P_{base} + \frac{1}{2} \frac{\sum C_i}{m_p} [P_{base} - P_{res} - P_{air}]. \quad (C.13)$$

Into the definition

$$P_{mean} = \frac{1}{z_p} \int_0^{z_p} P(z, t) dz \quad (C.14)$$

we substitute (C.11) and (C.12) and integrate, yielding

$$P_{mean} = P_{breach} - \frac{1}{6} \frac{\sum C_i}{m_p} [P_{base} - P_{res} - P_{air}]. \quad (C.15)$$

Then substituting for P_{breach} from (C.13) into (C.15) and rearranging, we find

$$P_{base} = \frac{3 P_{mean} + \frac{\sum C_i}{m_p} [P_{res} + P_{air}]}{3 + \frac{\sum C_i}{m_p}}. \quad (C.16)$$

Thus, according to the Lagrange model, knowledge of the charge-to-projectile weight ratio, the mean pressure, and the resistance pressures is sufficient to calculate the entire pressure gradient down the tube and, in particular, the desired base and breech pressures. Alternatively, the Pidduck-Kent gradient model may be employed.

The Pidduck-Kent model, as described by Corner[5], employs charge-to-mass ratio, Θ , specific heat ratio, γ , and space-mean pressure, P_{mean} , to estimate base and breech pressures in the ballistic gun system. The base pressure is scaled by the following:

$$\Theta \equiv \frac{\sum C_i}{m_p} \quad (C.17)$$

$$P_{base} = \frac{P_{mean}}{1 + \frac{\Theta}{\Delta}} \quad (C.18)$$

where Δ is the Pidduck-Kent constant. Breech pressure is related to the base pressure estimate. Let

$$p \equiv \frac{1}{\gamma - 1} \quad (C.19)$$

$$\frac{1}{a_0} \equiv \frac{2p+3}{\Delta} + 2 \frac{p+1}{\Theta}. \quad (C.20)$$

$$P_{\text{breach}} = P_{\text{base}} (1 - a_0)^{p+1}. \quad (\text{C.27})$$

The reader is encouraged to examine the classical derivation and its implicit assumptions for more information. The purpose here is to merely illustrate how IBHVG2 performs the calculations.

The Pidduck-Kent constant has been correlated with Θ and γ by a linear least squares fit described by Grollman and Baer[9]. No explanation was given for the formulation, but it is a fifth-order polynomial in charge-to-mass ratio and scaled with the specific heat ratio:

$$\Delta(\Theta) = 3 + a \Theta + b \Theta^2 + c \Theta^3 + d \Theta^4 + e \Theta^5 \quad (\text{C.21})$$

where

$$a = a_1 + \frac{a_2}{\gamma}, \quad b = b_1 + \frac{b_2}{\gamma}, \quad \dots, \quad e = e_1 + \frac{e_2}{\gamma}. \quad (\text{C.18})$$

Values for the fitted parameters ($a_1, a_2, b_1, b_2, \dots$) are given in the above reference. Not surprisingly with ten parameters, the regression error is quite small. The report states that the maximum error was 0.21% over the rectangular domain of $\gamma \in [1.2, 1.3]$ and $\Theta \in [0, 26]$. This is more than adequate for modeling considerations.

D. Work and Losses

The term $L(t)$ in (A.09) comprises the total work done by the interior ballistic system less the energy transferred from the system at time t . In IBHVG2, $L(t)$ includes contributions from: the translational kinetic energy of the projectile, the translational kinetic energy of the propellants and gases, the rotational kinetic energy of the projectile, the kinetic energy of the recoiling barrel, work done against barrel friction, work done against the resistance of the air in the tube opposing projectile motion, and heat lost to the gun tube. We neglect the amount of energy expended in the deformation of the gun barrel and any work done in overcoming the frictional resistance of the propellant bed or the combustion gases moving against the tube wall.

The translational kinetic energy of the projectile in a tube reference frame is

$$E_{\text{trans}} = \frac{1}{2} \frac{m_p}{g} \dot{z}_p^2. \quad (\text{D.01})$$

To find the translational energy of the propellants and gases, we first consider the Lagrange model developed in section C. In this case, all the propellant was assumed to be burned, an assumption which implies there is no work expended in moving any solid propellant, only work done moving gases. Alternatively, we may reinterpret the assumption as requiring the solid propellant remaining at any instant to have the same linear velocity profile as the gases and be distributed throughout the system so that the overall density is uniform.

Either view is consistent with the expression for energy in a differential volume of the system

$$dE_{prop} = \frac{1}{2} \rho v^2(z) dV, \quad 0 \leq z \leq z_p. \quad (D.02)$$

But the velocity at any point was found by (C.06), so

$$E_{prop} = \frac{1}{2} \rho A_b \int_0^{z_p} \left[z \frac{\dot{z}_p}{z_p} \right]^2 dz. \quad (D.03)$$

Integrating yields

$$E_{prop} = \frac{1}{6} \rho A_b z_p \dot{z}_p^2 \quad (D.04)$$

or, by substituting for ρ from (C.09) we have, with respect to the ground,

$$E_{prop} = \frac{1}{6} \frac{\sum C_i}{g} \dot{z}_p^2. \quad (D.05)$$

Similarly, it can be shown that for the Pidduck-Kent gradient model,

$$E_{prop} = \frac{1}{2} \frac{\sum \int \dot{m}_i dt + m_s}{\Delta g \dot{z}_p^2}. \quad (D.06)$$

The rotational kinetic energy of the projectile in a tube frame of reference is

$$E_{rot} = \frac{1}{2} I_p \omega_p^2 \quad (D.07)$$

where the moment of inertia of the projectile is taken to be that of a solid cylinder of bore diameter and uniform density, that is

$$I_p = \frac{1}{8} \frac{m_p}{g} D_b^2. \quad (D.08)$$

Because of varying weight distribution, sabot projectiles have a smaller I_p than this while artillery shells have a larger I_p , but the fraction of overall energy embodied in E_{rot} is so small that IBHVG2 currently assumes (D.08) for all projectiles. The twist for rifled barrels, τ , is commonly expressed as the number of "calibers" (barrel diameters) of downtube travel required for one complete revolution of the projectile. Thus, 2π radians are turned in τD_b inches of travel, so the definition

$$\theta_p = \omega_p t \quad (D.09)$$

implies

$$2\pi = \omega_p \left[\frac{\tau D_b}{\dot{z}_p} \right] \quad (D.10)$$

or, finally,

$$\omega_p(t) = \frac{2\pi \dot{z}_p}{\tau D_b}. \quad (D.11)$$

The translational energy of the recoiling barrel in a ground-based reference frame is

$$E_r = \frac{1}{2} \frac{m_r}{g} \dot{x}_r^2. \quad (D.12)$$

Currently, IBHVG2 requires tabular input of barrel frictional resistance pressure as a function of projectile displacement to compute the work done. These resistance profiles have been experimentally determined from measurements of force required to push projectiles through gun tubes or, perhaps more realistically, via instrumented projectiles used in actual firings which transmit data from onboard accelerometers and pressure gages. Given such tabular data, $P_{res}(z)$, the work required to overcome the frictional resistance of the gun tube is

$$E_{frict} = A_b \int_{x_p(0)}^{x_p} P_{res}(z) dz \quad (D.13)$$

where displacement is measured with respect to the barrel, or

$$E_{frict} = A_b \int [\dot{x}_p + \dot{x}_r] P_{res}(x_p + x_r) dt. \quad (D.14)$$

Similarly, the work done against air resistance is

$$E_{drag} = A_b \int \dot{z}_p P_{air} dt. \quad (D.15)$$

The last energy loss considered is that due to heat transfer to the gun barrel. The model employs a metal shell of thickness δ which is initially at temperature T_0 surrounding the interior ballistic system. As heat is transferred to the shell via convection from the combustion gases, it is assumed to come to thermal equilibrium instantaneously not only radially, but axially as the motion of the projectile exposes greater portions of the shell to heating. The rate of heat transfer is taken to be proportional to the difference between the mean temperature of the system, T_{mean} , and the average temperature of the shell, T_w , by Newton's Law of Cooling. That is,

$$E_{\text{heat}} = \int \dot{Q} dt \quad (\text{D.16})$$

with

$$\dot{Q} = A_w h [T_{\text{mean}} - T_w] \quad (\text{D.17})$$

where the wall area of the shell exposed to the system is that of the chamber plus that which has been exposed by the motion of the projectile, or

$$A_w = \left[\frac{V_o}{A_b} \right] \pi D_b + 2 A_b + \pi D_b [z_p + z_r] \quad (\text{D.18})$$

and the heat transfer coefficient

$$h = \lambda \bar{c}_p \bar{\rho} \bar{v} + h_n \quad (\text{D.19})$$

is that of Nordheim, Soodak, and Nordheim[8] with the addition of a natural convective term, h_n , to allow heat transfer in the absence of projectile motion. In the work cited, the authors selected a friction factor of

$$\lambda = \left[13.2 + 4 \log_{10} [2.54 D_b] \right]^{-2} \quad (\text{D.20})$$

based on studies with rifled and unrifled tubes. The mean gas velocity is

$$\bar{v} = \frac{1}{2} [\dot{z}_p + \dot{z}_r] \quad (\text{D.21})$$

from the linear gas velocity distribution in the Lagrange model (C.06). The mean gas density is the total weight of propellant burned divided by the volume of the system, or

$$\bar{\rho} = \frac{\sum_b \int \dot{m}_b dt + m_o}{V_o} \quad (\text{D.22})$$

Now (A.03) and (A.06) imply

$$c_p = \frac{F \gamma}{(\gamma - 1) T_f} \quad (\text{D.23})$$

so we take the charge-weight-burned weighted average

$$\bar{c}_p = \frac{\sum_k \int \frac{F_k \gamma_k \dot{m}_k}{(\gamma_k - 1) T_{fk}} dt + \frac{F_s \gamma_s m_s}{(\gamma_s - 1) T_{fs}}}{\sum_k \int \dot{m}_k dt + m_s} \quad (D.24)$$

At any instant, the heat already transferred to the shell is

$$Q + f E_{frict} = c_{ps} m_w [T_w - T_0] \quad (D.25)$$

or

$$Q + f F_{frict} = c_{ps} \rho_w A_w \delta [T_w - T_0] \quad (D.26)$$

where f is that fraction of work done against bore friction which pre-heats the shell. Knowledge of the heat capacity, density, and thickness of the shell permit calculation of the temperature of the shell

$$T_w = \frac{Q + f E_{frict}}{c_{ps} \rho_w A_w \delta} + T_0. \quad (D.27)$$

E. Propellant Grain Geometry

The calculation of instantaneous surface area and burning rates allows us to approximate burned propellant volume during the current time step at any point during deflagration. Thus the mass generation rate of propellant gases may be obtained for subsequent calculations of pressurization behind the projectile. (See Equation A.15)

Up to five different propellants may be described by as many \$PROP input decks. Each may have a different grain geometry, charge weight, burning rate characteristics, and other physical properties; each deck must be self-sufficient in describing its propellant. Later references use the parameter NTH to point to an individual deck (first propellant deck is NTH=1, etc.).

In IBHVG2, we include many of the conventional propellant grain geometries in the "form function" subroutines. These codes solve for current surface area (burned) volume for the different grain types shown in Table 1. Forms CORD, STAR, PF, SLOT, 7PF, 19PF, and MONO are all variations on a right circular cylinder. The special form functions (HEX, MONO, and GEN) will be described later in this section. Descriptions and drawings of the grain types are in Appendix B.

Table 1. Grain Types

cord	CORD
sphere	BALL or SPHR
slab	SLAB or RECT
pie-shaped	STAR or PIE
single-perf	1PF or 1P
slotted single-perf	SLOT
seven-perf	7PF or 7P
nineteen-perf cord	19PF or 19P
hexagonal	GHEX or HEX
nineteen-perf hexagonal	19HX or 19H
thirty-seven perf hex	37HX or 37H
monolithic n-perf	MONO
general undefined	GEN

Each geometry described to IBHVG2 requires a minimum of information: either absolute measurements, or one exact measurement and a combination of ratios to other surfaces. Incompatible measurements of perf diameters, grain diameter, and web distances will, in general, show up as a change in grain diameter. Using the geometry and density, we calculate a unit weight for one grain, then we find the number of grains for the charge by dividing the unit weight into the charge weight.

As an example, for a i^{th} propellant of cord-type grains, each of initial length l_i , density ρ_i , and initial diameter D_i , we compute the initial volume V_i and number of grains n_i by

$$V_i = \pi l_i \left(\frac{D_i}{2} \right)^2 \quad (\text{E.01})$$

and

$$n_i = \frac{C_i}{V_i \rho_i} \quad (\text{E.02})$$

Total initial surface area S_i as the sum of lateral and end areas is

$$S_i = \pi n_i \left[D_i l_i + 2 \left(\frac{D_i}{2} \right)^2 \right] \quad (E.03)$$

We assume all propellant burns in a direction perpendicular to the grain surface. During the current time step, a laminar layer is consumed which has total volume V_i^* approximated by

$$V_i^* = n_i S_i \epsilon_i, \quad (E.04)$$

where ϵ_i is the depth burned during the step. As long as the time increment is small and no gross change of grain geometry occurs during the step, then we may use V^* to calculate pressure increase. Each physical dimension affected by the loss of solid propellant is updated before the next time step, when surface and remaining volume are recalculated. For generality, we may define the lateral surfaces with a specific burning rate function, the end surfaces with a second burning rate, and a third function for any perforation surfaces.

If a major change occurs in the propellant geometry, as in this case when current grain diameter is D_i^* and

$$D_i^* \leq 2\epsilon_i, \quad (E.05)$$

then the grain has extinguished and all remaining volume has burned. IBHVG2 checks for this and similar cases on different grain types; the appropriate time step is decreased to find the exact time where geometry is flagged, and an output line is printed to notify the user.

All multiperforated grains develop fragments when depth burned reaches one-half web distance. The method of calculation differentiates between inner and outer slivers, as described in Reference [10].

HEX is a general form for right hexagonal grains. The geometry assumes at least one central perforation; additional perforations are described by a value for NRNG. NRNG=1 will provide a seven-perforated hexagonal grain; NRNG=2 will be a nineteen-perf hexagonal grain. The number of perforations possible is theoretically unlimited. Web distance is a required input; perforation diameter and grain length may be described directly or as ratios to given dimensions. Major diameter is computed from a combination of web distances and perforation diameters.

We attempt to generalize the right circular cylindrical grain for more than nineteen perforations: the type MONO. This is an experimental grain type currently under consideration. The idea is based on the catalytic monoliths currently found in automobile mufflers to reduce air pollution. It is hoped that recent advances in extrusion technology used to make the ceramic catalytic monoliths can be transferred to propellant manufacture. The concept is novel because the dimensions are on the order of the diameter of the gun tube. Conceptually, there is no difference in modeling this type of grain than a standard multi-perfed grain. The grain length, web distance, and diameters (perforation and grain) are required inputs. The routine will calculate the number of perforations consistent with the given dimensions.

We have a user-definable function, GEN, in the guise of two input arrays containing data pairs describing depth burned versus total surface area of propellant grains. This allows use of irregularly shaped grain forms as long as the user can describe the surface function. Test case 2 found in Appendix C demonstrates the use of a general form function approximating a 7-perf geometry.

Often real propellants are made in a series of layers. For example, an outer layer may consist of a thin, slow-burning layer applied over a fast-burning central propellant core. Each propellant geometry must have a core layer (designated as layer 4), and may have up to three more layers. The depth of the transitions between layers is order-dependent in the input deck description, with associated burning rates, densities, and other physical properties similarly defined. IBHVG2 keeps track of these layers during the deflagration process and signals to the user when each transition has been accomplished. Variation of density in grain layers affect grain weight so that for the i^{th} propellant having j distinct layers, Equation (E.02) becomes

$$m_i = \frac{C_i}{\sum_j V_{ij} \rho_{ij}} \quad (\text{E.06})$$

V. APPENDICES

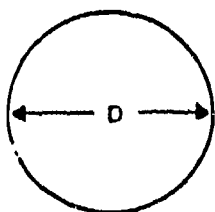
A. Nomenclature

Symbol	Definition	Units
α	exponent in burning-rate expression	<i>varies</i>
β	coefficient in burning-rate expression	<i>varies</i>
γ	specific heat ratio, c_p/c_v	—
δ	wall shell thickness	<i>in</i>
Δ	Pidduck-Kent constant	—
ϵ	distance burned into propellant	<i>in</i>
η	propellant covolume	in^3/lb_m
λ	friction factor	—
ω	rotational distance	<i>radians</i>
ρ	density	lb_m/in^3
r	gun tube rifling	<i>calibers / 2π</i>
θ	angle of rotation	<i>radians</i>
Θ	charge/projectile mass ratio	—
ζ	burning rate augmentation factor	—
a, b, c, d, e	Pidduck-Kent coefficients	—
c_p	specific heat at constant pressure	<i>in lb, lb_m⁻¹ °K⁻¹</i>
c_v	specific heat at constant volume	<i>in lb, lb_m⁻¹ °K⁻¹</i>
f	fraction of friction work converted to heating the tube	—
g	acceleration due to gravity	<i>in/sec²</i>
h	heat transfer coefficient	$\text{lb}_f \text{ft}^{-2} \text{°K}^{-1}$
l	length	<i>in</i>
m	charge weight	lb_m
n	number of propellant grains	—
p	Pidduck-Kent parameter	—
r	propellant regression rate	<i>in/sec</i>
t	time	<i>sec</i>
v	velocity	<i>in/sec</i>
x	travel coordinate, ground reference frame	<i>in</i>
z	travel coordinate, tube reference frame	<i>in</i>
A	area	in^2
C	unburnt propellant	lb_m
D	diameter	<i>in</i>
E	energy	<i>ft lb_f</i>

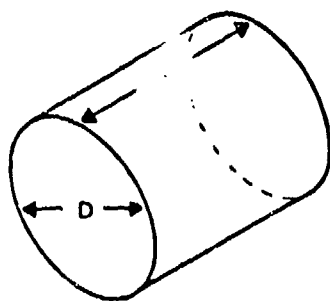
Symbol	Definition	Units
<i>F</i>	propellant "force"	$ft\ lb_f / lb_m$
<i>I</i>	moment of inertia	$lb_m\ in^2$
<i>L</i>	energy losses	$ft\ lb_f$
<i>P</i>	pressure	lb_f / in^2
<i>Q</i>	heat loss	$ft-lb_f$
<i>R</i>	universal gas constant	$ft\ lb_f\ mole^{-1}\ ^\circ K^{-1}$
<i>T</i>	temperature	$^\circ K$
<i>V</i>	volume	in^3

Subscript	Definition
<i>air</i>	property due to air in gun tube
<i>b</i>	bore
<i>base</i>	base of projectile
<i>breech</i>	breech of gun chamber
<i>c</i>	chamber
<i>drag</i>	resistance to motion
<i>f</i>	flame property
<i>free</i>	available space for propellant gases
<i>frict</i>	frictional property
<i>heat</i>	heat-induced property
<i>i</i>	propellant charge number
<i>j</i>	propellant grain surface
<i>k</i>	propellant type w.r.t. chemical/energetic properties
<i>mean</i>	averaged property
<i>p</i>	projectile
<i>prop</i>	propellant
<i>r</i>	recoil
<i>res</i>	frictional resistance
<i>rotat</i>	rotational property
<i>s</i>	primer property
<i>trans</i>	translational
<i>v</i>	free volume
<i>w</i>	wall property
ϕ	initial

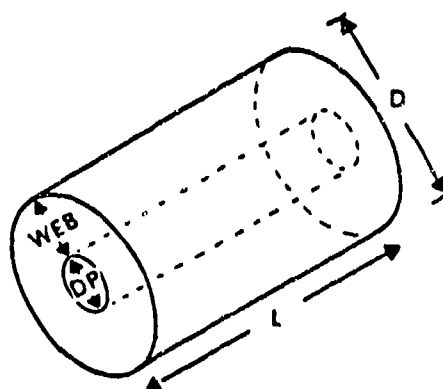
B. Propellant Grain Configurations



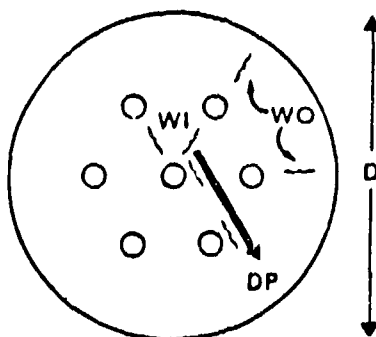
Ball



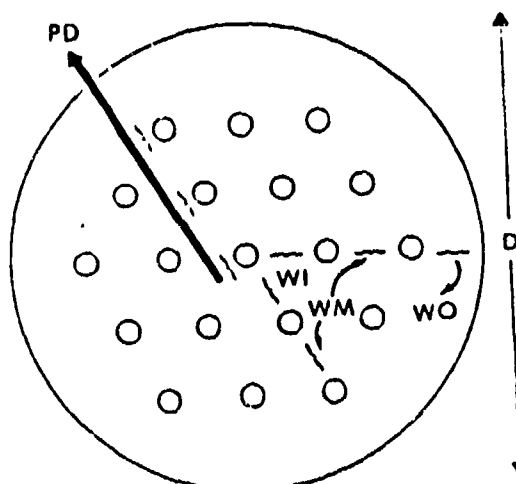
Cord



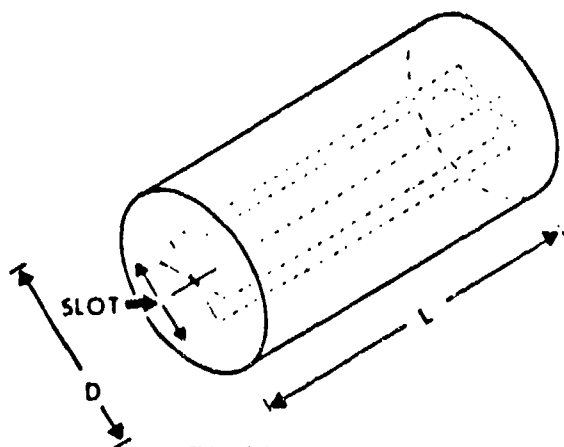
Single-Perf



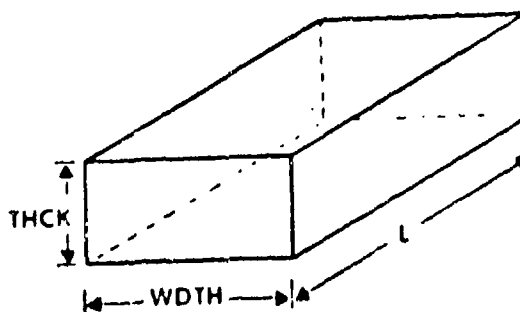
7-Perf



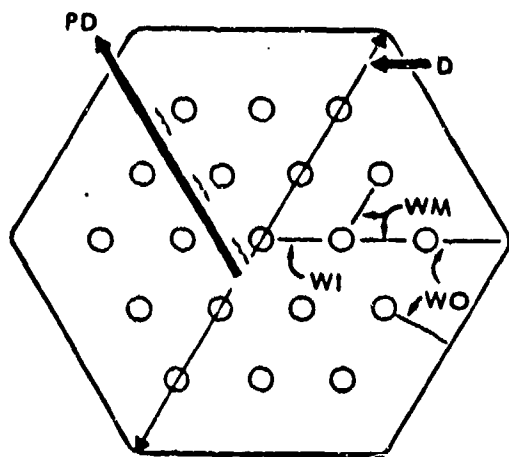
19-Perf



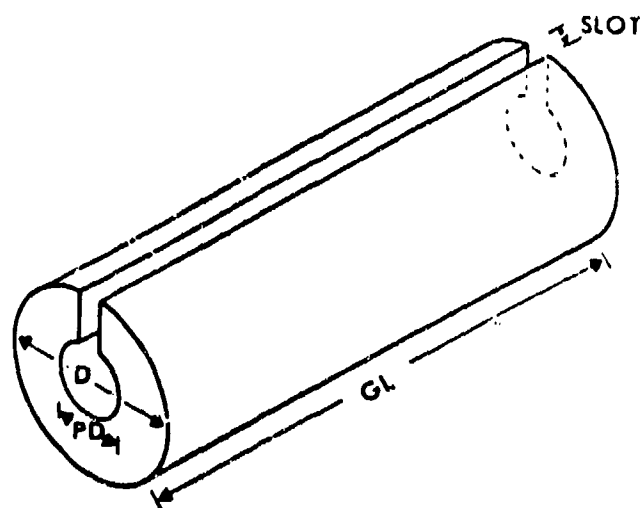
Pie (showing NSLT=3)



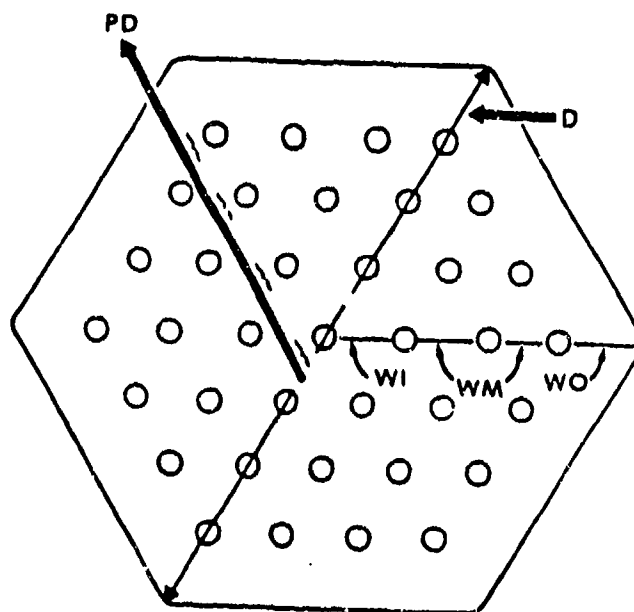
Strip (Rectangular)



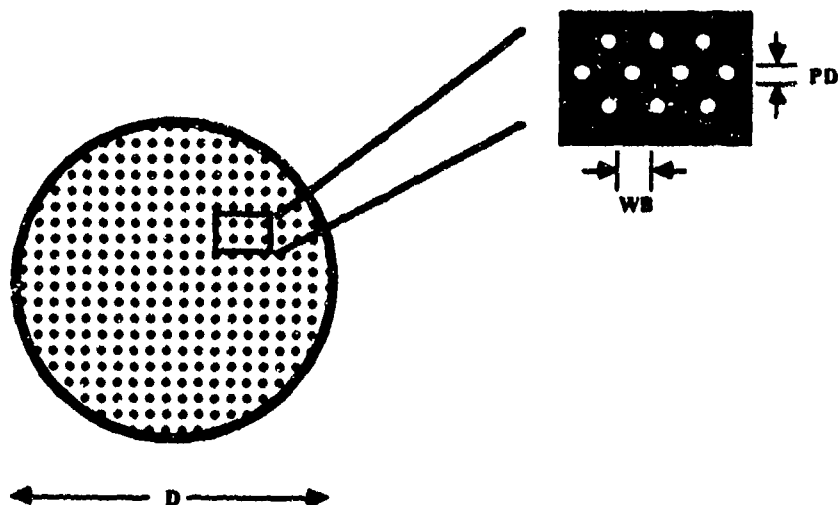
19-Perf, Hexagonal



Slotted Stick

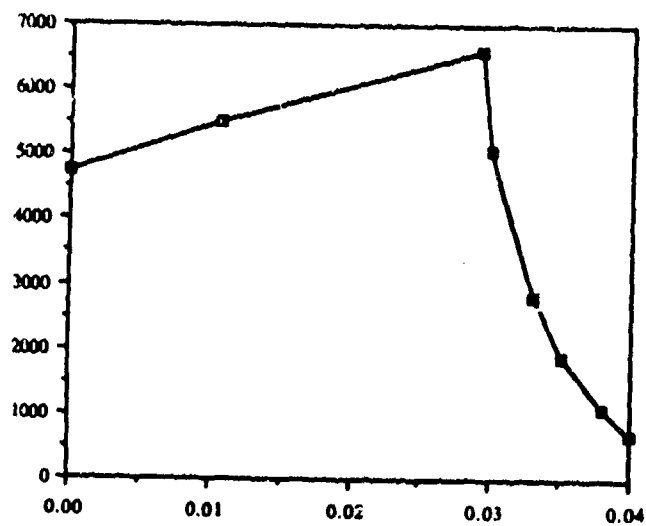


37-Perf, Hexagonal



Monolithic

Surface Function used in Test Case 2



Depth Burned

General

C. Installation

IBHVG2 (Version 400 and higher) has been re-designed for use with computers having no less than a 32-bit word length. Although the software may run on a shorter word-length machine, the precision of the output and ease of use will suffer greatly since the default tolerances require at least five significant digits. For example, the default pressure tolerance on a PMAX calculation is 1 psi, and normal pressure ranges are 10 kpsi and higher for most calculations. Therefore, a computer which does not have five decimal digit accuracy cannot reliably solve for pressure within default tolerance.

The first line of output from IBHVG2.400 is a CPU-dependent indicator of the attainable accuracy of a floating-point computation. The code computes the "machine epsilon" as commonly defined in numerical analysis. The pseudo-code shown below illustrates both the definition and the implementation.

```
i ← 0
repeat
  i ← i+1
  ε ← 2-i
until ( 1.0 ≥ 1.0 + ε )
```

The value of ϵ which terminates the loop is printed and saved in variable ERRTOL. It is typically on the order of 10^{-7} on 32-bit computers and 10^{-18} on 64-bit systems. ERRTOL is used for deciding when iterative solutions have converged to within the precision of a given machine.

IBHVG2.400 has been benchmarked and tested on computers using the FORTRAN66 and FORTRAN77 compilers. Some non-portable FORTRAN exists in the code and a description follows:

Main Program IBHVG

The PROGRAM statement is required to define I/O parameters in certain systems, while others only need to define the entry point. For the former, I/O devices are:

#	Unit Name	Description
5	NDEVI	Standard Input device
6	NDEVO	Standard Output device
7	NDEVS	When \$INFO deck option SOPT=1 or 2, this device saves output copy for user-supplied post-processing
9	NDEVT	Temporary character-manipulation device

All are formatted I/O devices, as opposed to unformatted binary files. NOTE: On many systems, more than one run may execute at any given time. Be sure that the separate runs do not overlap on I/O devices.

Subroutine CRKNUM

IBHVG2 writes characters, integers, and floating-point numbers to NDEVT and reads them back later for format conversion; CRKNUM handles the character-to-number conversion process. Since some operating systems use only upper-case alphabetic characters, and others may use lower-case letters, a provision has been made to interpret 'e' and 'd' as 'E' and 'D' during the conversion. Variables SMALLE and SMALLD should contain the lower-case letters. While transferring source code between systems, these characters often are converted to upper-case unintentionally.

Subroutine HELPPR

Array HOLD is used for run-time format development. Many FORTRAN77 compilers require that HOLD be declared as a CHARACTER array; FORTRAN66 does not recognize the CHARACTER statement.

Subroutine RDLIN

Reads input line and prints copy to standard output device. RDLIN must recognize the situation when end-of-input is reached. FORTRAN66 and FORTRAN77 use different end-of-file routines; use one of the given examples or re-write to suit the compiler.

Subroutine RUNDAT

Contains most of the machine-dependent coding, including a section which can be used to insert current date and time (if available from the CPU). Array DAYR holds the date; array TIMR holds the time. The original program opted for a 'DD-MMM-YY' and 'HH:MM:SS' format, but can be put in any format which will fit in the 12-character arrays. The arrays will be printed at the top of each page, along with the current run title. This feature has been commented out in the distribution deck in order to obtain maximum compiler flexibility. A section of interactive control statements concerning availability of input/output files has been added for IBM/PC-AT users.

When compiling, non-fatal warnings may occur in FORTRAN77 because non-character arrays are being filled with alphanumeric information. Ignore them if possible. After compilation, link the object code with standard FORTRAN libraries (including SIN, COS, MOD, SQRT, etc.).

D. Bugs

Sometimes, a particular calculation will not converge due to the integration algorithm. This has not been fully explored, but an eject mechanism has been installed in the KUTMER subroutine to indicate an error whenever ballistic time does not advance in twenty integration steps. A common action to relieve the thrashing is to change the integration step size (DT in the \$INFO deck). Because of this weakness in IBHVG2, one should monitor the calculations closely, observing that the solution is progressing, or one should use "time" cards or other time-limiting features of one's computer operating system to minimize endless computations. The integration routine is known to be suspect, and will be replaced in a future version.

IBHVG2 occasionally has serious problems with 37-perf propellant. The symptom is a sudden change in peak pressure and muzzle velocity with a tiny change in web dimension. It's almost as if, at the time of slivering, propellant gases come together to reform solid propellant. We are checking on this one; in the meantime, trust 37-perf simulations only after varying webs over a range around your final solution.

Due to the accuracy limitations of the integration routines, IBHVG2 will often seem to find successive pressure maximums and minimums when they do not co-exist in real situations. The overall maximums will be correctly reported in the end-of-trajectory summary. Extreme care must be taken if the user attempts to find values for the second (or later) pressure peaks (i.e., $NPMX > 1$ in the \$PMAX deck) since the numeric fluctuations will be treated as actual pressure peaks.

Some users have had trouble with using the \$FIND option. The problem can usually be traced to a poor initial guess to start off the optimization. The algorithm encoded is relatively weak and requires a better guess than perhaps more modern techniques. Therefore, we suggest that \$FIND be used with knowledge of its limitations and to apply some caution. It would not be unreasonable to perform a \$PARA iteration around the answer obtained with the \$FIND just to make sure. If the option converges correctly for your particular problem, it has proven to be quite useful in charge design.

E. Sample Input Decks and Outputs

Sample input decks follow. The corresponding outputs are among the files on the distribution media. These were run on a Perkin-Elmer 3252 (32-bit word) running AT&T UNIX System V, Release 2.0 and compiled using the 'f77' compiler. The calculations match closely with those of a CDC 7600 running NOS (64-bit word). Other machines checked were: DEC VAX/780 running VMS, IBM PC/AT running MSDOS with floating point, DEC VAX/780 running UNIX 4.2 BSD, and Cray X/MP-48 running COS (64-bit word).

Below is a table showing some execution times of the different inputs on some representative hardware. We are trying to give an approximate feel for performance on a mainframe computer, a minicomputer, and a microcomputer. As one can readily see, the most appropriate environment depends on what type of problem you are involved with. If the code was to estimate the behavior of a given input (few iterations), then the microcomputer will deliver the answer in a minute or two. On the other hand, complex optimization problems can require minutes of mainframe time.

Case	CPU Time (seconds)		
	Cray X/MP-48	VAX 780	IBM PC/AT
1	0.4	26.4	93
2	0.7	38.5	122
3	4.7	267.4	1054
4	2.8	115.9	868
5	14.9	526.7	4912
6	13.5	634.8	3895

One interesting quirk which might be noticed by the reader is that the ordering of the run times is not consistent among the different machines. For example, case 5 took less time to compute on the Cyber and the PC than case 6, while the order is reverse on the VAX. This is caused by the precision of the arithmetic with the intermediate results. The Cray has a 64-bit word at single-precision and the PC's floating point processor computes to 80 bits; the VAX is using only 32 bits of precision. We speculate that there are some convergence problems for these cases which are causing more difficulty for the VAX than the other two machines. Ideally, the integration routine should recognize this and compensate accordingly, but this remains a future project.

Test Case 1

This input deck represents a minimum IBHVG2 run. The two methods of commenting input decks are shown (\$COMM and after \$ on any input card). Note that all the primer in the \$PRIM deck is considered burnt at the start of calculation. A good practice for primer/igniter definition is to separate the igniter into two pieces so that a large amount of energetic material is not suddenly introduced into the gun chamber. One piece should be a \$PRIM deck including just enough to ignite the rest of the primer as a \$PROP deck. (Usually about 10 percent of the igniter in \$PRIM seems to work well.) Also notice that the second propellant geometry input does not include a main diameter since it is calculated in the form function subroutine. Blank lines and other white space between input deck sections allow easy readability, but are not necessary.

```
$COMM      IBHVG2 BENCHMARK TEST CASE 1
           HARP GUN WITH M30 PROP 7P

$INFO      POPT=1,1,1,0  $ ECHO INPUT LINES, PRINT TRAJECTORY + SUMMARY
           RUN='M30 7-PERF - LOT UNKNOWN'

$GUN       NAME='HARP GUN'
           CHAM=4378  GRVE=7.292  LAND=7.292  $ SMOOTH BORE
           TRAV=570.5  TWST=99

$COMMENT   PRIMER IS ASSUMED ALL BURNED AT TIME=0.0
           IGNITER CHARGE IS PROPELLANT 1
           MAIN CHARGE IS PROPELLANT 2

$PRIM      NAME='BLK POWDER'  CHWT=0.0154
           GAMA=1.25  FORC=96000  COV=30  TEMP=2000

$PROP      NAME='BLK POWDER'  CHWT=1.5  GRAN='CORD'
           LEN=0.198  DIAM=0.098  RHO=0.06
           GAMA=1.25  FORC=96000  COV=35  TEMP=2000
           ALPH=0.0  BETA=20

$PROP      NAME='M30 LOT UNKNOWN'  CHWT=55  GRAN='7PF'
           LEN=0.672  PD=0.026  WEB=0.0457  RHO=0.0607
           GAMA=1.2441  FORC=359876  COV=28.441  TEMP=3012
           NTBL=4  PR4L=6000,10000,12000,40000  BR4L=2.0,2.56,2.75,5.94

$COMMENT   NOMINAL PROJECTILE AND RESISTANCE PROFILE

$PROJ      NAME='PLASTIC LAB SABOT'  PRWT=52

$RESI      NPTS=4
           TRAV=0, 0.3, 3, 600
           PRES=100, 4000, 1800, 800

$END
```

Producing the following output:

ERRTOL= 4.768372E-07

```
CARD 1 --> $COMM
CARD 2 --> IBMVG2 BENCHMARK TEST CASE 1
CARD 3 -->
CARD 4 --> HARP GUN WITH M30 PROP 7P
CARD 5 -->
CARD 6 --> $INFO $ ECHO INPUT LINES, PRINT TRAJECTORY + SUMMARY
CARD 7 --> POPT=1,1,1,0
CARD 8 --> RUN='M30 7-PERF - LOT UNKNOWN'
CARD 9 -->
CARD 10 --> $GUN
CARD 11 --> NAME='HARP GUN'
CARD 12 --> CHAM=4378 GRVE=7.292 LAND=7.292 $ SMOOTH BORE
CARD 13 --> TRAV=570.5 TWST=99
CARD 14 -->
CARD 15 --> $COMMENT
CARD 16 --> PRIMER IS ASSUMED ALL BURNED AT TIME=0.0
CARD 17 --> IGNITER CHARGE IS PROPELLANT 1
CARD 18 --> MAIN CHARGE IS PROPELLANT 2
CARD 19 --> $PRIM
CARD 20 --> NAME='BLK POWDER' CHWT=.0154
CARD 21 --> GAMA=1.25 FORC=96000 COV=30 TEMP=2000
CARD 22 --> $PROP
CARD 23 --> NAME='BLK POWDER' CHWT=1.5 GRAM='COPD'
CARD 24 --> LEN=.198 DIAM=.098 RHO=0.06
CARD 25 --> GAMA=1.25 FORC=96000 COV=35 TEMP=2000
CARD 26 --> ALPH=0.0 BETA=20
CARD 27 --> $SPROP
CARD 28 --> NAME='M30 LOT UNKNOWN' CHWT=55 GRAM='7PF'
CARD 29 --> LEN=.672 FU=.026 WEB=.0457 RHO=0.0607
CARD 30 --> GAMA=1.2441 OPC=359876 COV=28.441 TEMP=3012
CARD 31 --> NTBL=4 PR4L=6000,10000,12000,40000 BR4L=2.0,2.56,2.75,5.94
CARD 32 -->
CARD 33 --> $COMMENT
CARD 34 --> NOMINAL PROJECTILE AND RESISTANCE PROFILE
CARD 35 --> $PROJ
CARD 36 --> NAME='PLASTIC LAB SABOT' PRWT=52
CARD 37 --> $RESI
CARD 38 --> NPYS=4
CARD 39 --> TRAV=0 .3 3 600
CARD 40 --> PRES=100, 4000, 1800, 800
CARD 41 --> $END
```

 - GUN TUBE -

 TYPE: MARP GUN
 GROOVE DIAMETER (IN): 7.292
 TWIST (CAL/S/TURN): 99.0
 SHELL THICKNESS (IN): 0.004000
 INITIAL SHELL TEMP (K): 293.

 - PROJECTILE -

 TYPE: PLASTIC LAB SABOT

 - RESISTANCE -

 AIR RESISTANCE OPTION: 1
 1 TRAVEL (IN) PRESSURE (PSI)
 1 0.00 100.
 2 0.30 4000.

 - GENERAL -

 MAX TIME STEP (S): 0.000100
 PRINT OPTIONS: 1 1 1 0 1 1
 GRADIENT MODEL: LAGRANGIAN

 - RECOIL -

 RECOIL OPTION: 0
 TYPE:

 - PRIMER -

 TYPE: BLK POWDER
 COVOLUME (IN3/LB): 30.000
 CHAMBER VOLUME (IN3): 4378.00
 LAND DIAMETER (IN): 7.292
 BORE AREA (IN2): 41.7622
 SHELL CP (IN-LB/LB-K): 1648.0
 AIR NO (IN-LB/IN2-S-K): 0.06480
 TRAVEL (IN): 570.50
 GROOVE/LAND RATIO (-): 0.000
 HEAT-LOSS OPTION: 1
 SHELL DENSITY (LB/IN3): 0.2840

 TOTAL WEIGHT (LB): 52.000
 WEIGHT PREDICTOR OPTION: 0

 WALL HEATING FRACTION: 0.000
 1 TRAVEL (IN) PRESSURE (PSI)
 3 3.00 1800.
 4 600.00 800.

 FRICTION TABLE LENGTH: 4
 1 TRAVEL (IN) PRESSURE (PSI)
 4 600.00 800.

 MAX RELATIVE ERROR (-): 0.00200
 CONSTANT-PRESSURE OPTION: 0

 RECOILING WEIGHT (LB): 0.

 FORCE (FT-LB/LB): 96000.
 WEIGHT (LB): 0.015400

- CHARGE 1 -

TYPE: BLK POWDER
EROSIVE COEFF (-):
GRAIN LENGTH (IN):

0.000000
0.19800
16739.
GRAINS:
CHARGE ICM CODE:
GRAIN DIAMETER (IN):
COND 0
0.09800
WEIGHT (LB):
CHARGE ICM AT (S):
1.5000
0.00000E+00

PROPERTIES AT LAYER BOUNDARIES OF		END SURFACES		PROPERTIES AT LAYER BOUNDARIES OF		LAT SURFACES	
1ST	2ND	3RD	4TH	1ST	2ND	3RD	4TH
---	---	---	---	---	---	---	---
---	---	---	0.00000	---	---	---	0.00000
---	---	---	100.000	---	---	---	100.000
---	---	---	0.06000	---	---	---	0.06000
---	---	---	1.2500	---	---	---	1.2500
---	---	---	96000.	---	---	---	96000.
---	---	---	35.000	---	---	---	35.000
---	---	---	2000.0	---	---	---	2000.0
---	---	---	0.0000	---	---	---	0.0000
---	---	---	20.0000000	---	---	---	20.0000000

AT DEPTH (IN):
ADJACENT LAYER WT %:
DENSITY (LB/IN3):
GAMMA (-):
FORCE (FT-LB/LB):
CONVOLUME (IN3/LB):
FLAME TEMP (K):
BURNING RATE EXPS:
BURNING RATE COEFFS:

----- CHARGE 2 -----

TYPE: 100 LOT UNKNOWN	GRAINS:	27128.	79F	HEIGHT (LB):	55.0000
EROSIVE COEFF (-):	CHARGE IGM CODE:		0	CHARGE IGM AT (S):	0.00000E+00
GRAIN LENGTH (IN):	GRAIN DIAMETER (IN):	0.67200	0.26080	PERF DIAMETER (IN):	0.02600
INNER WEB (IN):	OUTER WEB (IN):	0.06570	0.06570		

	PROPERTIES AT LAYER BOUNDARIES OF PERF SURFACES			PROPERTIES AT LAYER BOUNDARIES OF END SURFACES		
	1ST	2ND	3RD	1ST	2ND	4TH
AT DEPTH (IN):	---	---	---	---	---	---
ADJACENT LAYER UT %:	---	---	---	---	---	---
DENSITY (LB/IN3):	---	---	---	---	---	---
GAMMA (-):	---	---	---	---	---	---
FORCE (FT-LB/LB):	---	---	---	---	---	---
COVOLUME (IN3/LB):	---	---	---	---	---	---
FLAME TEMP (K):	---	---	---	---	---	---
MEAN PRESSURES (PSI):	---	---	---	---	---	---
MEAN PRESSURES (PSI):	---	---	---	---	---	---
MEAN PRESSURES (PSI):	---	---	---	---	---	---
BURNING RATES (IN/S):	---	---	---	---	---	---
BURNING RATES (IN/S):	---	---	---	---	---	---
BURNING RATES (IN/S):	---	---	---	---	---	---

	PROPERTIES AT LAYER BOUNDARIES OF LAT SURFACES		
	1ST	2ND	3RD
AT DEPTH (IN):	---	---	---
ADJACENT LAYER UT %:	---	---	---
DENSITY (LB/IN3):	---	---	---
GAMMA (-):	---	---	---
FORCE (FT-LB/LB):	---	---	---
COVOLUME (IN3/LB):	---	---	---
FLAME TEMP (K):	---	---	---
MEAN PRESSURES (PSI):	---	---	---
MEAN PRESSURES (PSI):	---	---	---
MEAN PRESSURES (PSI):	---	---	---
BURNING RATES (IN/S):	---	---	---
BURNING RATES (IN/S):	---	---	---
BURNING RATES (IN/S):	---	---	---

TIME (MS)	TRAV (IN)	VEL (FT/S)	ACC (G)	BREECH PRESS (PSI)	MEAN PRESS (PSI)	BASE PRESS (PSI)	MEAN TEMP (K)	FRAC BURN 1	FRAC BURN 2
0.000	0.00	0.	0.	5.	5.	5.	2000.	0.000	0.000
0.100	0.00	0.	0.	94.	94.	94.	2329.	0.099	0.001
0.106	0.00	0.	0.	100.	100.	100.	2337.	0.104	0.001
SHOT-START PRESSURE ACHIEVED									
0.200	0.00	0.	66.	227.	212.	182.	2432.	0.191	0.002
0.300	0.00	0.	147.	386.	353.	287.	2501.	0.277	0.003
0.400	0.00	1.	235.	567.	514.	408.	2554.	0.356	0.005
0.500	0.00	2.	327.	768.	694.	546.	2597.	0.431	0.007
0.600	0.01	3.	420.	986.	891.	702.	2634.	0.499	0.009
0.700	0.01	5.	511.	1221.	1106.	875.	2665.	0.562	0.012
0.800	0.02	6.	597.	1471.	1337.	1068.	2693.	0.620	0.015
0.900	0.03	8.	674.	1757.	1585.	1280.	2717.	0.673	0.018
1.000	0.04	11.	741.	2016.	1848.	1514.	2739.	0.720	0.021
1.100	0.1	13.	796.	2308.	2128.	1769.	2759.	0.764	0.025
1.200	0.1	16.	837.	2613.	2425.	2047.	2777.	0.803	0.029
1.300	0.09	19.	862.	2931.	2737.	2348.	2793.	0.838	0.033
1.400	0.11	21.	872.	3262.	3065.	2672.	2808.	0.868	0.037
1.500	0.14	24.	865.	3505.	3410.	3020.	2822.	0.895	0.042
1.600	0.17	27.	842.	3961.	3771.	3391.	2834.	0.919	0.047
1.700	0.21	30.	804.	4330.	4149.	3786.	2846.	0.938	0.052
1.800	0.24	32.	753.	4713.	4543.	4203.	2857.	0.955	0.058
1.900	0.28	34.	689.	5110.	4954.	4643.	2867.	0.969	0.064
2.000	0.33	37.	627.	5569.	5383.	5009.	2876.	0.980	0.070
2.100	0.37	40.	1112.	6079.	5828.	5327.	2884.	0.988	0.076
2.200	0.42	44.	1409.	6610.	6292.	5656.	2892.	0.994	0.082
2.300	0.48	49.	1719.	7160.	6773.	5997.	2899.	0.998	0.089
2.400	0.54	55.	2043.	7732.	7271.	6350.	2906.	1.000	0.096
2.450	0.57	58.	2211.	8026.	7527.	6530.	2909.	1.000	0.100
PROPELLANT 1 BURNED OUT									
2.500	0.61	62.	2382.	8325.	7788.	6714.	2911.	1.000	0.103
2.600	0.69	70.	2735.	8940.	8323.	7990.	2917.	1.000	0.111
2.700	0.78	80.	3105.	9578.	8877.	7477.	2922.	1.000	0.119
2.800	0.88	90.	3491.	10237.	9450.	7875.	2926.	1.000	0.127
2.900	1.00	102.	3895.	10919.	10041.	8284.	2929.	1.000	0.135
3.000	1.13	115.	4315.	11621.	10648.	8701.	2932.	1.000	0.144
3.100	1.27	130.	4752.	12340.	11268.	9125.	2935.	1.000	0.153
3.200	1.44	146.	5205.	13076.	11902.	9555.	2937.	1.000	0.162
3.300	1.63	164.	5677.	13833.	12552.	9991.	2939.	1.000	0.172
3.400	1.83	183.	6172.	14615.	13223.	10439.	2940.	1.000	0.181
3.500	2.07	203.	6690.	15423.	13914.	10896.	2941.	1.000	0.192
3.600	2.32	226.	7233.	16257.	14626.	11363.	2941.	1.000	0.202
3.700	2.61	250.	7801.	17116.	15356.	11838.	2941.	1.000	0.213
3.800	2.92	276.	8394.	17999.	16106.	12319.	2941.	1.000	0.225
3.900	3.27	304.	8882.	18876.	16873.	12866.	2940.	1.000	0.236
4.000	3.65	333.	9344.	19763.	17656.	13441.	2939.	1.000	0.249
4.100	4.07	364.	9815.	20658.	18454.	14027.	2938.	1.000	0.261
4.200	4.53	396.	10294.	21589.	19267.	14624.	2936.	1.000	0.274
4.300	5.02	430.	10780.	22523.	20092.	15229.	2934.	1.000	0.288
4.400	5.56	466.	11273.	23471.	20928.	15843.	2931.	1.000	0.302
4.500	6.14	503.	11771.	24428.	21773.	16463.	2928.	1.000	0.316
4.600	6.77	542.	12274.	25394.	22626.	17089.	2925.	1.000	0.331
4.700	7.44	582.	12779.	26366.	23483.	17719.	2921.	1.000	0.346
4.800	8.17	624.	13287.	27341.	24344.	18351.	2917.	1.000	0.362
4.900	8.94	668.	13795.	28318.	25207.	18984.	2912.	1.000	0.378
5.000	9.77	713.	14302.	29293.	26047.	19616.	2907.	1.000	0.395

TIME (MS)	TRAV (IN)	VEL. (FT/S)	ACC (G)	BREECH PRESS (PSI)	MEAN PRESS (PSI)	BASE PRESS (PSI)	MEAN TEMP (K)	FRAC BURN 1	FRAC BURN 2
5.100	10.65	760.	14808.	30264.	26925.	20245.	2902.	1.000	0.412
5.200	11.59	808.	15309.	31229.	27776.	20870.	2897.	1.000	0.429
5.300	12.59	858.	15806.	32184.	28619.	21489.	2891.	1.000	0.447
5.400	13.65	910.	16296.	33126.	29450.	22099.	2885.	1.000	0.466
5.500	14.78	963.	16779.	34053.	30269.	22700.	2879.	1.000	0.485
5.600	15.97	1018.	17252.	34963.	31072.	23290.	2872.	1.000	0.504
5.700	17.22	1074.	17714.	35852.	31857.	23866.	2865.	1.000	0.524
5.800	18.55	1132.	18164.	36718.	32621.	24427.	2858.	1.000	0.544
5.900	19.94	1191.	18601.	37558.	33363.	24972.	2851.	1.000	0.565
6.000	21.41	1252.	19024.	38371.	34080.	25499.	2843.	1.000	0.586
6.100	22.94	1314.	19431.	39154.	34771.	26006.	2836.	1.000	0.607
6.200	24.56	1377.	19821.	39905.	35434.	26493.	2828.	1.000	0.629
6.300	26.25	1441.	20194.	40622.	36067.	26958.	2820.	1.000	0.652
6.400	28.02	1507.	20548.	41303.	36669.	27400.	2812.	1.000	0.674
6.500	29.87	1574.	20883.	41948.	37238.	27818.	2803.	1.000	0.698
6.600	31.80	1641.	21198.	42555.	37774.	28211.	2795.	1.000	0.721
6.700	33.81	1710.	21493.	43123.	38275.	28580.	2786.	1.000	0.745
6.800	35.90	1780.	21767.	43651.	38741.	28922.	2778.	1.000	0.769
6.900	38.08	1850.	22020.	44139.	39172.	29239.	2769.	1.000	0.794
7.000	40.34	1922.	22252.	44586.	39567.	29529.	2761.	1.000	0.819
7.100	42.69	1994.	22463.	44992.	39926.	29793.	2752.	1.000	0.844
7.191	44.89	2059.	22539.	45141.	40057.	29890.	2743.	1.000	0.864
LOCAL PRESSURE MAX DETECTED									
7.191	44.89	2059.	22539.	45141.	40057.	29890.	2743.	1.000	0.864
LOCAL PRESSURE MIN DETECTED									
7.200	45.13	2066.	22539.	45140.	4005	29889.	2742.	1.000	0.866
LOCAL PRESSURE MAX DETECTED									
7.300	47.65	2139.	22465.	45001.	39934.	29800.	2731.	1.000	0.884
7.400	50.26	2211.	22298.	44680.	39651.	29593.	2720.	1.000	0.900
7.500	52.95	2282.	22058.	44221.	39246.	29296.	2708.	1.000	0.913
7.600	55.74	2353.	21759.	43649.	38742.	28926.	2695.	1.000	0.926
7.700	58.60	2422.	21413.	42986.	38156.	28497.	2682.	1.000	0.936
7.800	61.55	2491.	21028.	42247.	37504.	28019.	2669.	1.000	0.945
7.900	64.58	2558.	20611.	41447.	36798.	27501.	2655.	1.000	0.954
8.000	67.69	2623.	20166.	40597.	36048.	26951.	2641.	1.000	0.960
8.100	70.87	2687.	19706.	39710.	35265.	26376.	2627.	1.000	0.966
8.200	74.14	2750.	19234.	38805.	34467.	25790.	2613.	1.000	0.972
8.300	77.47	2811.	18759.	37893.	33662.	25200.	2599.	1.000	0.976
8.400	80.88	2871.	18283.	36979.	32856.	24608.	2585.	1.000	0.980
8.500	84.36	2929.	17808.	36067.	32051.	24018.	2571.	1.000	0.984
8.600	87.91	2986.	17337.	35161.	31251.	23430.	2557.	1.000	0.987
8.700	91.53	3041.	16869.	34263.	30458.	22849.	2542.	1.000	0.990
8.800	95.21	3094.	16407.	33375.	29675.	22274.	2528.	1.000	0.992
8.900	98.95	3146.	15952.	32501.	28903.	21707.	2514.	1.000	0.994
9.000	102.76	3197.	15505.	31641.	28144.	21150.	2500.	1.000	0.996
9.100	106.63	3246.	15065.	30796.	27398.	20603.	2486.	1.000	0.997
9.200	110.55	3294.	14635.	29969.	26668.	20066.	2472.	1.000	0.998
9.300	114.53	3341.	14215.	29160.	25954.	19542.	2458.	1.000	0.999
9.400	118.57	3386.	13804.	28369.	25256.	19029.	2444.	1.000	1.000
9.500	122.66	3429.	13403.	27598.	24575.	18529.	2430.	1.000	1.000
9.537	124.18	3445.	13257.	27317.	24327.	18347.	2425.	1.000	1.000
PROPELLANT 2 BURNED OUT									
9.600	126.79	3472.	13013.	26848.	23913.	18042.	2417.	1.000	1.000
9.700	130.99	3513.	12637.	26124.	23273.	17573.	2403.	1.000	1.000
9.800	135.23	3553.	12275.	25426.	22657.	17120.	2390.	1.000	1.000

TIME (MS)	TRAV (IN)	VEL (FT/S)	ACC (G)	BRECH PRESS (PSI)	MEAN PRESS (PSI)	BASE PRESS (PSI)	MEAN TEMP (K)	FRAC BURN 1	FRAC BURN 2
9.900	139.51	3592.	11926.	24753.	22063.	16683.	2377.	1.000	1.000
10.000	143.85	3630.	11589.	24104.	21490.	16263.	2364.	1.000	1.000
10.100	148.23	3667.	11265.	23479.	20938.	15857.	2351.	1.000	1.000
10.200	152.65	3703.	10952.	22876.	20406.	15465.	2339.	1.000	1.000
10.300	157.11	3737.	10651.	22294.	19892.	15087.	2326.	1.000	1.000
10.400	161.62	3771.	10361.	21733.	19397.	14723.	2314.	1.000	1.000
10.500	166.16	3804.	10081.	21192.	18919.	14372.	2302.	1.000	1.000
10.600	170.75	3836.	9811.	20670.	18458.	14032.	2291.	1.000	1.000
10.700	175.37	3867.	9550.	20167.	18013.	13705.	2279.	1.000	1.000
10.800	180.03	3898.	9299.	19680.	17583.	13389.	2267.	1.000	1.000
10.900	184.72	3927.	9056.	19211.	17168.	13083.	2256.	1.000	1.000
11.000	189.45	3956.	8822.	18757.	16768.	12788.	2245.	1.000	1.000
11.100	194.22	3984.	8596.	18320.	16381.	12503.	2234.	1.000	1.000
11.200	199.02	4011.	8378.	17897.	16007.	12228.	2223.	1.000	1.000
11.300	203.85	4038.	8167.	17488.	15646.	11961.	2213.	1.000	1.000
11.400	208.71	4064.	7964.	17093.	15296.	11704.	2202.	1.000	1.000
11.500	213.60	4089.	7767.	16710.	14959.	11455.	2192.	1.000	1.000
11.600	218.52	4114.	7577.	16341.	14632.	11214.	2182.	1.000	1.000
11.700	223.47	4138.	7394.	15984.	14316.	10981.	2172.	1.000	1.000
11.800	228.45	4162.	7216.	15638.	14010.	10755.	2162.	1.000	1.000
11.900	233.46	4185.	7044.	15303.	13714.	10536.	2152.	1.000	1.000
12.000	238.50	4207.	6878.	14979.	13428.	10325.	2143.	1.000	1.000
12.100	243.56	4229.	6717.	14665.	13150.	10120.	2133.	1.000	1.000
12.200	248.64	4250.	6562.	14361.	12881.	9921.	2124.	1.000	1.000
12.300	253.76	4271.	6411.	14067.	12621.	9728.	2115.	1.000	1.000
12.400	258.90	4292.	6266.	13781.	12368.	9542.	2106.	1.000	1.000
12.500	264.06	4312.	6124.	13504.	12123.	9360.	2097.	1.000	1.000
12.600	269.24	4331.	5988.	13236.	11886.	9185.	2088.	1.000	1.000
12.700	274.45	4350.	5855.	12976.	11655.	9014.	2080.	1.000	1.000
12.800	279.68	4369.	5727.	12724.	11432.	8849.	2071.	1.000	1.000
12.900	284.94	4387.	5602.	12479.	11215.	8688.	2063.	1.000	1.000
13.000	290.21	4405.	5482.	12241.	11004.	8532.	2054.	1.000	1.000
13.100	295.51	4422.	5365.	12010.	10800.	8380.	2046.	1.000	1.000
13.200	300.83	4439.	5251.	11786.	10601.	8233.	2038.	1.000	1.000
13.300	306.16	4456.	5141.	11568.	10408.	8090.	2030.	1.000	1.000
13.400	311.52	4473.	5034.	11356.	10221.	7950.	2022.	1.000	1.000
13.500	316.90	4489.	4930.	11151.	10039.	7815.	2014.	1.000	1.000
13.600	322.29	4504.	4829.	10951.	9862.	7683.	2007.	1.000	1.000
13.700	327.71	4520.	4732.	10756.	9689.	7555.	1999.	1.000	1.000
13.800	333.14	4535.	4637.	10567.	9522.	7430.	1992.	1.000	1.000
13.900	338.59	4550.	4544.	10384.	9359.	7309.	1984.	1.000	1.000
14.000	344.06	4564.	4455.	10205.	9200.	7190.	1977.	1.000	1.000
14.100	349.54	4578.	4368.	10030.	9045.	7075.	1970.	1.000	1.000
14.200	355.05	4592.	4283.	9861.	8895.	6963.	1963.	1.000	1.000
14.300	360.57	4606.	4201.	9696.	8748.	6854.	1956.	1.000	1.000
14.400	366.10	4619.	4120.	9535.	8606.	6747.	1949.	1.000	1.000
14.500	371.65	4632.	4043.	9378.	8467.	6643.	1942.	1.000	1.000
14.600	377.22	4645.	3967.	9226.	8331.	6542.	1935.	1.000	1.000
14.700	382.80	4658.	3893.	9077.	8199.	6443.	1928.	1.000	1.000
14.800	388.40	4670.	3822.	8932.	8070.	6347.	1922.	1.000	1.000
14.900	394.01	4683.	3752.	8791.	7945.	6252.	1915.	1.000	1.000
15.000	399.64	4695.	3684.	8653.	7822.	6161.	1909.	1.000	1.000
15.100	405.28	4706.	3618.	8519.	7703.	6071.	1902.	1.000	1.000
15.200	410.93	4718.	3553.	8388.	7586.	5983.	1896.	1.000	1.000
15.300	416.60	4729.	3491.	8260.	7472.	5898.	1890.	1.000	1.000

TIME (MS)	TRAV (IN)	VEL (FT/S)	ACC (G)	BREECH PRESS (PSI)	MEAN PRESS (PSI)	BASE PRESS (PSI)	MEAN TEMP (K)	FRAC BURN 1	FRAC BURN 2
15.400	422.28	4740.	3430.	8135.	7361.	5814.	1884.	1.000	1.000
15.500	427.97	4751.	3370.	8013.	7253.	5733.	1877.	1.000	1.000
15.600	433.68	4762.	3312.	7894.	7147.	5653.	1871.	1.000	1.000
15.700	439.40	4773.	3256.	7778.	7044.	5575.	1865.	1.000	1.000
15.800	445.14	4783.	3201.	7664.	6943.	5499.	1860.	1.000	1.000
15.900	450.88	4793.	3147.	7554.	6844.	5424.	1854.	1.000	1.000
16.000	456.64	4803.	3095.	7445.	6747.	5351.	1848.	1.000	1.000
16.100	462.41	4813.	3044.	7340.	6653.	5280.	1842.	1.000	1.000
16.200	468.19	4823.	2994.	7236.	6561.	5210.	1837.	1.000	1.000
16.300	473.98	4832.	2946.	7135.	6471.	5142.	1831.	1.000	1.000
16.400	479.79	4842.	2898.	7036.	6382.	5075.	1825.	1.000	1.000
16.500	485.60	4851.	2852.	6940.	6296.	5010.	1820.	1.000	1.000
16.600	491.43	4860.	2807.	6845.	6212.	4946.	1815.	1.000	1.000
16.700	497.27	4869.	2763.	6753.	6129.	4883.	1809.	1.000	1.000
16.800	503.12	4878.	2720.	6662.	6048.	4821.	1804.	1.000	1.000
16.900	508.98	4887.	2679.	6574.	5969.	4761.	1799.	1.000	1.000
17.000	514.85	4895.	2638.	6487.	5892.	4702.	1793.	1.000	1.000
17.100	520.72	4904.	2598.	6402.	5816.	4644.	1788.	1.000	1.000
17.200	526.61	4912.	2559.	6319.	5742.	4587.	1783.	1.000	1.000
17.300	532.51	4920.	2521.	6238.	5669.	4532.	1778.	1.000	1.000
17.400	538.42	4928.	2484.	6158.	5598.	4477.	1773.	1.000	1.000
17.500	544.34	4936.	2448.	6080.	5528.	4424.	1768.	1.000	1.000
17.600	550.27	4944.	2413.	6004.	5460.	4371.	1763.	1.000	1.000
17.700	556.21	4952.	2378.	5929.	5393.	4320.	1758.	1.000	1.000
17.800	562.15	4959.	2344.	5856.	5327.	4270.	1753.	1.000	1.000
17.900	568.11	4967.	2311.	5784.	5263.	4220.	1749.	1.000	1.000
17.960	570.50	4970.	2298.	5756.	5237.	4200.	1747.	1.000	1.000
PROJECTILE EXIT									

CONDITIONS AT:	PMAX	MUZZLE
TIME (MS):	7.191	17.940
TRAVEL (IN):	44.89	570.50
VELOCITY (FT/S):	2059.	4970.
ACCELERATION (G):	22539.	2248.
BREECH PRESS (PSI):	45141.	5756.
MEAN PRESS (PSI):	40057.	5237.
BASE PRESS (PSI):	29890.	4200.
MEAN TEM° (K):	2743.	1747.
Z CHARGE 1 (-):	1.000	1.000
Z CHARGE 2 (-):	0.864	1.000

ENERGY BALANCE SUMMARY	IN-LB	%
TOTAL CHEMICAL:	979802624.	100.00
(1) INTERNAL GAS:	570262272.	58.20
(2) WORK AND LOSSES:	409540352.	41.80
(A) PROJECTILE KINETIC:	239312960.	24.42
(B) GAS KINETIC:	86697888.	8.85
(C) PROJECTILE ROTATIONAL:	120494.	0.01
(D) FRICTIONAL WORK TO TUBE:	0.	0.00
(E) OTHER FRICTIONAL WORK:	31748304.	3.24
(F) WORK DONE AGAINST AIR:	8165177.	0.83
(G) HEAT CONVECTED TO BORE:	43515312.	4.44
(H) RECOIL ENERGY:	0.	0.00
LOADING DENSITY (G/CM3):	0.357	
CHARGE WT/PROJECTILE WT:	1.087	
PIEZOMETRIC EFFICIENCY:	0.223	
EXPANSION RATIO:	6.442	

Test Case 2

This case demonstrates how to include two successive, but independent, runs as a single input file. The input descriptions do not overlap because the program will reset all parameters after an \$END card unless specifically told not to do so. The main propellant in the first sub-case is divided into three layers: outer layer (2) is a deterred propellant with a low burning rate, middle layer (3) is a thin transition zone, and the inner layer (4) is a fast-burning propellant. The transition zone is used to avoid an abrupt change in burning rates. Though all surfaces (lateral, end, and perforation) are defined for layers 2 and 3, the core layer has its end and perforation parameters overridden by the lateral inputs. Gun chamber length is defined as 5 inches, and pressure gages are specified at the breech end (position at -5.0 inches with respect to the base of projectile) and at the projectile end (position 0.0 inches) of the chamber. The default equations for finding internal pressures are Lagrangian, but Pidduck-Kent is used in this case.

The second data set also uses the Pidduck-Kent gradient to solve for internal pressures. A prominent feature here is the form function 'GEN' instead of the standard '7PF' granulation. The data for the depth-burned versus surface array came from a similar run where DB-P and SRF(2) were printed as part of the trajectory information. (See input descriptions for \$TDIS, \$TRAJ, and \$INFO decks.) Again, the igniter has been split into two parts with a small portion as \$PRIM and the rest as the first \$PROP deck. Blank lines and liberal indents allow easy readability, but are not necessary.

\$COMMENT

18HVG2 BENCHMARK TEST CASE 2

TWO INDEPENDENT DATA SETS IN ONE 18HVG2 RUN

FIRST SET : Laterally Deterred Propellant

(VERY THIN TRANSITION ZONE BETWEEN OUTER AND INNER
PROPELLANT TYPES, RESULTING IN THREE LAYERS)

- 1 - DETERRENT, .0007 THICK, LOW B/R EXPONENT
- 2 - TRANSITION ZONE, .0001 THICK, FROM LOW TO HI EXP
- 3 - CORE PROPELLANT, HI BURNING RATE

SECOND SET : STANDARD 105MM CANNON

PIDDUCK-KENT INTERNAL PRESSURE GRADIENT EQUATION
USE GENERAL GRAIN FORM F/ANCTION

\$HEAT

TSHL = 0.00450 CSHL = 1848 RSHL = 0.284
TVAL = 293 NO = 0.0648 NL = 1

\$GUN

NAME='XM881 25MM APFSDS-T' CHAM=5.86 GRVE=0.988 LAND=0.980
G/L=1. TRAV=74 TWST=25
CLEN=5 NGAG=2 GLOC=-5.0

\$PROJ

NAME = 'APFSDS-T' PRWT = 0.170

\$RESI

NPTS = 4 AIR = 1
TRAV = 0, 0.2, 1.0, 74
PRES = 200, 2000, 400, 400

\$INFO

RUN = '120MATCH-182H881' DELT = SE-5 DELP = SE-5
GRAD = 2 POPT = 1,1,1,0,2 SOPT = 0
EPS = 0.002 COMP = 0

SRECO
 NAME = 'NONE' RECO = 0 RCWT = 0
 SPRIM
 NAME='H/KNO3' CHWT=0.00022
 GAMA = 1.25 FORC = 212500
 COV = 30 TEMP = 2000
 SPROP
 NAME='H10 7P' CHWT=0.2071 GRAN='7PF'
 RHO=0.06 GAMA=1.2385 FORC=330000
 COV=27.04 TEMP=3073 EROS=0
 NTBL=-1
 PR2P=100000 PR2E=100000 PR2L=100000
 PR3P=100000 PR3E=100000 PR3L=100000
 PR4L=100000
 CF2P=0.00289 CF2E=0.00289 CF2L=0.00289
 EX2P=0.678 EX2E=0.678 EX2L=0.678
 CF3P=0.00289 CF3E=0.00289 CF3L=0.00289
 EX3P=0.678 EX3E=0.678 EX3L=0.678
 CF4L=0.004656 EX4L=0.7061
 DEPP=0.0007,0.0008 DEPE=0.0007,0.0008 DEPL=0.0007,0.0008
 LEN=0.0972 DIAM=0.0928 PD=0.0058
 WI=0.0175 WO=0.0202

SEND

SNEAT
 TSHL = 0.00450 CSHL = 1848 RSHL = 0.284
 TVAL = 293 NO = 0.0648 HL = 1

SGLH
 NAME = '105-MM GUN M68' CHAM = 375 GRVE = 4.224
 LAND = 4.134 G/L = 2. TRAV = 187
 TWST = 99

SPROJ
 NAME = 'M456A2' PRUT = 23.2

SRESI
 NPTS = 4 AIR = 1
 TRAV = 0, 0.5, 8.0, 187
 PRES = 100, 2100, 500, 200

SINFO
 RUN = '105MATCH-1105' DELT = 5E-5 DELP = 5E-5
 GRAD = 2 POPT = 1,1,1,0,2 SOPT = 0
 EPS = 0.002 COMP = 0

SRECO
 NAME = 'NONE' RECO = 0 RCWT = 0

SPRIM
 NAME = 'BENITE' CHWT = 0.001
 GAMA = 1.25 FORC = 212500
 COV = 30 TEMP = 2000

SPROP
 NAME = 'BENITE' CHWT = 0.072 GRAN = 'CORD'
 RHO = 0.06 GAMA = 1.25 FORC = 212500
 COV = 30 TEMP = 2000 EROS = 0.00000
 ALPH = 0 BETA = 10 IGNC = 0
 LEN = 10. DIAM = 0.08

SPROP
 NAME = 'M30 7P' CHWT = 11.9 GRAN='GEN'
 RHO = 0.0607 GAMA = 1.241 FORC = 360000
 COV = 29.11 TEMP = 3010 EROS = 0.0000000
 NTBL=0 ALPH=0.8 BETA=0.001320
 \$ THE FOLLOWING PARAMETERS REPLACED BY DEPTH-BURNED/SURFACE ARRAY
 \$ LEN =0.63 DIAM = 0.3087 PD = 0.0245
 \$ WEB=0.0588 GRAN = '7PF'
 NSUR=8
 DEPB=0. 0.0106, 0.02925, 0.0300, 0.0330, 0.0351, 0.038, 0.040
 SURF=4756., 5517., 6589., 5067., 2823., 1900., 1100., 710.

SEND

Producing the following output:

ERRTOL= 4.768372E-07

```

CARD 1 --- $COMMENT
CARD 2 --- IBHVG2 BENCHMARK TEST CASE 2
CARD 3 ---
CARD 4 --- TWO INDEPENDENT DATA SETS IN ONE IBHVG2 RUN
CARD 5 ---
CARD 6 --- FIRST SET : Laterally Deterred Propellant
CARD 7 --- (VERY THIN TRANSITION ZONE BETWEEN OUTER AND INNER
CARD 8 --- PROPELLANT TYPES, RESULTING IN THREE LAYERS)
CARD 9 --- 1 - DETERRENT, .0007 THICK, LOW B/R EXPONENT
CARD 10 --- 2 - TRANSITION ZONE, .0001 THICK, FROM LOW TO HI EXP
CARD 11 --- 3 - CORE PROPELLANT, HI BURNING RATE
CARD 12 ---
CARD 13 --- SECOND SET : STANDARD 105MM CANNON
CARD 14 --- PIDDUCK-KENT INTERNAL PRESSURE GRADIENT EQUATION
CARD 15 --- USE GENERAL GRAIN FORM FUNCTION
CARD 16 ---
CARD 17 --- $HEAT
CARD 18 --- TSHL = 0.00450 CSHL = 1848 RSHL = 0.284
CARD 19 --- TVAL = 293 NO = 0.0648 NL = 1
CARD 20 ---
CARD 21 --- $GUN
CARD 22 --- NAME='XM881 25MM APFSDS-T' CHAM=5.86 GRVE=0.988 LAND=0.980
CARD 23 --- G/L=1 TRAV=74 TWST=25
CARD 24 --- CLEN=5 NGAG=2 GLOC=-5.0
CARD 25 ---
CARD 26 --- $PROJ
CARD 27 --- NAME = 'APFSDS-T' PRVT = 0.170
CARD 28 ---
CARD 29 --- $RESI
CARD 30 --- NPTS = 4 AIR = 1
CARD 31 --- TRAV = 0, 0.2, 1.0, 74
CARD 32 --- PRES = 200, 2000, 400, 400
CARD 33 ---
CARD 34 --- $INFO
CARD 35 --- RUN = '120MATCH-182M881' DELT = 5E-5 DELP = 5E-5
CARD 36 --- GRAD = 2 POPT = 1,1,1,0,2 SOPT = 0
CARD 37 --- EPS = 0.002 COMP = 0
CARD 38 ---
CARD 39 --- $RECO
CARD 40 --- NAME = 'NONE' RECO = 0 RCWT = 0
CARD 41 ---
CARD 42 --- $PRIM
CARD 43 --- NAME='B/KNO3' CHWT=0.00022
CARD 44 --- GAMA = 1.25 FORC = 212500
CARD 45 --- COV = 30 TEMP = 2000
CARD 46 ---
CARD 47 --- $PROP
CARD 48 --- NAME='M10 7P' CHWT=0.2071 GRAN='7PF'
CARD 49 --- RHO=0.06 GAMA=1.2385 FORC=330000
CARD 50 --- COV=27.04 TEMP=3073 EROS=0
CARD 51 --- NTBL=-1
CARD 52 --- PR2P=100000 PR2E=100000 PR2L=100000
CARD 53 --- PR3P=100000 PR3E=100000 PR3L=100000
CARD 54 --- PR4L=100000
CARD 55 --- CF2P=.00289 CF2E=0.00289 CF2L=0.00289

```


CARD	56	-->	EX2P=0.678	EX2E=0.678	EX2L=0.678
CARD	57	-->	CF3P=0.00289	CF3E=0.00289	CF3L=0.00289
CARD	58	-->	EX3P=0.678	EX3E=0.678	EX3L=0.678
CARD	59	-->	CF4L=0.004656	EX4L=0.7061	
CARD	60	-->	DEPP=,0.0007,0.0008	DEPE=,0.0007,0.0008	DZPL=,0.0007,0.0008
CARD	61	-->	LEN=0.0972	DIAH=0.0928	PD=0.0058
CARD	62	-->	W1=0.0175	W0=0.0202	
CARD	63	-->	SEND		

 - GUN TUNE -

 TYPE: M0801 25MM APFS08-T
 GROOVE DIAMETER (IN): 0.988
 TWIST (CALS/TURN): 25.0
 SHELL THICKNESS (IN): 0.004500
 INITIAL SHELL TEMP (K): 293.
 NO. GAGES: 2
 1 LOCATION (IN) 1
 1 -5.00 2
 CHAMBER VOLUME (IN3): 5.86
 LAND DIAMETER (IN): 0.980
 BORE AREA (IN2): 0.7605
 SHELL CP (IN-LB/LB-K): 1048.0
 AIR NO (IN-LB/IN2-S-K): 0.06480
 CHAMBER LENGTH (IN): 5.00
 1 LOCATION (IN) 1
 2 0.00
 TRAVEL (IN): 74.00
 GROOVE/LAND RATIO (-): 1.000
 HEAT-LOSS OPTION: 1
 SHELL DENSITY (LB/IN3): 0.2040

 - PROJECTILE -

 TYPE: APFS08-T
 TOTAL WEIGHT (LB): 0.170
 WEIGHT PREDICTOR OPTION: 0

 - RESISTANCE -

 AIR RESISTANCE OPTION: 1
 1 TRAVEL (IN) PRESSURE (PSI) 1 TRAVEL (IN) PRESSURE (PSI)
 1 0.00 200. 3 1.00 400. 4 74.00 400.
 2 0.20 2000.
 WALL HEATING FRACTION: 0.000
 FRICTION TABLE LENGTH: 4

 - GENERAL -

 MAX TIME STEP (S): 0.000050
 PRINT OPTIONS: 1 1 1 0 2 1
 GRADIENT MODEL: PIDOUCK-KENT
 PRINT STEP (S): 0.000050
 STORE OPTION: 0
 MAX RELATIVE ERROR (-): 0.00200
 CONSTANT-PRESSURE OPTION: 0

 - RECOIL -

 RECOIL OPTION: 0
 TYPE: NONE
 RECOILING WEIGHT (LB): 0.

 - PRIMER -

 TYPE: B/KM03
 CONVOLUME (IN3/LB): 30.000
 GAMMA (-): 1.2500
 FLAME TEMP (K): 2000.0
 FORCE (FT-LB/LB): 212500.
 WEIGHT (LB): 0.000220

- CHARGE 1 -

TYPE: M10 7P
 EROSION COEFF (-):
 GRAIN LENGTH (IN):
 INNER WEB (IN):

0.000000
 0.09720
 0.01750

GRAINS:
 CHARGE IGM CODE:
 GRAIN DIAMETER (IN):
 OUTER WEB (IN):

5397.8
 0
 0.09280
 0.02020

WEIGHT (LB):
 CHARGE IGM AT (S):
 PERF DIAMETER (IN):

0.2071
 0.00000E+00
 0.00580

PROPERTIES AT LAYER BOUNDARIES OF PERF SURFACES

	1ST	2ND	3RD	4TH
AT DEPTH (IN):	---	0.00000	0.00070	0.00080
ADJACENT LAYER WT %:	---	1.510	0.240	93.161
DENSITY (LB/IN3):	---	0.06000	0.06000	0.06000
GAMMA (-):	---	1.2385	1.2385	1.2385
FORCE (FT-LB/LB):	---	330000.	330000.	330000.
COVOLUME (IN3/LB):	---	27.040	27.040	27.040
FLAME TEMP (K):	---	3073.0	3073.0	3073.0
MEAN PRESSURES (PSI):	---	100000.0	100000.0	100000.0
BURNING RATE EXPS:	---	0.6780	0.6780	0.6780
BURNING RATE COEFFS:	---	0.0028900	0.0028900	0.0046560

PROPERTIES AT LAYER BOUNDARIES OF END SURFACES

	1ST	2ND	3RD	4TH
AT DEPTH (IN):	---	0.00000	0.00070	0.00080
ADJACENT LAYER WT %:	---	1.408	0.196	93.161
DENSITY (LB/IN3):	---	0.06000	0.06000	0.06000
GAMMA (-):	---	1.2385	1.2385	1.2385
FORCE (FT-LB/LB):	---	330000.	330000.	330000.
COVOLUME (IN3/LB):	---	27.040	27.040	27.040
FLAME TEMP (K):	---	3073.0	3073.0	3073.0
MEAN PRESSURES (PSI):	---	100000.0	100000.0	100000.0
BURNING RATE EXPS:	---	0.6780	0.6780	0.6780
BURNING RATE COEFFS:	---	0.0028900	0.0028900	0.0046560

PROPERTIES AT LAYER BOUNDARIES OF LAT SURFACES

	1ST	2ND	3RD	4TH
AT DEPTH (IN):	---	0.00000	0.00070	0.00080
ADJACENT LAYER WT %:	---	3.057	0.429	93.161
DENSITY (LB/IN3):	---	0.06000	0.06000	0.06000
GAMMA (-):	---	1.2385	1.2385	1.2385
FORCE (FT-LB/LB):	---	330000.	330000.	330000.
COVOLUME (IN3/LB):	---	27.040	27.040	27.040
FLAME TEMP (K):	---	3073.0	3073.0	3073.0
MEAN PRESSURES (PSI):	---	100000.0	100000.0	100000.0
BURNING RATE EXPS:	---	0.6780	0.6780	0.6780
BURNING RATE COEFFS:	---	0.0028900	0.0028900	0.0046560

TIME (MS)	TRAV (IN)	VEL (FT/S)	ACC (G)	BREECH PRESS (PSI)	MEAN PRESS (PSI)	BASE PRESS (PSI)	MEAN TEMP (K)	FRAC BURN 1
0.000	0.00	0.	0.	234.	234.	234.	2000.	0.000
0.050	0.00	0.	570.	516.	449.	328.	2411.	0.001
0.100	0.00	2.	1586.	882.	768.	561.	2651.	0.002
0.150	0.00	6.	2950.	1393.	1212.	885.	2793.	0.003
0.200	0.01	12.	4677.	2073.	1803.	1317.	2878.	0.005
0.250	0.02	21.	6765.	2944.	2561.	1871.	2932.	0.007
0.300	0.03	34.	9183.	4024.	3500.	2557.	2965.	0.010
0.350	0.06	51.	11867.	5324.	4631.	3383.	2985.	0.013
0.400	0.10	72.	14714.	6843.	5953.	4349.	2995.	0.017
0.450	0.15	98.	17574.	8569.	7454.	5445.	2999.	0.022
0.500	0.21	129.	20933.	10472.	9109.	6654.	2996.	0.027
0.550	0.30	168.	27484.	12499.	10873.	7943.	2988.	0.034
0.600	0.42	217.	34389.	14569.	12673.	9258.	2974.	0.041
0.650	0.57	278.	41401.	16571.	14415.	10530.	2954.	0.049
0.700	0.75	351.	48241.	18388.	15995.	11685.	2927.	0.057
0.714	0.81	372.	50010.	18825.	16375.	11963.	2918.	0.060
LAYER TRANSITION 2 TO 3 ON PERF SURFACE OF PROPELLANT 1								
LAYER TRANSITION 2 TO 3 ON END SURFACE OF PROPELLANT 1								
LAYER TRANSITION 2 TO 3 ON LAT SURFACE OF PROPELLANT 1								
SHOT-START PRESSURE ACHIEVED								
0.745	0.96	426.	56718.	20715.	18019.	13163.	2904.	0.068
LAYER TRANSITION 3 TO 4 ON PERF SURFACE OF PROPELLANT 1								
LAYER TRANSITION 3 TO 4 ON END SURFACE OF PROPELLANT 1								
LAYER TRANSITION 3 TO 4 ON LAT SURFACE OF PROPELLANT 1								
0.750	0.99	435.	58346.	21208.	18448.	13477.	2903.	0.070
0.800	1.28	540.	72675.	26216.	22804.	16659.	2885.	0.093
0.850	1.64	668.	86257.	31000.	26966.	19699.	2857.	0.119
0.900	2.09	817.	98072.	35165.	30589.	22346.	2821.	0.146
0.950	2.62	983.	107234.	38399.	33402.	24401.	2777.	0.180
1.000	3.27	1161.	113276.	40537.	35262.	25760.	2729.	0.213
1.050	4.02	1346.	116206.	41582.	36171.	26424.	2678.	0.248
1.079	4.51	1456.	116611.	41735.	36304.	26521.	2647.	0.269
LOCAL PRESSURE MAX DETECTED								
1.100	4.88	1533.	116389.	41665.	36243.	26476.	2626.	0.284
1.150	5.86	1719.	114406.	40986.	35653.	26045.	2573.	0.319
1.200	6.95	1901.	110871.	39763.	34588.	25268.	2522.	0.355
1.250	8.14	2076.	106336.	38189.	33220.	24268.	2473.	0.389
1.300	9.44	2243.	101247.	36421.	31682.	23144.	2426.	0.423
1.350	10.83	2402.	95931.	34574.	30075.	21970.	2382.	0.456
1.400	12.32	2552.	90614.	32726.	28467.	20796.	2340.	0.488
1.450	13.89	2694.	85441.	30929.	26904.	19654.	2301.	0.518
1.500	15.55	2827.	80500.	29713.	25411.	18564.	2264.	0.548
1.550	17.28	2953.	75837.	27595.	24004.	17535.	2229.	0.576
1.600	19.09	3072.	71472.	26081.	22687.	16573.	2196.	0.604
1.650	20.97	3183.	67406.	24672.	21461.	15678.	2165.	0.630
1.700	22.91	3289.	63631.	23365.	20324.	14847.	2136.	0.655
1.750	24.91	3388.	60133.	22154.	19271.	14078.	2108.	0.680
1.800	26.97	3483.	56892.	21033.	18296.	13366.	2082.	0.704
1.850	29.09	3572.	53891.	19997.	17394.	12707.	2057.	0.726
1.900	31.26	3656.	51110.	19037.	16559.	12097.	2033.	0.749
1.950	33.48	3736.	48531.	18147.	15786.	11532.	2011.	0.770
2.000	35.74	3813.	46136.	17322.	15068.	11008.	1989.	0.791
2.050	38.05	3885.	43910.	16556.	14402.	10521.	1968.	0.811
2.100	40.40	3954.	41744.	15811.	13753.	10047.	1946.	0.829
2.150	42.79	4019.	39598.	15072.	13110.	9577.	1924.	0.845

TIME (MS)	TRAV (IN)	VEL (FT/S)	ACC (G)	BRECH PRESS (PSI)	MEAN PRESS (PSI)	BASE PRESS (PSI)	MEAN TEMP (K)	FRAC BURN 1
2.200	45.22	4082.	37540.	14362.	12493.	9127.	1901.	0.860
2.250	47.69	4140.	35585.	13689.	11908.	8699.	1878.	0.873
2.300	50.19	4196.	33737.	13054.	11355.	8295.	1855.	0.886
2.350	52.73	4249.	31996.	12454.	10834.	7914.	1833.	0.897
2.400	55.29	4299.	30358.	11891.	10344.	7556.	1812.	0.908
2.450	57.88	4347.	28817.	11361.	9883.	7220.	1790.	0.918
2.500	60.51	4392.	27312.	10844.	9433.	6891.	1768.	0.927
2.550	63.15	4435.	25853.	10342.	8996.	6572.	1745.	0.934
2.600	65.83	4475.	24462.	9864.	8580.	6268.	1723.	0.940
2.650	68.52	4514.	23144.	9410.	8186.	5980.	1700.	0.946
2.700	71.24	4550.	21903.	8984.	7815.	5709.	1678.	0.951
2.750	73.98	4584.	20735.	8582.	7465.	5454.	1656.	0.955
2.750	74.00	4584.	20729.	8580.	7464.	5452.	1656.	0.955
PROJECTILE EXIT								

CONDITIONS AT:	P _{MAX}	MUZZLE
TIME (MS):	1.079	2.750
TRAVEL (IN):	4.51	74.00
VELOCITY (FT/S):	1456.	4584.
ACCELERATION (G):	116611.	20729.
BREECH PRESS (PSI):	41735.	8580.
MEAN PRESS (PSI):	36304.	7464.
BASE PRESS (PSI):	26521.	5452.
MEAN TEMP (K):	2647.	1656.
Z CHARGE 1 (-):	0.269	0.955

GAGE	AT (IN)	P _{MAX} (PSI)
	WRT SON	
1	-5.00	41735.
2	0.00	35559.

ENERGY BALANCE SUMMARY	IN-LB	%
TOTAL CHEMICAL:	3286882.	100.00
(1) INTERNAL GAS:	1771932.	53.91
(2) WORK AND LOSSES:	1514950.	46.09
(A) PROJECTILE KINETIC:	665761.	20.26
(B) GAS KINETIC:	245588.	7.47
(C) PROJECTILE ROTATIONAL:	5257.	0.16
(D) FRICTIONAL WORK TO TUBE:	0.	0.00
(E) OTHER FRICTIONAL WORK:	23103.	0.70
(F) WORK DONE AGAINST AIR:	15303.	0.47
(G) HEAT CONVECTED TO BORE:	559938.	17.04
(H) RECOIL ENERGY:	0.	0.00

LOADING DENSITY (G/CM ³):	0.979
CHARGE WT/PROJECTILE WT:	1.220
PIEZOMETRIC EFFICIENCY:	0.283
EXPANSION RATIO:	10.603

CARD 64 -->
 CARD 65 -->
 CARD 66 --> SHEAT
 CARD 67 --> TSHL = 0.00450 CSHL = 1848 RSHL = 0.284
 CARD 68 --> TWAL = 293 NO = 0.0648 NL = 1
 CARD 69 -->
 CARD 70 --> SGUN
 CARD 71 --> NAME = '105-MM GUN M68' CHAM = 375 GRVE = 4.224
 CARD 72 --> LAND = 4.134 G/L = 2. TRAV = 187
 CARD 73 --> TWST = 99
 CARD 74 -->
 CARD 75 --> \$PROJ
 CARD 76 --> NAME = 'M456A2' PRWT = 23.2
 CARD 77 -->
 CARD 78 --> \$RESI
 CARD 79 --> NPTS = 4 AIR = 1
 CARD 80 --> TRAV = 0, 0.5, 8.0, 187
 CARD 81 --> PRES = 100, 2100, 500, 200
 CARD 82 -->
 CARD 83 --> \$INFO
 CARD 84 --> RUN = '10SMATCH-1105' DELT = 5E-5 DELP = 5E-5
 CARD 85 --> GRAD = 2 POPT = 1,1,1,0,2 SOPT = 0
 CARD 86 --> EPS = 0.002 COMP = 0
 CARD 87 -->
 CARD 88 --> \$RECO
 CARD 89 --> NAME = 'NONE' RECO = 0 RCWT = 0
 CARD 90 -->
 CARD 91 --> \$PRIN
 CARD 92 --> NAME = 'BENITE' CHWT = 0.001
 CARD 93 --> GAMA = 1.25 FORC = 212500
 CARD 94 --> COV = 30 TEMP = 2000
 CARD 95 -->
 CARD 96 --> \$PROP
 CARD 97 --> NAME = 'BENITE' CHWT = 0.072 GRAN = 'CORD'
 CARD 98 --> RHO = 0.06 GAMA = 1.25 FCRC = 212500
 CARD 99 --> COV = 30 TEMP = 2000 EROS = 0.000000
 CARD 100 --> ALPH = 0 BETA = 10 IGMC = 0
 CARD 101 --> LEN = 10. DIAM = 0.08
 CARD 102 -->
 CARD 103 --> \$PROP
 CARD 104 --> NAME = 'M30 7P' CHWT = 11.9 GRAN = 'GEN'
 CARD 105 --> RHO = 0.0607 GAMA = 1.241 FORC = 360000
 CARD 106 --> COV = 29.11 TEMP = 3010 EROS = 0.00000000
 CARD 107 --> NTBL=0 ALPH=0.8 BETA=0.001320
 CARD 108 --> \$ THE FOLLOWING PARAMETERS REPLACED BY DEPTH-BURNED/SURFACE ARRAY
 CARD 109 --> \$ LEN = 0.63 DIAM = 0.3087 PD = 0.0245
 CARD 110 --> \$ WEB=0.0588 GRAN = '7PF'
 CARD 111 --> NSUR=8
 CARD 112 --> DEPB=0., 0.0106, 0.02925, 0.0300, 0.0330, 0.0351, 0.038, 0.040
 CARD 113 --> SURF=4756., 5517., 6589., 5067., 2823., 1900., 1100., 710.
 CARD 114 -->
 CARD 115 --> \$END

- GUN TUBE -

TYPE: 105-MM GUN M68
GROOVE DIAMETER (IN):
TUIST (CAL/S/TURN):
SHELL THICKNESS (IN):
INITIAL SHELL TEMP (K):

4.224
99.0
0.004500
293.

CHAMBER VOLUME (IN3):
LAND DIAMETER (IN):
BORE AREA (IN2):
SHELL CP (IN-LB/LB-K):
AIR MO (IN-LB/IN2-S-K):

375.00
4.134
13.8163
1848.0
0.06480

TRAVEL (IN):
GROOVE/LAND RATIO (-):
HEAT-LOSS OPTION:
SHELL DENSITY (LB/IN3):

187.00
2.000
1
0.2840

- PROJECTILE -

TYPE: M456A2

TOTAL WEIGHT (LB):

23.200

WEIGHT PREDICTOR OPTION: 0

- RESISTANCE -

AIR RESISTANCE OPTION: 1

WALL HEATING FRACTION: 0.000

FRICTION TABLE LENGTH: 4

1 TRAVEL (IN) PRESSURE (PSI)
1 1 1 0 2 1
2 0.00 100.
0.50 2100.

1 TRAVEL (IN) PRESSURE (PSI)
3 8.00 500.

1 TRAVEL (IN) PRESSURE (PSI)
4 187.00 200.

- GENERAL -

MAX TIME STEP (S): 0.000050
PRINT OPTIONS: 1 1 1 0 2 1
GRADIENT MODEL: PIDDUCK-KENT

PRINT STEP (S):
STORE OPTION:

0.000050
0

MAX RELATIVE ERROR (-): 0.00200
CONSTANT-PRESSURE OPTION: 0

- RECOIL -

RECOIL OPTION: 0

TYPE: NONE

RECOILING WEIGHT (LB): 0.

- PRIMER -

TYPE: BENITE
COVOLUME (IN3/LB):

30.000

1.2500
2000.0

FORCE (FT-LB/LB): 212500.
WEIGHT (LB): 0.001000

- CHARGE 1 -

TYPE: BENITE	GRAINS:	23.873	0.00000	0.00000	0.0720
EROSIVE COEFF (-):	CHARGE IGM CODE:				
GRAIN LENGTH (IN):	GRAIN DIAMETER (IN):	0.08000			0.00000E+00

AT DEPTH (IN):	PROPERTIES AT LAYER BOUNDARIES OF END SURFACES	PROPERTIES AT LAYER BOUNDARIES OF LAT SURFACES
ADJACENT LAYER WT %:	1ST 2ND 3RD 4TH	1ST 2ND 3RD 4TH
DENSITY (LB/IN3):	0.00000	0.00000
GAMMA (-):	100.000	100.000
FORCE (FT-LB/LB):	0.06000	0.06000
COVOLUME (IN3/LB):	1.2500	1.2500
FLAME TEMP (K):	212500.	212500.
BURNING RATE EXPS:	30.000	30.000
BURNING RATE COEFFS:	2000.0	2000.0
	0.0000	0.0000
	10.0000000	10.0000000

- CHARGE 2 -

TYPE: M30 7P	GRAINS:	1.0000	0.00000	0.00000	11.9000
EROSIVE COEFF (-):	CHARGE IGM CODE:				0.00000E+00
1 DEPTH (IN)	1 DEPTH (IN)				
1 0.00000	4 0.03000	5067.0			
2 0.01060	5 0.03500	2823.0			
3 0.02925	6 0.03510	1900.0			

AT DEPTH (IN):	PROPERTIES AT LAYER BOUNDARIES OF LAT SURFACES	PROPERTIES AT LAYER BOUNDARIES OF LAT SURFACES
ADJACENT LAYER WT %:	1ST 2ND 3RD 4TH	1ST 2ND 3RD 4TH
DENSITY (LB/IN3):	0.00000	0.00000
GAMMA (-):	100.000	100.000
FORCE (FT-LB/LB):	0.06070	0.06070
COVOLUME (IN3/LB):	1.2610	1.2610
FLAME TEMP (K):	360000.	360000.
BURNING RATE EXPS:	29.110	29.110
BURNING RATE COEFFS:	3010.0	3010.0
	0.8000	0.8000
	0.0013200	0.0013200

TIME (MS)	TRAV (IN)	VEL (FT/S)	ACC (G)	BREECH PRESS (PSI)	MEAN PRESS (PSI)	BASE PRESS (PSI)	MEAN TEMP (K)	FRAC BURN 1	FRAC BURN 2
0.000	0.00	0.	0.	14.	14.	14.	2000.	0.000	0.000
0.050	0.00	0.	0.	47.	47.	47.	2109.	0.025	0.000
0.100	0.00	0.	0.	86.	86.	86.	2177.	0.050	0.000
0.116	0.00	0.	0.	100.	100.	100.	2197.	0.058	0.000
SHOT-START PRESSURE ACHIEVED									
0.150	0.00	0.	7.	141.	131.	112.	2235.	0.074	0.000
0.200	0.00	0.	34.	196.	182.	157.	2286.	0.098	0.000
0.250	0.00	0.	63.	258.	241.	207.	2332.	0.122	0.000
0.300	0.00	0.	97.	329.	306.	263.	2375.	0.145	0.000
0.350	0.00	0.	134.	408.	380.	326.	2415.	0.168	0.001
0.400	0.00	1.	175.	496.	462.	397.	2452.	0.191	0.001
0.450	0.00	1.	221.	594.	553.	475.	2486.	0.213	0.001
0.500	0.00	1.	271.	703.	655.	562.	2518.	0.235	0.001
0.550	0.00	2.	326.	823.	766.	658.	2548.	0.257	0.002
0.600	0.00	2.	386.	955.	890.	764.	2576.	0.278	0.002
0.650	0.01	3.	451.	1101.	1025.	880.	2602.	0.300	0.002
0.700	0.01	4.	522.	1260.	1173.	1007.	2627.	0.320	0.003
0.750	0.01	5.	598.	1434.	1335.	1147.	2649.	0.341	0.003
0.800	0.01	6.	681.	1624.	1512.	1299.	2671.	0.361	0.004
0.850	0.02	7.	771.	1830.	1705.	1464.	2691.	0.381	0.004
0.900	0.02	8.	867.	2055.	1914.	1644.	2709.	0.400	0.005
0.950	0.03	10.	970.	2299.	2141.	1839.	2727.	0.420	0.006
1.000	0.03	11.	1080.	2563.	2387.	2050.	2743.	0.439	0.007
1.050	0.04	13.	1199.	2848.	2652.	2278.	2758.	0.457	0.007
1.100	0.05	15.	1325.	3157.	2939.	2525.	2772.	0.476	0.008
1.150	0.06	18.	1460.	3489.	3249.	2790.	2786.	0.494	0.009
1.200	0.07	20.	1603.	3846.	3581.	3076.	2798.	0.511	0.010
1.250	0.08	23.	1755.	4230.	3939.	3383.	2809.	0.529	0.012
1.300	0.10	26.	1917.	4642.	4322.	3712.	2820.	0.546	0.013
1.350	0.11	29.	2088.	5083.	4733.	4065.	2830.	0.562	0.014
1.400	0.13	32.	2269.	5555.	5173.	4443.	2839.	0.579	0.016
1.450	0.15	36.	2460.	6059.	5642.	4846.	2847.	0.595	0.017
1.500	0.18	40.	2662.	6597.	6143.	5276.	2855.	0.611	0.019
1.550	0.20	45.	2874.	7170.	6676.	5734.	2862.	0.626	0.021
1.600	0.23	50.	3097.	7779.	7244.	6222.	2869.	0.641	0.023
1.650	0.26	55.	3330.	8426.	7847.	6739.	2875.	0.656	0.025
1.700	0.30	60.	3575.	9113.	8486.	7268.	2880.	0.670	0.027
1.750	0.33	66.	3831.	9840.	9163.	7870.	2885.	0.685	0.029
1.800	0.38	73.	4098.	10609.	9879.	8485.	2890.	0.699	0.032
1.850	0.42	79.	4375.	11420.	10635.	9134.	2894.	0.712	0.034
1.900	0.47	87.	4665.	12276.	11432.	9818.	2897.	0.725	0.037
1.950	0.53	95.	5028.	13177.	12271.	10539.	2900.	0.738	0.040
2.000	0.58	103.	5486.	14124.	13152.	11296.	2902.	0.751	0.043
2.050	0.65	112.	5967.	15117.	14077.	12090.	2904.	0.763	0.047
2.100	0.72	122.	6471.	16156.	15044.	12921.	2906.	0.772	0.050
2.150	0.80	133.	6997.	17241.	16055.	13789.	2907.	0.787	0.054
2.200	0.88	145.	7547.	18373.	17108.	14694.	2907.	0.798	0.058
2.250	0.97	157.	8118.	19549.	18204.	15635.	2908.	0.809	0.062
2.300	1.07	171.	8712.	20769.	19340.	16611.	2907.	0.820	0.066
2.350	1.18	185.	9326.	22031.	20515.	17620.	2906.	0.831	0.071
2.400	1.29	201.	9961.	23333.	21728.	18661.	2905.	0.841	0.076
2.450	1.42	217.	10615.	24673.	22975.	19733.	2903.	0.851	0.081
2.500	1.55	235.	11286.	26046.	24254.	20832.	2901.	0.860	0.086
2.550	1.70	254.	11973.	27451.	25562.	21955.	2898.	0.869	0.092
2.600	1.86	274.	12674.	28881.	26894.	23099.	2894.	0.878	0.097

TIME (MS)	TRAV (IN)	VEL (FT/S)	ACC (G)	BREECH PRESS (PSI)	MEAN PRESS (PSI)	BASE PRESS (PSI)	MEAN TEMP (K)	FRAC BURN 1	FRAC BURN 2
2.650	2.03	295.	13387.	30333.	28246.	24260.	2891.	0.887	0.103
2.700	2.21	317.	14110.	31802.	29614.	25435.	2886.	0.895	0.110
2.750	2.41	340.	14839.	33281.	30991.	26618.	2881.	0.903	0.116
2.800	2.62	365.	15572.	34764.	32372.	27804.	2876.	0.911	0.123
2.850	2.85	390.	16306.	36245.	33751.	28988.	2870.	0.918	0.130
2.900	3.09	417.	17037.	37717.	35122.	30165.	2864.	0.925	0.138
2.950	3.35	445.	17763.	39172.	36477.	31329.	2857.	0.931	0.145
3.000	3.62	474.	18479.	40604.	37810.	32474.	2850.	0.938	0.153
3.050	3.92	505.	19183.	42004.	39114.	33595.	2842.	0.944	0.161
3.100	4.23	536.	19871.	43366.	40383.	34684.	2834.	0.950	0.170
3.150	4.56	569.	20539.	44683.	41609.	35737.	2825.	0.955	0.178
3.200	4.91	602.	21186.	45947.	42786.	36748.	2816.	0.960	0.187
3.250	5.28	637.	21806.	47153.	43909.	37712.	2807.	0.965	0.196
3.300	5.67	672.	22399.	48294.	44971.	38625.	2797.	0.970	0.206
3.350	6.09	709.	22961.	49364.	45968.	39481.	2787.	0.974	0.215
3.400	6.53	746.	23490.	50360.	46395.	40278.	2776.	0.978	0.225
3.450	6.98	784.	23984.	51277.	47749.	41011.	2766.	0.981	0.235
3.500	7.47	823.	24442.	52113.	48527.	41679.	2755.	0.984	0.245
3.550	7.97	863.	24863.	52863.	49226.	42280.	2743.	0.987	0.256
3.600	8.50	903.	25183.	53528.	49846.	42811.	2732.	0.990	0.266
3.650	9.06	944.	25458.	54107.	50385.	43274.	2720.	0.992	0.277
3.700	9.64	985.	25692.	54599.	50842.	43648.	2709.	0.994	0.288
3.750	10.24	1027.	25884.	55003.	51219.	43991.	2697.	0.996	0.299
3.800	10.87	1069.	26035.	55321.	51515.	44246.	2685.	0.998	0.310
3.850	11.52	1111.	26146.	55556.	51734.	44433.	2673.	0.999	0.321
3.900	12.20	1153.	26219.	55711.	51878.	44557.	2661.	0.999	0.332
3.950	12.91	1195.	26256.	55789.	51950.	44619.	2649.	1.000	0.343
4.000	13.64	1237.	26257.	55793.	51954.	44623.	2637.	1.000	0.354
PROPELLANT 1 BURNED OUT									
4.050	14.39	1280.	26226.	55729.	51894.	44571.	2625.	1.000	0.366
LOCAL PRESSURE MAX DETECTED									
4.100	15.17	1322.	26164.	55599.	51774.	44468.	2613.	1.000	0.377
4.150	15.98	1364.	26073.	55410.	51598.	44316.	2601.	1.000	0.388
4.200	16.81	1406.	25956.	55165.	51370.	44121.	2590.	1.000	0.400
4.250	17.66	1448.	25814.	54869.	51094.	43884.	2578.	1.000	0.411
4.300	18.54	1489.	25651.	54527.	50775.	43610.	2566.	1.000	0.423
4.350	19.45	1530.	25447.	54142.	50417.	43302.	2555.	1.000	0.434
4.400	20.38	1571.	25265.	53719.	50023.	42964.	2544.	1.000	0.445
4.450	21.34	1611.	25047.	53263.	49598.	42599.	2533.	1.000	0.457
4.500	22.31	1652.	24815.	52776.	49145.	42210.	2522.	1.000	0.468
4.550	23.32	1691.	24570.	52263.	48668.	41800.	2511.	1.000	0.479
4.600	24.34	1731.	24314.	51728.	48169.	41371.	2501.	1.000	0.490
4.650	25.39	1770.	24049.	51173.	47652.	40928.	2490.	1.000	0.501
4.700	26.47	1808.	23777.	50601.	47120.	40470.	2480.	1.000	0.512
4.750	27.56	1846.	23497.	50016.	46575.	40003.	2470.	1.000	0.523
4.800	28.68	1884.	23213.	49420.	46020.	39526.	2460.	1.000	0.534
4.850	29.82	1921.	22924.	48816.	45457.	39042.	2451.	1.000	0.545
4.900	30.99	1958.	22633.	48204.	44888.	38553.	2441.	1.000	0.556
4.950	32.17	1994.	22339.	47589.	44315.	38061.	2432.	1.000	0.567
5.000	33.38	2030.	22044.	46971.	43739.	37567.	2423.	1.000	0.577
5.050	34.61	2065.	21749.	46351.	43162.	37071.	2414.	1.000	0.588
5.100	35.86	2100.	21453.	45732.	42586.	36576.	2405.	1.000	0.598
5.150	37.13	2134.	21159.	45115.	42011.	36082.	2396.	1.000	0.609
5.200	38.42	2168.	20866.	44500.	41439.	35591.	2388.	1.000	0.619
5.250	39.73	2201.	20575.	43890.	40870.	35103.	2380.	1.000	0.629

TIME (MS)	TRAV (IN)	VEL (FT/S)	ACC (G)	BREECH PRESS (PSI)	MEAN PRESS (PSI)	BASE PRESS (PSI)	MEAN TEMP (K)	FRAC BURN 1	FRAC BURN 2
5.300	41.06	2234.	20286.	43284.	40306.	34618.	2372.	1.000	0.639
5.350	42.41	2266.	19999.	42683.	39747.	34138.	2364.	1.000	0.649
5.400	43.78	2298.	19716.	42089.	39193.	33662.	2356.	1.000	0.659
5.450	45.17	2330.	19436.	41501.	38646.	33192.	2348.	1.000	0.669
5.500	46.57	2361.	19159.	40921.	38106.	32728.	2341.	1.000	0.679
5.550	48.00	2392.	18886.	40348.	37572.	32270.	2333.	1.000	0.689
5.600	49.44	2422.	18617.	39784.	37047.	31819.	2326.	1.000	0.698
5.650	50.91	2451.	18352.	39228.	36529.	31374.	2319.	1.000	0.708
5.700	52.39	2481.	18091.	38680.	36019.	30936.	2312.	1.000	0.718
5.750	53.88	2510.	17834.	38141.	35517.	30505.	2305.	1.000	0.727
5.800	55.40	2538.	17581.	37611.	35023.	30081.	2299.	1.000	0.736
5.850	56.93	2566.	17333.	37090.	34538.	29664.	2292.	1.000	0.746
5.900	58.48	2594.	17089.	36578.	34061.	29255.	2286.	1.000	0.755
5.950	60.04	2621.	16849.	36075.	33593.	28852.	2280.	1.000	0.764
6.000	61.62	2648.	16614.	35581.	33133.	28457.	2273.	1.000	0.773
6.050	63.22	2675.	16383.	35096.	32682.	28070.	2267.	1.000	0.782
6.100	64.83	2701.	16156.	34621.	32239.	27689.	2261.	1.000	0.791
6.150	66.46	2727.	15934.	34154.	31804.	27316.	2256.	1.000	0.799
6.200	68.11	2752.	15716.	33696.	31377.	26949.	2250.	1.000	0.808
6.250	69.76	2778.	15502.	33247.	30959.	26590.	2244.	1.000	0.817
6.300	71.44	2802.	15292.	32806.	30549.	26238.	2239.	1.000	0.825
6.350	73.13	2827.	15087.	32374.	30147.	25893.	2233.	1.000	0.834
6.400	74.83	2851.	14885.	31951.	29752.	25554.	2228.	1.000	0.842
6.450	76.55	2875.	14688.	31536.	29366.	25222.	2223.	1.000	0.851
6.500	78.28	2898.	14491.	31122.	28981.	24891.	2217.	1.000	0.859
6.550	80.03	2921.	14283.	30686.	28574.	24542.	2212.	1.000	0.866
6.600	81.79	2944.	14065.	30227.	28148.	24175.	2205.	1.000	0.873
6.650	83.56	2967.	13839.	29752.	27705.	23795.	2199.	1.000	0.879
6.700	85.35	2989.	13613.	29276.	27262.	23415.	2192.	1.000	0.885
6.750	87.15	3010.	13387.	28803.	26821.	23036.	2185.	1.000	0.891
6.800	88.96	3032.	13163.	28331.	26382.	22659.	2179.	1.000	0.896
6.850	90.78	3053.	12940.	27863.	25946.	22284.	2172.	1.000	0.901
6.900	92.62	3074.	12719.	27398.	25513.	21913.	2165.	1.000	0.906
6.950	94.47	3094.	12500.	26937.	25084.	21544.	2158.	1.000	0.910
7.000	96.33	3114.	12283.	26481.	24659.	21179.	2151.	1.000	0.914
7.050	98.21	3133.	12069.	26029.	24239.	20818.	2144.	1.000	0.918
7.100	100.09	3153.	11857.	25583.	23823.	20461.	2136.	1.000	0.922
7.150	101.99	3172.	11647.	25142.	23412.	20108.	2129.	1.000	0.926
7.200	103.90	3190.	11440.	24706.	23006.	19760.	2122.	1.000	0.929
7.250	105.82	3208.	11236.	24277.	22606.	19416.	2115.	1.000	0.932
7.300	107.75	3226.	11035.	23853.	22212.	19077.	2108.	1.000	0.935
7.350	109.69	3244.	10837.	23434.	21824.	18744.	2100.	1.000	0.938
7.400	111.64	3261.	10643.	23028.	21443.	18417.	2093.	1.000	0.941
7.450	113.60	3278.	10453.	22628.	21071.	18097.	2086.	1.000	0.944
7.500	115.58	3295.	10267.	22236.	20706.	17784.	2079.	1.000	0.946
7.550	117.56	3311.	10085.	21852.	20349.	17477.	2072.	1.000	0.948
7.600	119.55	3327.	9907.	21476.	19999.	17177.	2065.	1.000	0.951
7.650	121.55	3343.	9733.	21108.	19656.	16882.	2057.	1.000	0.953
7.700	123.56	3359.	9562.	20748.	19321.	16594.	2050.	1.000	0.955
7.750	125.58	3374.	9395.	20395.	18992.	16312.	2043.	1.000	0.957
7.800	127.61	3389.	9231.	20050.	18671.	16036.	2037.	1.000	0.958
7.850	129.65	3404.	9071.	19712.	18356.	15766.	2030.	1.000	0.960
7.900	131.69	3418.	8914.	19381.	18048.	15501.	2023.	1.000	0.962
7.950	133.75	3432.	8761.	19058.	17747.	15242.	2016.	1.000	0.963
8.000	135.81	3446.	8612.	18742.	17452.	14990.	2009.	1.000	0.965

TIME (MS)	TRAV (IN)	VEL (FT/S)	ACC (G)	BREECH PRESS (PSI)	MEAN PRESS (PSI)	BASE PRESS (PSI)	MEAN TEMP (K)	FRAC BURN 1	FRAC BURN 2
8.050	137.88	3460.	8466.	18433.	17165.	14743.	2003.	1.000	0.966
8.100	139.96	3474.	8323.	18132.	16884.	14502.	1996.	1.000	0.968
8.150	142.05	3487.	8184.	17837.	16610.	14266.	1989.	1.000	0.969
8.200	144.15	3500.	8048.	17549.	16342.	14026.	1983.	1.000	0.971
8.250	146.25	3513.	7915.	17268.	16080.	13811.	1976.	1.000	0.972
8.300	148.36	3525.	7785.	16993.	15824.	13591.	1970.	1.000	0.973
8.350	150.48	3538.	7658.	16724.	15574.	13376.	1964.	1.000	0.974
8.400	152.61	3550.	7534.	16462.	15329.	13166.	1957.	1.000	0.975
8.450	154.74	3562.	7413.	16205.	15090.	12960.	1951.	1.000	0.976
8.500	156.88	3574.	7294.	15953.	14856.	12759.	1945.	1.000	0.977
8.550	159.03	3586.	7179.	15708.	14627.	12563.	1939.	1.000	0.978
8.600	161.19	3597.	7065.	15467.	14403.	12371.	1932.	1.000	0.979
8.650	163.35	3608.	6955.	15232.	14184.	12183.	1926.	1.000	0.980
8.700	165.52	3620.	6846.	15002.	13970.	11999.	1920.	1.000	0.981
8.750	167.69	3630.	6740.	14777.	13761.	11819.	1914.	1.000	0.982
8.800	169.87	3641.	6637.	14557.	13556.	11643.	1908.	1.000	0.983
8.850	172.06	3652.	6535.	14342.	13355.	11470.	1903.	1.000	0.983
8.900	174.26	3662.	6436.	14131.	13159.	11302.	1897.	1.000	0.984
8.950	176.46	3673.	6339.	13925.	12967.	11137.	1891.	1.000	0.985
9.000	178.66	3683.	6245.	13723.	12779.	10975.	1885.	1.000	0.986
9.050	180.88	3693.	6152.	13525.	12595.	10813.	1879.	1.000	0.986
9.100	183.09	3702.	6061.	13332.	12415.	10663.	1874.	1.000	0.987
9.150	185.32	3712.	5973.	13143.	12239.	10512.	1868.	1.000	0.988
9.188	187.00	3719.	5907.	13003.	12109.	10406.	1864.	1.000	0.988

PROJECTILE EXIT

CONDITIONS AT:	PMAX	MUZZLE
TIME (MS):	4.000	9.188
TRAVEL (IN):	13.64	187.00
VELOCITY (FT/S):	1237.	3719.
ACCELERATION (G):	26257.	5907.
BREECH PRESS (PSI):	55793.	13003.
MEAN PRESS (PSI):	51954.	12109.
BASE PRESS (PSI):	44623.	10400.
MEAN TEMP (K):	2637.	1864.
Z CHARGE 1 (-):	1.000	1.000
Z CHARGE 2 (-):	0.354	0.988

ENERGY BALANCE SUMMARY	IN-LB	%
TOTAL CHEMICAL:	211486528.	100.00
(1) INTERNAL GAS:	131203024.	62.04
(2) WORK AND LOSSES:	80283504.	37.96
(A) PROJECTILE KINETIC:	59803360.	28.28
(B) GAS KINETIC:	9825915.	4.65
(C) PROJECTILE ROTATIONAL:	30111.	0.01
(D) FRICTIONAL WORK TO TUBE:	0.	0.00
(E) OTHER FRICTIONAL WORK:	1007907.	0.48
(F) WORK DONE AGAINST AIR:	463070.	0.22
(G) HEAT CONVECTED TO BORE:	9153141.	4.33
(H) RECOIL ENERGY:	0.	0.00
LOADING DENSITY (G/CM3):	0.884	
CHARGE WT/PROJECTILE WT:	0.516	
PIEZOMETRIC EFFICIENCY:	0.415	
EXPANSION RATIO:	7.890	

Test Case 3

The purpose here is to illustrate how to change the trajectory print and how to use the MULT function to alter one of the outputs. Projectile velocity, normally given in *feet/second*, has been multiplied by 12 and is now in units of *inches/second*. Three pressure gage locations have been added, one at thirty inches from projectile base (toward the breech), the second at original projectile base position, and the third at 10 inches of travel. After projectile exit, IBHVG2 also prints the blowdown phase of the shot, showing a rarefaction wave (pressure relief) moving from muzzle exit to breech.

Another complete ballistic calculation is initiated after the first solution and uses much of the previous input. The \$SAVE feature enables IBHVG2 to carry over values from the previous run except those parameters specifically given in the \$SAVE deck. Trajectory display is set back to default outputs, and blowdown phase dropped. Burning rate inputs have been changed for the second \$PROP deck from the ALPHA/BETA method to an array of pressure/rate points. The \$PARA deck is shown, where the charge weight of the second propellant (NTH=2) is varied from 25 through 27 by increments of 0.2 pounds. On the output, after the trajectory and summary information from the first iteration (CHWT=25), a table of values is printed showing iterated charge weights, maximum pressure, velocity and pressure at muzzle exit, propellant fractions burned and the point in travel where each propellant burned out (X@Z=1). Each line of output here represents an entire IBHVG2 calculation where only the charge weight input is changed from one run to the next.

```
SCOMM
IBHVG2 BENCHMARK TEST CASE 3

- SHOW TRAJECTORY PRINT OPTIONS, GUN TUBE GAUGE PRINTS, BLOWDOWN PHASE
- SHOW 'SAVE' FEATURE ; CHANGE PRINT OPTION AND BURN-RATE INPUTS;
- SHOW SMALL PARAMETRIC STUDY ON CHARGE WEIGHT FOR PROPELLANT 2, AND
  USE DEFAULT OUTPUTS FOR CHARGE WEIGHT VARIATIONS (PMAX,VMUZ,PMUZ,XBZ=1)

'TDIS' VALUES USED WITH SPECIAL PRINT OPTION - POPT(2)=2
STDIS
SHOW='TIME' REMK='TIME (MS)'
STDIS
SHOW='TRAV' REM1='TRAVEL (INCHES)'
STDIS
SHOW='VEL' REM1='VELOCITY (IN/SEC)' MULT=12.  $ IF MULT=1, THEN VEL=FT/SEC
STDIS
SHOW='ACCL' REMK='ACCEL (GRAV)'
STDIS
SHOW='FRCR' REM1='FRICTION (PSI)'
STDIS
SHOW='BRCH' REM1='BREECH PRESSURE (PSI)'
STDIS
SHOW='BASE' REM1='BASE PRESSURE (PSI)'
STDIS
SHOW='TBAR' REM1='MEAN TEMP (DEG K)'
STDIS
SHOW='WTB(1)' REM1='PROP 1 (LBS BURNED)'
STDIS
SHOW='WTB(2)' REMK='PROP 2 (LBS BURNED)'
STDIS
SHOW='WTB(3)' REM1='PROP 3 (LBS BURNED)'

SHEAT
TSHL=0.00384

SCOMM
```

```

GET MAXIMUM PRESSURES AT GAGE LOCATIONS - BREECH,
ORIGINAL PROJECTILE BASE, AND AT 10 INCHES OF TRAVEL
$GUN
NAME='155-MM 198' CHAM=1150 GRVE=6.2 LAND=6.1
G/L=1.66 TRAV=205. TWST=20 NGAG=3 GLOC=-30.,0.,10. CLEN=30.
$PROJ
NAME='M549A1' PRWT=96
$RESI
NPTS=7 TRAV=0,0.4,1.,1.55,2.05,4.5,200
PRES=250,3350,4950,3625,3250,2500,1500
$COMM
INVOKE SPECIAL TRAJECTORY PRINT OPTION - POPT(2)=2
CALCULATE AND PRINT BLOWDOWN PHASE - POPT(4)=1
$INFO
POPT=1,2,1,1,0
RUN='NEAR-STANDARD M203/M549'
$SPRM
NAME='BLK POWDER' CHWT=0.0154
GAMA=1.25 FORC=96000 COV=30 TEMP=2000
$SPROP
NAME='BLK POWDER' CHWT=0.2976 GRAN='CORD'
LEN=0.198 DIAM=0.095
RHO=0.06 GAMA=1.25 FORC=96000 COV=30 TEMP=2000
ALPH=0.0 BETA=50 EROS=0.00000
$SPROP
NAME='M30A1' CHWT=26.2 GRAN='7PF'
LEN=0.9481 DIAM=0.4173 PD=0.0338 WI=0.078975 WO=0.078975
RHO=0.0572 GAMA=1.243 FORC=356400 COV=28.5 TEMP=3040
NTBL=0 ALPH=0.701 BETA=0.004025
$SPROP
NAME='MC TUBE' CHWT=0.5 GRAN='1PF' NTBL=0 ALPH=0 BETA=30
LEN=28 DIAM=1.5 PD=1.25 WEB=0.125
FORC=180000 COV=30 TEMP=1553 RHO=0.034 GAMA=1.25
$SEND
$SAVE $ KEEP PREVIOUS INPUTS EXCEPT FOR FOLLOWING VALUES
$COMM
CHANGE TRAJECTORY PRINT OPTION AND TITLE
$INFO
POPT=1,1,1,0,1 RUN='M203/M549 TABULAR B/R DATA'
$SPROP $ NO CHANGES IN FIRST PROPELLANT DECK
$SPROP $ CHANGE BURNING RATE SPECIFICATION METHOD
NTBL=4 PR4L=1000,5000,10000,30000 BR4L=0.5102,1.577,2.563,5.536
$COMM
ADD PARAMETRIC VARIATION ON CHARGE WEIGHT FOR SECOND PROPELLANT
$SPARA
VARY='CHWT' DECK='PROP' NTH=2 FROM=25 TO=27 BY=0.2
$SEND

```

Producing the following output:

ERRTOL= 4.768372E-07

```
CARD 1 --> $COMM
CARD 2 --> IBHVG2 BENCHMARK TEST CASE 3
CARD 3 -->
CARD 4 --> - SHOW TRAJECTORY PRINT OPTIONS, GUN TUBE GAUGE PRINTS, BLOWDOWN PHASE
CARD 5 --> - SHOW 'SAVE' FEATURE ; CHANGE PRINT OPTION AND BURN-RATE INPUTS;
CARD 6 --> - SHOW SMALL PARAMETRIC STUDY ON CHARGE WEIGHT FOR PROPELLANT 2, AND
CARD 7 --> USE DEFAULT OUTPUTS FOR CHARGE WEIGHT VARIATIONS (PMAX,VMU2,PMU2,XB2=1)
CARD 8 -->
CARD 9 --> 'TDIS' VALUES USED WITH SPECIAL PRINT OPTION - POPT(2)=2
CARD 10 --> $TDIS
CARD 11 --> SHOW='TIME' REMK='TIME (MS)';
CARD 12 --> $TDIS
CARD 13 --> SHOW='TRAV' REM1='TRAVEL (INCHES)';
CARD 14 --> $TDIS
CARD 15 --> SHOW='VEL' REM1='VELOCITY (IN/SEC)' MULT=12. $ IF MULT=1, THEN VEL=FT/SEC
CARD 16 --> $TDIS
CARD 17 --> SHOW='ACCL' REMK='ACCEL (GRAV)';
CARD 18 --> $TDIS
CARD 19 --> SHOW='FRCR' REM1='FRICTION (PSI)';
CARD 20 --> $TDIS
CARD 21 --> SHOW='BRCH' REM1='BREECH PRESSURE (PSI)';
CARD 22 --> $TDIS
CARD 23 --> SHOW='BASE' REM1='BASE PRESSURE (PSI)';
CARD 24 --> $TDIS
CARD 25 --> SHOW='TBAR' REM1='MEAN TEMP (DEG K)';
CARD 26 --> $TDIS
CARD 27 --> SHOW='WTB(1)' REM1='PROP 1 (LBS BRND)';
CARD 28 --> $TDIS
CARD 29 --> SHOW='WTB(2)' REMK='PROP 2 (LBS BRND)';
CARD 30 --> $TDIS
CARD 31 --> SHOW='WTB(3)' REM1='PROP 3 (LBS BRND)';
CARD 32 -->
CARD 33 --> SHEAT
CARD 34 --> TSHL=0.00384
CARD 35 -->
CARD 36 --> $COMM
CARD 37 --> GET MAXIMUM PRESSURES AT GAGE LOCATIONS - BREECH,
CARD 38 --> ORIGINAL PROJECTILE BASE, AND AT 10 INCHES OF TRAVEL
CARD 39 --> $GUN
CARD 40 --> NAME='155-MM 198' CHAM=1150 GRVE=6.2 LAND=6.1
CARD 41 --> G/L=1.66 TRAV=205. TWST=20 NGAG=3 GLOC=-30.,0.,10. CLEN=30.
CARD 42 -->
CARD 43 --> $PROJ
CARD 44 --> NAME='M549A1' PRWT=96
CARD 45 --> $RES1
CARD 46 --> NPTS=7 TRAV=0,0.4,1.,1.55,2.05,4.5,200
CARD 47 --> PRES=250,3350,4950,3625,3250,2500,1500
CARD 48 -->
CARD 49 --> $COMM
CARD 50 --> INVOKE SPECIAL TRAJECTORY PRINT OPTION - POPT(2)=2
CARD 51 --> CALCULATE AND PRINT BLOWDOWN PHASE - POPT(4)=1
CARD 52 --> $INFO
CARD 53 --> POPT=1,2,1,1,0
CARD 54 --> RUN='NEAR-STANDARD M203/M549'
CARD 55 -->
```

CARD 56 --> SPRIN
 CARD 57 --> NA 'LK POWDER' CHWT=0.0154
 CARD 58 --> G 25 FORC=96000 COV=30 TEMP=2000
 CARD 59 --> SPRO
 CARD 60 --> NA 'LK POWDER' CHWT=0.2976 GRAN='ORD'
 CARD 61 --> LEN=0.198 DIAM=0.098
 CARD 62 --> RHO=0.06 GAMA=1.25 FORC=96000 COV=30 TEMP=2000
 CARD 63 --> ALPH=0.0 BETA=50 EROS=0.00000
 CARD 64 --> SPROP
 CARD 65 --> NAME='M30A1' CHWT=26.2 GRAN='7PF'
 CARD 66 --> LEN=0.9481 DIAM=0.4173 PD=0.0378 W1=0.078975 W0=0.078975
 CARD 67 --> RHO=0.0572 GAMA=1.243 FORC=356400 COV=28.1 TEMP=3040
 CARD 68 --> NTBL=0 ALPH=0.701 BETA=0.004025
 CARD 69 --> SPROP
 CARD 70 --> NAME='NC TUBE' CHWT=0.5 GRAN='1PF' NTBL=0 ALPH= A=50
 CARD 71 --> LEN=28 DIAM=1.5 PD=1.25 WEB=0.125
 CARD 72 --> FORC=180000 COV=30 TEMP=1553 RHO=0.034 GAMA=1.25
 CARD 73 --> SEND

TYPE: 155-MM 198	
GROOVE DIAMETER (IN):	6.200
TWIST (CALS/TURN):	20.0
SHELL THICKNESS (IN):	0.003840
INITIAL SHELL TEMP (°F):	203
CHAMBER VOLUME (IN ³):	1150.00
LAND DIAMETER (IN):	6.100
BORE AREA (IN ²):	29.8275
SHELL CP (IN-LB/LB-K):	1048.0
SHR. NO. (IN-LB/IN ² -K):	0.00000
TRAVEL (IN):	205.00
GROOVE/LAND RATIO (-):	1.660
HEAT-LOSS OPTION:	1
SHELL DENSITY (LB/IN ³):	0.2840

NO. PAGES:

I	LOCATION (IN)	I	LOCATION (IN)	I	LOCATION (IN)
1	-30.00	2	0.00	3	10.00

- PROJECTILE -

TYPE: 4649A1

- RESISTANCE -

WEIGHT PREDICTOR OPTION: 0

94

AIR RESISTANCE OPTION:		1
1	TRAVEL (IN)	PRESSURE (PSI)
1	0.00	250.
2	0.40	3350.
3	1.00	4950.

----- GENERAL -----

```

MAX TIME STEP ($): 0.000100
PRINT STEP ($): 1 2 1 1 0 1
STORE OPTION: 0
GRADIENT MODEL: LAGRANGIAN
MAX RELATIVE ERROR (-): 0.000000
CONSTANT-PRESSURE OPTION: 0
0.002000

```

RECOIL -

RECOIL OPTION:	0	TYPE:	RECOILING WEIGHT (LB):	0.

PRIMER -

TYPE: BLK POWDER	GAMMA (-):	1.2500	FORCE (FT-LB/LB):	94000.
COVOLUME (IN3/LB):	FLAME TEMP (K):	2000.0	WEIGHT (LB):	0.015400

- CHARGE 1 -

TYPE: BLK POWDER
EROSIVE COEFF (-):
GRAIN LENGTH (IN):

0.000000
0.19800

GRAINS:
CHARGE IGM CODE:
GRAIN DIAMETER (IN):

3321.0
0.09800

WEIGHT (LB):
CHARGE IGM AT (\$):

0.2976
0.00000E+00

PROPERTIES AT LAYER BOUNDARIES OF END SURFACES PROPERTIES AT LAYER BOUNDARIES OF LAT SURFACES

AT DEPTH (IN):
ADJACENT LAYER WT %:
DENSITY (LB/IN3):
GAMMA (-):
FORCE (FT-LB/LB):
COWOLUME (IN3/LB):
FLAME TEMP (K):
BURNING RATE EXPS:
BURNING RATE COEFFS:

1ST 2ND 3RD 4TH

0.00000
100.000
0.06300
1.2500
96000.
30.000
2000.0
0.0000
50.0000000

1ST 2ND 3RD 4TH

0.00000
100.000
0.06000
1.2500
96000.
30.000
2000.0
0.0000
50.0000000

[illegible]

PROPERTIES AT LAYER BOUNDARIES OF		LAT SURFACES
1ST	2ND	3RD
AT DEPTH (IN):	-----	-----
ADJACENT LAYER WT %:	-----	-----
DENSITY (LB/IN3):	-----	-----
GAMMA (-):	-----	-----
FORCE (FT-LB/LB):	-----	-----
COVOLUME (IN3/LB):	-----	-----
FLAME TEMP (K):	-----	-----
BURNING RATE EXPS:	-----	-----
BURNING RATE COEFFS:	-----	-----
		0.00000
		100.000
		0.05720
		1.2430
		356400.
		28.500
		3040.0
		0.7010
		0.0040250

----- CHARGE 3 -----

TYPE: MC TUBE	GRAINS:	0.97268	1PF	WEIGHT (LB):	0.5000
EXPLOSIVE COEFF (-):	CHARGE IGM CODE:		0	CHARGE IGM AT (S):	0.00000E+00
GRAIN LENGTH (IN):	GRAIN DIAMETER (IN):		1.50000	PERF DIAMETER (IN):	1.25000
INNER WEB (IN):	WEB RATIO:		1.0000		

	PROPERTIES AT LAYER BOUNDARIES OF PERF SURFACES	PROPERTIES AT LAYER BOUNDARIES OF END SURFACES
	1ST 2ND 3RD 4TH	1ST 2ND 3RD 4TH
AT DEPTH (IN):	---	---
ADJACENT LAYER UT %:	---	---
DENSITY (LB/IN3):	---	---
GAMMA (-):	---	---
FORCE (FT-LB/LB):	---	---
COVOLUME (IN3/LB):	---	---
FLAME TEMP (K):	---	---
BURNING RATE EXPS:	---	---
BURNING RATE COEFFS:	---	---

	PROPERTIES AT LAYER BOUNDARIES OF LAT SURFACES
	1ST 2ND 3RD 4TH
AT DEPTH (IN):	---
ADJACENT LAYER UT %:	---
DENSITY (LB/IN3):	---
GAMMA (-):	---
FORCE (FT-LB/LB):	---
COVOLUME (IN3/LB):	---
FLAME TEMP (K):	---
BURNING RATE EXPS:	---
BURNING RATE COEFFS:	---

TRAJECTORY VARIABLES:										
TIME (MS)										
TRAVEL (INCHES)										
VELOCITY (IN/SEC)										
ACCEL (GRAV)										
FRICTION (PSI)										
BREECH PRESSURE (PSI)										
MEAN TEMP (DEG K)										
PROP 1 (LBS BRNED)										
PROP 2 (LBS BRNED)										
PROP 3 (LBS BRNED)										
1/	2/	3/	4/	5/	6/	7/	8/	9/	10/	11/
0.95191E-01	0.45392E-09	0.	0.	26.407	26.407	26.407	2000.0	0.	0.	0.
SHOT-START PRESSURE ACHIEVED	0.	0.	0.28444E-03	250.00	250.00	250.00	1930.6	0.66666E-01	0.54050E-02	0.22943E-01
0.10000	0.71886E-08	0.31346E-02	3.3780	250.00	262.40	260.87	1933.1	0.69755E-01	0.59065E-02	0.24102E-01
0.20000	0.53071E-04	1.5284	76.405	250.41	530.92	496.32	1985.2	0.12812	0.18176E-01	0.48194E-01
0.30000	0.40276E-03	5.9640	153.83	253.12	817.89	748.23	2034.7	0.17603	0.35912E-01	0.72275E-01
0.40000	0.13490E-02	13.462	234.78	260.45	1122.4	1016.1	2081.2	0.21442	0.58764E-01	0.96344E-01
0.50000	0.32013E-02	24.146	318.69	274.81	1444.9	1300.6	2125.2	0.24423	0.86558E-01	0.12041
0.60000	0.62869E-02	38.123	405.13	298.72	1786.1	1602.7	2167.1	0.26641	0.11922	0.14446
0.70000	0.10959E-01	55.483	493.77	334.77	2147.6	1924.1	2207.1	0.28189	0.15673	0.16850
0.80000	0.17496E-01	76.306	594.35	385.62	2531.1	2266.5	2245.3	0.29162	0.19914	0.19253
0.90000	0.35238E-01	122.74	751.66	523.10	3282.9	2942.5	2309.4	0.29764	0.28805	0.23576
PROPELLANT 1 BURNED OUT										
1.0000	0.37751E-01	128.62	770.58	542.57	3371.8	3022.9	2316.2	0.29764	0.29895	0.24056
1.1000	0.52164E-01	160.25	866.91	654.27	3437.2	3444.7	2348.6	0.29764	0.35662	0.26456
1.2000	0.69924E-01	195.65	965.73	791.93	4337.7	3900.4	2378.9	0.29764	0.41972	0.28854
1.3000	0.91421E-01	234.90	1066.6	958.51	4874.5	4391.6	2407.2	0.29764	0.48849	0.31252
1.4000	0.11704	278.09	1168.9	1157.0	5448.8	4919.5	2433.6	0.29764	0.56314	0.33649
1.5000	0.14717	325.25	1272.1	1390.6	6061.5	5485.5	2458.5	0.29764	0.64392	0.36045
1.6000	0.18222	376.40	1375.8	1642.2	6713.9	6090.9	2481.7	0.29764	0.73105	0.38440
1.7000	0.22259	431.57	1479.3	1975.0	7406.9	6737.0	2503.6	0.29764	0.82480	0.40833
1.8000	0.26867	490.72	1582.1	2332.2	8141.4	7425.0	2524.0	0.29764	0.92539	0.43226
1.9000	0.32086	553.82	1683.5	2736.7	8918.3	8156.0	2543.2	0.29764	1.0331	0.45618
2.0000	0.37956	620.80	1783.0	3191.6	9738.6	8931.2	2561.2	0.29764	1.1482	0.48009
2.0833	0.43373	680.01	1912.0	3440.0	10460.	9594.7	2575.6	0.29764	1.2499	0.49934
PROPELLANT 3 BURNED OUT										
2.1000	0.44517	692.42	1940.7	3470.4	10596.	9717.6	2580.5	0.29764	1.2708	0.49934
2.2000	0.51827	770.78	2116.2	3665.4	11436.	10477.	2607.9	0.29764	1.4010	0.49934
2.3000	0.59955	856.03	2297.1	3882.1	12317.	11277.	2633.0	0.29764	1.5385	0.49934
2.4000	0.68971	948.36	2483.0	4122.6	13240.	12116.	2655.8	0.29764	1.6838	0.49934
2.5000	0.78947	1048.0	2673.3	4388.6	14205.	12994.	2676.6	0.29764	1.8371	0.49934
2.6000	0.89956	1155.0	2867.4	4682.1	15211.	13913.	2695.5	0.29764	1.9986	0.49934
2.7000	1.0207	1269.8	3094.4	4900.1	16263.	14861.	2712.6	0.29764	2.1685	0.49934
2.8000	1.1539	1396.9	3485.4	4579.2	17378.	15800.	2727.9	0.29764	2.3472	0.49934
2.9000	1.3006	1529.4	3896.7	4225.6	18534.	16770.	2741.6	0.29764	2.5349	0.49934
3.0000	1.4624	1698.3	4327.9	3836.1	19728.	17768.	2753.8	0.29764	2.7317	0.49934
3.1000	1.6408	1873.9	4736.9	3556.9	20950.	18808.	2764.5	0.29764	2.9379	0.49934
3.2000	1.8376	2064.2	5116.4	3409.3	22196.	19880.	2773.7	0.29764	3.1537	0.49934
3.3000	2.0542	2269.4	5506.4	3248.7	23468.	20979.	2781.5	0.29764	3.3792	0.49934
3.4000	2.2920	2469.3	5877.0	3175.9	24756.	22075.	2788.0	0.29764	3.6145	0.49934
3.5000	2.5525	2723.7	6253.6	3096.2	26060.	23228.	2793.2	0.29764	3.8598	0.49934
3.6000	2.8372	2972.6	6634.9	3009.0	27373.	24368.	2797.2	0.29764	4.1152	0.49934
3.7000	3.1475	3236.4	7019.1	2914.0	28689.	25511.	2800.0	0.29764	4.3807	0.49934
3.8000	3.4850	3515.1	7404.7	2810.7	30002.	26649.	2801.7	0.29764	4.6563	0.49934

TRAJECTORY VARIABLES:										
1/	2/	3/	4/	5/	6/	7/	8/	9/	10/	11/
TRAJ 1	TRAJ 1	TRAJ 1	TRAJ 1	TRAJ 1	TRAJ 1	TRAJ 1	TRAJ 1	TRAJ 1	TRAJ 1	TRAJ 1
TIME	TIME	TIME	TIME	TIME	TIME	TIME	TIME	TIME	TIME	TIME
TRAV	TRAV	TRAV	TRAV	TRAV	TRAV	TRAV	TRAV	TRAV	TRAV	TRAV
VEL	VEL	VEL	VEL	VEL	VEL	VEL	VEL	VEL	VEL	VEL
ACCL	ACCL	ACCL	ACCL	ACCL	ACCL	ACCL	ACCL	ACCL	ACCL	ACCL
FRIC	FRIC	FRIC	FRIC	FRIC	FRIC	FRIC	FRIC	FRIC	FRIC	FRIC
BRCH	BRCH	BRCH	BRCH	BRCH	BRCH	BRCH	BRCH	BRCH	BRCH	BRCH
BASE	BASE	BASE	BASE	BASE	BASE	BASE	BASE	BASE	BASE	BASE
TBAR	TBAR	TBAR	TBAR	TBAR	TBAR	TBAR	TBAR	TBAR	TBAR	TBAR
VTB(1)	VTB(1)	VTB(1)	VTB(1)	VTB(1)	VTB(1)	VTB(1)	VTB(1)	VTB(1)	VTB(1)	VTB(1)
VTB(2)	VTB(2)	VTB(2)	VTB(2)	VTB(2)	VTB(2)	VTB(2)	VTB(2)	VTB(2)	VTB(2)	VTB(2)
VTB(3)	VTB(3)	VTB(3)	VTB(3)	VTB(3)	VTB(3)	VTB(3)	VTB(3)	VTB(3)	VTB(3)	VTB(3)
TIME (MS)	TIME (MS)	TIME (MS)	TIME (MS)	TIME (MS)	TIME (MS)	TIME (MS)	TIME (MS)	TIME (MS)	TIME (MS)	TIME (MS)
TRAVEL (INCHES)	TRAVEL (INCHES)	TRAVEL (INCHES)	TRAVEL (INCHES)	TRAVEL (INCHES)	TRAVEL (INCHES)	TRAVEL (INCHES)	TRAVEL (INCHES)	TRAVEL (INCHES)	TRAVEL (INCHES)	TRAVEL (INCHES)
VELOCITY (IN/SEC)	VELOCITY (IN/SEC)	VELOCITY (IN/SEC)	VELOCITY (IN/SEC)	VELOCITY (IN/SEC)	VELOCITY (IN/SEC)	VELOCITY (IN/SEC)	VELOCITY (IN/SEC)	VELOCITY (IN/SEC)	VELOCITY (IN/SEC)	VELOCITY (IN/SEC)
ACCEL (GRAV)	ACCEL (GRAV)	ACCEL (GRAV)	ACCEL (GRAV)	ACCEL (GRAV)	ACCEL (GRAV)	ACCEL (GRAV)	ACCEL (GRAV)	ACCEL (GRAV)	ACCEL (GRAV)	ACCEL (GRAV)
FRIC (PSI)	FRIC (PSI)	FRIC (PSI)	FRIC (PSI)	FRIC (PSI)	FRIC (PSI)	FRIC (PSI)	FRIC (PSI)	FRIC (PSI)	FRIC (PSI)	FRIC (PSI)
BRECH PRESSURE (PSI)	BRECH PRESSURE (PSI)	BRECH PRESSURE (PSI)	BRECH PRESSURE (PSI)	BRECH PRESSURE (PSI)	BRECH PRESSURE (PSI)	BRECH PRESSURE (PSI)	BRECH PRESSURE (PSI)	BRECH PRESSURE (PSI)	BRECH PRESSURE (PSI)	BRECH PRESSURE (PSI)
BASE PRESSURE (PSI)	BASE PRESSURE (PSI)	BASE PRESSURE (PSI)	BASE PRESSURE (PSI)	BASE PRESSURE (PSI)	BASE PRESSURE (PSI)	BASE PRESSURE (PSI)	BASE PRESSURE (PSI)	BASE PRESSURE (PSI)	BASE PRESSURE (PSI)	BASE PRESSURE (PSI)
MEAN TEMP (DEG K)	MEAN TEMP (DEG K)	MEAN TEMP (DEG K)	MEAN TEMP (DEG K)	MEAN TEMP (DEG K)	MEAN TEMP (DEG K)	MEAN TEMP (DEG K)	MEAN TEMP (DEG K)	MEAN TEMP (DEG K)	MEAN TEMP (DEG K)	MEAN TEMP (DEG K)
PROP 1 (LBS BRNED)	PROP 1 (LBS BRNED)	PROP 1 (LBS BRNED)	PROP 1 (LBS BRNED)	PROP 1 (LBS BRNED)	PROP 1 (LBS BRNED)	PROP 1 (LBS BRNED)	PROP 1 (LBS BRNED)	PROP 1 (LBS BRNED)	PROP 1 (LBS BRNED)	PROP 1 (LBS BRNED)
PROP 2 (LBS BRNED)	PROP 2 (LBS BRNED)	PROP 2 (LBS BRNED)	PROP 2 (LBS BRNED)	PROP 2 (LBS BRNED)	PROP 2 (LBS BRNED)	PROP 2 (LBS BRNED)	PROP 2 (LBS BRNED)	PROP 2 (LBS BRNED)	PROP 2 (LBS BRNED)	PROP 2 (LBS BRNED)
PROP 3 (LBS BRNED)	PROP 3 (LBS BRNED)	PROP 3 (LBS BRNED)	PROP 3 (LBS BRNED)	PROP 3 (LBS BRNED)	PROP 3 (LBS BRNED)	PROP 3 (LBS BRNED)	PROP 3 (LBS BRNED)	PROP 3 (LBS BRNED)	PROP 3 (LBS BRNED)	PROP 3 (LBS BRNED)
3.9000	3.8510	3808.7	7789.8	2698.7	31304.	27777.	2802.2	0.29764	4.9419	0.49934
4.0000	4.2472	4117.1	8172.6	2577.4	32589.	28886.	2801.7	0.29764	5.2376	0.49934
4.1000	4.6750	4440.1	8536.2	2499.1	33847.	29981.	2800.3	0.29764	5.5431	0.49934
4.2000	5.1357	4776.4	8869.4	2496.7	35048.	31052.	2797.8	0.29764	5.8585	0.49934
4.3000	5.6307	5125.4	9191.7	2494.2	36250.	32087.	2794.5	0.29764	6.1834	0.49934
4.4000	6.1612	5486.6	9501.5	2491.5	37385.	33082.	2790.3	0.29764	6.5176	0.49934
4.5000	6.7284	5859.5	9796.9	2488.6	38467.	34031.	2785.2	0.29764	6.8609	0.49934
4.6000	7.3334	6243.5	10076.	2485.5	39491.	34929.	2779.5	0.29764	7.2131	0.49934
4.7000	7.9774	6637.9	10339.	2482.2	40452.	35770.	2773.0	0.29764	7.5736	0.49934
4.8000	8.6613	7042.2	10582.	2478.7	41344.	36552.	2765.9	0.29764	7.9423	0.49934
4.9000	9.3861	7455.5	10807.	2475.0	42165.	37271.	2758.2	0.29764	8.3187	0.49934
4.9805	10.0000	7794.3	10972.	2471.9	42772.	37803.	2751.7	0.29764	8.6270	0.49934
5.0000	10.153	7877.0	11011.	2471.1	42911.	37925.	2750.0	0.29764	8.7023	0.49934
5.1000	10.962	8306.1	11194.	2466.9	43580.	38512.	2741.3	0.29764	9.0929	0.49934
5.2000	12.814	8741.8	11356.	2462.6	44172.	39030.	2732.2	0.29764	9.4899	0.49934
5.3000	12.710	9183.4	11497.	2458.0	44686.	39480.	2722.7	0.29764	9.8928	0.49934
5.4000	13.651	9630.0	11616.	2453.2	45122.	39862.	2712.9	0.29764	10.301	0.49934
5.5000	14.636	10081.	11715.	2448.2	45481.	40176.	2702.7	0.29764	10.715	0.49934
5.6000	15.667	10535.	11794.	2442.9	45766.	40425.	2692.4	0.29764	11.133	0.49934
5.7000	16.743	10992.	11852.	2437.4	45978.	40611.	2681.9	0.29764	11.555	0.49934
5.8000	17.864	11451.	11892.	2431.6	46121.	40735.	2671.2	0.29764	11.981	0.49934
5.9000	19.034	11911.	11914.	2425.7	46197.	40802.	2660.4	0.29764	12.410	0.49934
5.9715	19.897	12240.	11920.	2421.2	46212.	40815.	2652.7	0.29764	12.718	0.49934
LOCAL PRESSURE MAX DETECTED										
6.0000	20.248	12371.	11919.	2419.4	46210.	40813.	2649.6	0.29764	12.842	0.49934
6.1000	21.508	12832.	11908.	2413.0	46164.	40772.	2638.7	0.29764	13.276	0.49934
6.2000	22.814	13291.	11882.	2406.3	46064.	40683.	2627.8	0.29764	13.712	0.49934
6.3000	24.166	13750.	11842.	2399.4	45912.	40550.	2616.9	0.29764	14.150	0.49934
6.4000	25.564	14206.	11789.	2392.3	45714.	40375.	2606.1	0.29764	14.589	0.49934
6.5000	27.007	14661.	11725.	2384.9	45472.	40163.	2595.3	0.29764	15.029	0.49934
6.6000	28.496	15112.	11650.	2377.3	45192.	39917.	2584.6	0.29764	15.469	0.49934
6.7000	30.029	15561.	11566.	2369.4	44877.	39640.	2574.0	0.29764	15.910	0.49934
6.8000	31.608	16006.	11474.	2361.3	44531.	39335.	2563.5	0.29764	16.351	0.49934
6.9000	33.230	16447.	11373.	2353.0	44157.	39007.	2553.2	0.29764	16.791	0.49934
7.0000	34.897	16885.	11267.	2344.5	43759.	38657.	2543.0	0.29764	17.231	0.49934
7.1000	36.607	17318.	11154.	2335.8	43339.	38288.	2532.9	0.29764	17.671	0.49934
7.2000	38.361	17747.	11037.	2326.8	42902.	37904.	2523.0	0.29764	18.109	0.49934
7.3000	40.157	18171.	10915.	2317.6	42448.	37506.	2513.2	0.29764	18.546	0.49934
7.4000	41.995	18590.	10790.	2308.2	41983.	37096.	2503.6	0.29764	18.982	0.49934
7.5000	43.874	19005.	10663.	2298.6	41506.	36678.	2494.2	0.29764	19.416	0.49934
7.6000	45.795	19414.	10533.	2288.8	41021.	36252.	2484.9	0.29764	19.849	0.49934
7.7000	47.757	19819.	10401.	2278.7	40530.	35820.	2475.8	0.29764	20.280	0.49934
7.8000	49.759	20218.	10268.	2268.5	40034.	35384.	2466.9	0.29764	20.709	0.49934

TRAJECTORY VARIABLES:

TIME (MS)
TRAVEL (INCHES)
VELOCITY (IN/SEC)
ACCEL (GRAV)
FRICTION (PSI)
BREECH PRESSURE (PSI)
BASE PRESSURE (PSI)
MEAN TEMP (DEG K)
PROP 1 (LBS BRND)
PROP 2 (LBS BRND)
PROP 3 (LBS BRND)

TRAJ 1 TIME
TRAJ 1 TRAV
TRAJ 1 VEL
TRAJ 1 ACCL
TRAJ 1 FRCR
TRAJ 1 BRCH
TRAJ 1 BASE
TRAJ 1 TBAR
TRAJ 1 UTB(1)
TRAJ 1 UTB(2)
TRAJ 1 UTB(3)

/ 1/	/ 2/	/ 3/	/ 4/	/ 5/	/ 6/	/ 7/	/ 8/	/ 9/	/ 10/	/ 11/
7.9000	51.801	20612.	10134.	2258.1	39535.	34946.	2458.1	0.29764	21.136	0.49934
8.0000	53.881	21001.	10000.	2247.4	39034.	34506.	2449.5	0.29764	21.561	0.49934
8.1000	56.001	21385.	9865.2	2236.6	38533.	34066.	2441.1	0.29764	21.984	0.49934
8.2000	58.158	21764.	9732.3	2225.5	38033.	33626.	2432.8	0.29764	22.405	0.49934
8.3000	60.353	22137.	9574.7	2214.3	37445.	33110.	2423.7	0.29764	22.783	0.49934
8.4000	62.585	22503.	9386.9	2202.9	36747.	32496.	2413.3	0.29764	23.103	0.49934
8.5000	64.854	22862.	9134.7	2191.3	35995.	31836.	2402.3	0.29764	23.386	0.49934
8.6000	67.157	23213.	8974.1	2179.5	35212.	31148.	2390.9	0.29764	23.640	0.49934
8.7000	69.496	23556.	8758.7	2167.5	34412.	30445.	2379.2	0.29764	23.871	0.49934
8.8000	71.848	23890.	8541.0	2155.4	33602.	29735.	2367.4	0.29764	24.080	0.49934
8.9000	74.273	24216.	8322.8	2143.1	32791.	29022.	2355.4	0.29764	24.271	0.49934
9.0001	76.711	24533.	8105.5	2130.6	31983.	28313.	2343.3	0.29764	24.444	0.49934
9.1001	79.180	24842.	7890.2	2118.0	31182.	27609.	2331.1	0.29764	24.603	0.49934
9.2001	81.679	25143.	7677.6	2105.2	30391.	26914.	2318.9	0.29764	24.747	0.49934
9.3001	84.208	25435.	7468.4	2092.3	29612.	26230.	2306.7	0.29764	24.879	0.49934
9.4001	86.766	25720.	7263.1	2079.2	28847.	25558.	2294.5	0.29764	24.998	0.49934
9.5001	89.352	25997.	7062.1	2066.0	28098.	24900.	2282.4	0.29764	25.107	0.49934
9.6001	91.965	26266.	6865.6	2052.6	27365.	24256.	2270.2	0.29764	25.205	0.49934
9.7001	94.605	26527.	6673.9	2039.1	26649.	23627.	2258.1	0.29764	25.294	0.49934
9.8001	97.270	26782.	6487.1	2025.5	25952.	23014.	2246.1	0.29764	25.375	0.49934
9.9001	99.961	27029.	6306.0	2011.7	25275.	22419.	2234.1	0.29764	25.448	0.49934
10.000	102.68	27269.	6130.8	1997.8	24620.	21843.	2222.4	0.29764	25.517	0.49934
10.100	105.41	27503.	5961.4	1983.8	23985.	21286.	2210.7	0.29764	25.581	0.49934
10.200	108.18	27730.	5797.5	1969.7	23371.	20746.	2199.2	0.29764	25.640	0.49934
10.300	110.96	27951.	5639.2	1955.4	22777.	20224.	2187.8	0.29764	25.695	0.49934
10.400	113.77	28166.	5486.1	1941.1	22203.	19719.	2176.6	0.29764	25.746	0.49934
10.500	116.59	28375.	5338.3	1926.6	21647.	19230.	2165.5	0.29764	25.793	0.49934
10.600	119.44	28578.	5195.4	1912.1	21109.	18757.	2154.5	0.29764	25.836	0.49934
10.700	122.31	28776.	5057.3	1897.4	20589.	18299.	2143.7	0.29764	25.876	0.49934
10.800	125.20	28969.	4923.9	1882.6	20086.	17857.	2133.0	0.29764	25.913	0.49934
10.900	128.10	29157.	4795.0	1867.8	19600.	17429.	2122.4	0.29764	25.947	0.49934
11.000	131.03	29340.	4670.5	1852.8	19129.	17014.	2111.9	0.29764	25.979	0.49934
11.100	133.97	29518.	4550.2	1837.8	18674.	16613.	2101.6	0.29764	26.007	0.49934
11.200	136.93	29691.	4433.9	1822.6	18233.	16225.	2091.4	0.29764	26.033	0.49934
11.300	139.91	29861.	4321.6	1807.4	17807.	15850.	2081.3	0.29764	26.057	0.49934
11.400	142.90	30025.	4213.0	1792.1	17394.	15486.	2071.3	0.29764	26.078	0.49934
11.500	145.91	30186.	4106.0	1776.7	16995.	15134.	2061.5	0.29764	26.097	0.49934
11.600	148.94	30343.	4006.5	1761.2	16608.	14794.	2051.8	0.29764	26.114	0.49934
11.700	151.98	30496.	3908.4	1745.6	16233.	14463.	2042.1	0.29764	26.129	0.49934
11.800	155.04	30645.	3813.5	1730.0	15870.	14144.	2032.6	0.29764	26.143	0.49934
11.900	158.11	30791.	3721.7	1714.3	15519.	13834.	2023.2	0.29764	26.155	0.49934
12.000	161.20	30933.	3632.9	1698.5	15178.	13533.	2013.9	0.29764	26.165	0.49934
12.100	164.30	31071.	3547.1	1682.6	14849.	13242.	2004.7	0.29764	26.173	0.49934
12.200	167.41	31207.	3464.0	1666.7	14529.	12960.	1995.6	0.29764	26.180	0.49934

CONDITIONS AT:	PMAX	MUZZLE
TIME (MS):	5.972	13.377
TRAVEL (IN):	19.90	205.00
VELOCITY (FT/S):	1020.	2716.
ACCELERATION (G):	11920.	2660.
BREECH PRESS (PSI):	46212.	11421.
MEAN PRESS (PSI):	44413.	11019.
BASE PRESS (PSI):	40815.	10216.
MEAN TEMP (K):	2653.	1897.
Z CHARGE 1 (-):	1.000	1.000
Z CHARGE 2 (-):	0.485	1.000
Z CHARGE 3 (-):	1.000	1.000

GAGE	AT (IN)	PMAX (PSI)
	WRT SOM	
1	-30.00	46212.
2	0.00	43943.
3	10.00	42699.

ENERGY BALANCE SUMMARY	IN-LB	%
TOTAL CHEMICAL:	466804736.	100.00
(1) INTERNAL GAS:	294272512.	63.04
(2) WORK AND LOSSES:	172532304.	36.96
(A) PROJECTILE KINETIC:	131932192.	28.26
(B) GAS KINETIC:	12374597.	2.65
(C) PROJECTILE ROTATIONAL:	1627647.	0.35
(D) FRICTIONAL WORK TO TUBE:	0.	0.00
(E) OTHER FRICTIONAL WORK:	12313598.	2.64
(F) WORK DONE AGAINST AIR:	621945.	0.13
(G) HEAT CONVECTED TO BORE:	13662321.	2.93
(H) RECOIL ENERGY:	0.	0.00

LOADING DENSITY (G/CM3):	0.650
CHARGE WT/PROJECTILE WT:	0.281
PIEZOMETRIC EFFICIENCY:	0.467
EXPANSION RATIO:	6.317

TIME (MS)	RAREFACTION WAVE LOC'N (IN)	BREECH PRESS (PSI)	MOMENTUM (LB-SEC)	RECOIL TRAVEL (IN)	RECOIL VEL (FT/S)
13.377	243.55	11421.	9236.	0.00	0.00
13.500	242.66	11166.	9277.	0.00	0.00
14.000	238.57	10217.	9436.	0.00	0.00
14.500	233.78	9392.	9582.	0.00	0.00
15.000	228.29	8670.	9717.	0.00	0.00
15.500	222.13	8034.	9842.	0.00	0.00
16.000	215.30	7470.	9957.	0.00	0.00
16.500	207.84	6967.	10065.	0.00	0.00
17.000	199.75	6517.	10165.	0.00	0.00
17.500	191.05	6113.	10259.	0.00	0.00
18.000	181.75	5747.	10348.	0.00	0.00
18.500	171.88	5416.	10431.	0.00	0.00
19.000	161.45	5115.	10509.	0.00	0.00
19.500	150.48	4839.	10584.	0.00	0.00
20.000	138.97	4587.	10654.	0.00	0.00
20.500	126.95	4356.	10720.	0.00	0.00
21.000	114.42	4143.	10784.	0.00	0.00
21.500	101.41	3946.	10844.	0.00	0.00
22.000	87.91	3764.	10902.	0.00	0.00
22.500	73.95	3595.	10956.	0.00	0.00
23.000	59.53	3438.	11009.	0.00	0.00
23.500	44.66	3291.	11059.	0.00	0.00
24.000	29.36	3155.	11107.	0.00	0.00
24.500	13.63	3027.	11153.	0.00	0.00
24.923	0.00	2926.	11191.	0.00	0.00

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CARD 74 -->
CARD 75 --> $SAVE          $ KEEP PREVIOUS INPUTS EXCEPT FOR FOLLOWING VALUES
CARD 76 -->
CARD 77 --> $COMM
CARD 78 --> CHANGE TRAJECTORY PRINT OPTION AND TITLE
CARD 79 --> $INFO
CARD 80 --> POPT=1,1,0,1  RUN='M203/M549  TABULAR B/R DATA'
CARD 81 -->
CARD 82 --> $PROP          $ NO CHANGES IN FIRST PROPELLANT DECK
CARD 83 --> $PROP          $ CHANGE BURNING RATE SPECIFICATION METHOD
CARD 84 --> NTBL=4 PR4L=1000,5000,10000,30000 BR4L=0.5102,1.577,2.563,5.536
CARD 85 -->
CARD 86 --> $COMM
CARD 87 --> ADD PARAMETRIC VARIATION ON CHARGE WEIGHT FOR SECOND PROPELLANT
CARD 88 --> $PARA
CARD 89 --> VARY='CHWT' DECK='PROP' NTH=2 FROM=25 TO=27 BY=0.2
CARD 90 --> $END

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 - GUN TUBE -

 TYPE: 155-MM 198
 GROOVE DIAMETER (IN): 20.0
 TWIST (CAL/S/TURN): 0.003040
 SHELL THICKNESS (IN): 293.
 INITIAL SHELL TEMP (K): 3
 NO. GAGES: 3
 1 LOCATION (IN) 1 LOCATION (IN)
 1 -30.00 2 0.00

 - PROJECTILE -

 TYPE: M549A1

 - RESISTANCE -

 TOTAL WEIGHT (LB): 96.000 WEIGHT PREDICTOR OPTION: 0

 AIR RESISTANCE OPTION: 1
 1 TRAVEL (IN) PRESSURE (PSI)
 1 0.00 250.
 2 0.40 3350.
 3 1.00 4950.

 - GENERAL -

 MAX TIME STEP (S): 0.000100
 PRINT OPTIONS: 1 1 0 1 1
 GRADIENT MODEL: LAGRANGIAN

 - RECOIL -

 RECOIL OPTION: 0 TYPE:

 - PRIMER -

 TYPE: BLK POWDER
 COVOLUME (IN3/LB): 30.000
 CHAMBER VOLUME (IN3): 1150.00
 LAND DIAMETER (IN): 6.100
 BORE AREA (IN2): 29.8275
 SHELL CP (IN-LB/LB-K): 1848.0
 AIR NO (IN-LB/IN2-S-K): 0.06480
 CHAMBER LENGTH (IN): 30.00
 1 LOCATION (IN)
 2 0.00
 TRAVEL (IN): 205.00
 GROOVE/LAND RATIO (-): 1.660
 HEAT-LOSS OPTION: 1
 SHELL DENSITY (LB/IN3): 0.2840

 FRICTION TABLE LENGTH: 7
 1 TRAVEL (IN) PRESSURE (PSI)
 6 4.50 2500.
 7 200.00 1500.

 MAX RELATIVE ERROR (-): 0.00200
 CONSTANT-PRESSURE OPTION: 0

 RECOILING WEIGHT (LB): 0.

 FORCE (FT-LB/LB): 96000.
 WEIGHT (LB): 0.015400

TYPE: BLK POWDER
EROSIVE COEFF (-):
GRAIN LENGTH (IN):

GRAINS:	3321.0	CORD	0.2976
CHARGE	IGN CODE:	0	0.00000E+00
0.19000	GRAIN DIAMETER (IN):	0.05900	
			WEIGHT (LB):
			CHARGE IGN AT (S):

[illegible]

- CHARGE 2 -

TYPE: H30A1	GRAINS:	3532.8	7PF	WEIGHT (LB):	25.0000
EROSIVE COEFF (-):	CHARGE IGM CODE:		0	CHARGE IGM AT (S):	0.00000E+00
GRAIN LENGTH (IN):	GRAIN DIAMETER (IN):		0.41730	PERF DIAMETER (IN):	0.03390
INNER WEB (IN):	OUTER WEB (IN):		0.07898		

PROPERTIES AT LAYER BOUNDARIES OF PERF SURFACES		PROPERTIES AT LAYER BOUNDARIES OF END SURFACES			
	1ST	2ND	3RD	4TH	
AT DEPTH (IN):	---	---	---	---	---
ADJACENT LAYER WT %:	---	---	---	---	---
DENSITY (LB/IN3):	---	---	---	---	---
GAMMA (-):	---	---	---	---	---
FORCE (FT-LB/LB):	---	---	---	---	---
COVOLUME (IN3/LB):	---	---	---	---	---
FLAME TEMP (K):	---	---	---	---	---
MEAN PRESSURES (PSI):	---	---	---	---	---
MEAN PRESSURES (PSI):	---	---	---	---	---
MEAN PRESSURES (PSI):	---	---	---	---	---
BURNING RATES (IN/S):	---	---	---	---	---
BURNING RATES (IN/S):	---	---	---	---	---
BURNING RATES (IN/S):	---	---	---	---	---

PROPERTIES AT LAYER BOUNDARIES OF LAT SURFACES

	1ST	2ND	3RD	4TH
AT DEPTH (IN):	---	---	---	---
ADJACENT LAYER WT %:	---	---	---	---
DENSITY (LB/IN3):	---	---	---	---
GAMMA (-):	---	---	---	---
FORCE (FT-LB/LB):	---	---	---	---
COVOLUME (IN3/LB):	---	---	---	---
FLAME TEMP (K):	---	---	---	---
MEAN PRESSURES (PSI):	---	---	---	---
MEAN PRESSURES (PSI):	---	---	---	---
MEAN PRESSURES (PSI):	---	---	---	---
BURNING RATES (IN/S):	---	---	---	---
BURNING RATES (IN/S):	---	---	---	---
BURNING RATES (IN/S):	---	---	---	---

- CHARGE 3 -

TYPE: MC TUBE
 EROSION COEFF (-): 0.000000
 GRAIN LENGTH (IN): 28.00000
 INNER WEB (IN): 0.12500

GRAINS:
 CHARGE ICM CODE: 0.97268
 GRAIN DIAMETER (IN): 1.50000
 WEB RATIO: 1.00000

HEIGHT (LB): 0.5000
 CHARGE ICM AT (S): 0.00000E+00
 PERF DIAMETER (IN): 1.250

1PF 0
 1.50000
 1.00000

PROPERTIES AT LAYER BOUNDARIES OF PERF SURFACES

	1ST	2ND	3RD	4TH
AT DEPTH (IN):	---	---	---	---
ADJACENT LAYER WT %:	---	---	---	---
DENSITY (LB/IN3):	---	---	---	---
GAMMA (-):	---	---	---	---
FORCE (FT-LB/LB):	---	---	---	---
COVOLUME (IN3/LB):	---	---	---	---
FLAME TEMP (K):	---	---	---	---
BURNING RATE EXPS:	---	---	---	---
BURNING RATE COEFFS:	---	---	---	---

PROPERTIES AT LAYER BOUNDARIES OF END SURFACES

	1ST	2ND	3RD	4TH
AT DEPTH (IN):	---	---	---	---
ADJACENT LAYER WT %:	---	---	---	---
DENSITY (LB/IN3):	---	---	---	---
GAMMA (-):	---	---	---	---
FORCE (FT-LB/LB):	---	---	---	---
COVOLUME (IN3/LB):	---	---	---	---
FLAME TEMP (K):	---	---	---	---
BURNING RATE EXPS:	---	---	---	---
BURNING RATE COEFFS:	---	---	---	---

PROPERTIES AT LAYER BOUNDARIES OF LAT SURFACES

	1ST	2ND	3RD	4TH
AT DEPTH (IN):	---	---	---	---
ADJACENT LAYER WT %:	---	---	---	---
DENSITY (LB/IN3):	---	---	---	---
GAMMA (-):	---	---	---	---
FORCE (FT-LB/LB):	---	---	---	---
COVOLUME (IN3/LB):	---	---	---	---
FLAME TEMP (K):	---	---	---	---
BURNING RATE EXPS:	---	---	---	---
BURNING RATE COEFFS:	---	---	---	---

TIME (MS)	TRAV (IN)	VEL (FT/S)	ACC (G)	BREECH PRESS (PSI)	MEAN PRESS (PSI)	BASE PRESS (PSI)	MEAN TEMP (K)	FRAC BURN 1	FRAC BURN 2	FRAC BURN 3
0.000	0.00	0.	0.	26.	26.	26.	2000.	0.000	0.000	0.000
0.099	0.00	0.	0.	250.	250.	250.	1925.	0.233	0.000	0.048
SHOT-START PRESSURE ACHIEVED										
0.100	0.00	0.	0.	251.	251.	251.	1926.	0.234	0.000	0.048
0.200	0.00	0.	70.	505.	495.	475.	1973.	0.431	0.001	0.096
0.300	0.00	0.	143.	774.	753.	712.	2019.	0.591	0.001	0.145
0.400	0.00	1.	218.	1056.	1025.	962.	2062.	0.720	0.002	0.193
0.500	0.00	2.	296.	1353.	1310.	1225.	2104.	0.821	0.003	0.241
0.600	0.01	3.	375.	1664.	1610.	1502.	2143.	0.895	0.004	0.289
0.700	0.01	4.	455.	1991.	1926.	1794.	2181.	0.947	0.006	0.337
0.800	0.02	6.	537.	2336.	2258.	2104.	2217.	0.980	0.007	0.385
0.980	0.03	9.	686.	3006.	2907.	2709.	2278.	1.000	0.010	0.472
PROPELLANT 1 BURNED OUT										
1.000	0.03	10.	702.	3085.	2983.	2781.	2285.	1.000	0.011	0.481
1.100	0.05	12.	787.	3496.	3383.	3156.	2316.	1.000	0.013	0.529
1.200	0.06	15.	873.	3937.	3811.	3559.	2345.	1.000	0.015	0.577
1.300	0.08	18.	960.	4409.	4270.	3991.	2373.	1.000	0.018	0.625
1.400	0.11	21.	1048.	4911.	4760.	4457.	2399.	1.000	0.020	0.673
1.500	0.13	25.	1137.	5445.	5281.	4953.	2423.	1.000	0.023	0.721
1.600	0.17	28.	1224.	6012.	5836.	5483.	2446.	1.000	0.026	0.769
1.700	0.20	33.	1311.	6613.	6424.	6046.	2468.	1.000	0.030	0.817
1.800	0.24	37.	1397.	7248.	7047.	6644.	2488.	1.000	0.033	0.865
1.900	0.29	42.	1481.	7918.	7705.	7278.	2507.	1.000	0.037	0.912
2.000	0.34	46.	1562.	8624.	8399.	7948.	2526.	1.000	0.041	0.960
2.083	0.39	51.	1627.	9238.	9003.	8534.	2540.	1.000	0.044	1.000
PROPELLANT 3 BURNED OUT										
2.100	0.40	52.	1641.	9351.	9115.	8641.	2545.	1.000	0.045	1.000
2.200	0.47	57.	1788.	10061.	9804.	9288.	2574.	1.000	0.050	1.000
2.300	0.54	63.	1939.	10806.	10526.	9967.	2600.	1.000	0.055	1.000
2.400	0.62	70.	2094.	11585.	11283.	10679.	2624.	1.000	0.060	1.000
2.500	0.71	77.	2253.	12399.	12074.	11424.	2646.	1.000	0.065	1.000
2.600	0.80	84.	2415.	13247.	12898.	12202.	2666.	1.000	0.070	1.000
2.700	0.91	92.	2579.	14129.	13757.	13013.	2684.	1.000	0.076	1.000
2.800	1.03	101.	2782.	15050.	14648.	13846.	2701.	1.000	0.083	1.000
2.900	1.15	110.	3133.	16024.	15572.	14669.	2716.	1.000	0.089	1.000
3.000	1.29	121.	3500.	17032.	16527.	15518.	2730.	1.000	0.096	1.000
3.100	1.44	133.	3885.	18072.	17512.	16391.	2742.	1.000	0.103	1.000
3.200	1.61	146.	4260.	19137.	18522.	17293.	2753.	1.000	0.110	1.000
3.300	1.79	160.	4594.	20219.	19557.	18232.	2763.	1.000	0.118	1.000
3.400	1.99	176.	4938.	21324.	20612.	19188.	2771.	1.000	0.126	1.000
3.500	2.22	192.	5270.	22444.	21684.	20164.	2778.	1.000	0.134	1.000
3.600	2.46	209.	5600.	23578.	22770.	21154.	2784.	1.000	0.143	1.000
3.700	2.72	228.	5935.	24720.	23864.	22152.	2789.	1.000	0.152	1.000
3.800	3.00	248.	6273.	25868.	24963.	23154.	2793.	1.000	0.162	1.000
3.900	3.31	268.	6613.	27016.	26062.	24154.	2795.	1.000	0.171	1.000
4.000	3.65	290.	6954.	28157.	27154.	25148.	2797.	1.000	0.181	1.000
4.100	4.01	313.	7294.	29288.	28236.	26132.	2797.	1.000	0.192	1.000
4.200	4.40	337.	7631.	30402.	29301.	27100.	2797.	1.000	0.203	1.000
4.300	4.82	362.	7938.	31489.	30344.	28054.	2796.	1.000	0.214	1.000
4.400	5.27	388.	8228.	32546.	31359.	28986.	2794.	1.000	0.225	1.000
4.500	5.75	415.	8508.	33569.	32342.	29887.	2791.	1.000	0.237	1.000
4.600	6.27	443.	8778.	34552.	33286.	30754.	2787.	1.000	0.249	1.000
4.700	6.82	472.	9036.	35492.	34188.	31582.	2782.	1.000	0.262	1.000
4.800	7.40	501.	9281.	36382.	35044.	32367.	2777.	1.000	0.274	1.000
4.900	8.02	532.	9511.	37220.	35849.	33105.	2771.	1.000	0.287	1.000

TIME (MS)	TRAV (IN)	VEL (FT/S)	ACC (G)	BREECH PRESS (PSI)	MEAN PRESS (PSI)	BASE PRESS (PSI)	MEAN TEMP (K)	FRAC BURN 1	FRAC BURN 2	FRAC BURN 3
5.000	8.68	563.	9726.	38002.	36599.	33794.	2765.	1.000	0.301	1.000
5.100	9.37	594.	9924.	38725.	37294.	34431.	2758.	1.000	0.314	1.000
5.186	10.00	622.	10082.	39299.	37845.	34937.	2752.	1.000	0.326	1.000
PRESSURE GAGE 3 EXPOSED										
5.200	10.10	626.	10106.	39387.	37929.	35014.	2751.	1.000	0.328	1.000
5.300	10.87	659.	10271.	39985.	38504.	35541.	2743.	1.000	0.342	1.000
5.400	11.69	693.	10418.	40520.	39017.	36012.	2734.	1.000	0.356	1.000
5.500	12.54	726.	10548.	40990.	39469.	36426.	2726.	1.000	0.371	1.000
5.600	13.43	760.	10660.	41396.	39858.	36703.	2717.	1.000	0.385	1.000
5.700	14.36	795.	10755.	41738.	40187.	37085.	2707.	1.000	0.400	1.000
5.800	15.34	830.	10832.	42018.	40456.	37331.	2698.	1.000	0.415	1.000
5.900	16.35	865.	10893.	42237.	40666.	37523.	2688.	1.000	0.430	1.000
6.000	17.41	900.	10938.	42397.	40819.	37664.	2678.	1.000	0.445	1.000
6.100	18.51	935.	10968.	42501.	40919.	37755.	2668.	1.000	0.461	1.000
6.200	19.66	970.	10983.	42551.	40967.	37799.	2658.	1.000	0.476	1.000
6.248	20.21	987.	10985.	42556.	40972.	37803.	2653.	1.000	0.484	1.000
LOCAL PRESSURE MAX DETECTED										
6.300	20.84	1006.	10984.	42550.	40966.	37797.	2648.	1.000	0.492	1.000
6.400	22.07	1041.	10971.	42501.	40918.	37754.	2637.	1.000	0.508	1.000
6.500	23.34	1076.	10947.	42407.	40828.	37670.	2627.	1.000	0.523	1.000
6.600	24.65	1112.	10912.	42272.	40698.	37551.	2617.	1.000	0.539	1.000
6.700	26.01	1147.	10865.	42099.	40531.	37397.	2607.	1.000	0.555	1.000
6.800	27.41	1182.	10810.	41890.	40331.	37212.	2597.	1.000	0.571	1.000
6.900	28.84	1216.	10745.	41649.	40099.	36999.	2586.	1.000	0.587	1.000
7.000	30.33	1251.	10673.	41379.	39839.	36760.	2576.	1.000	0.603	1.000
7.100	31.85	1285.	10593.	41082.	39554.	36499.	2567.	1.000	0.618	1.000
7.200	33.41	1319.	10507.	40763.	39247.	36216.	2557.	1.000	0.634	1.000
7.300	35.01	1353.	10416.	40422.	38920.	35915.	2547.	1.000	0.650	1.000
7.400	36.66	1386.	10320.	40064.	38575.	35598.	2538.	1.000	0.666	1.000
7.500	38.34	1419.	10219.	39689.	38215.	35268.	2528.	1.000	0.682	1.000
7.600	40.06	1452.	10114.	39301.	37842.	34925.	2519.	1.000	0.698	1.000
7.700	41.82	1484.	10007.	38902.	37458.	34572.	2510.	1.000	0.713	1.000
7.800	43.62	1516.	9897.	38492.	37065.	34210.	2501.	1.000	0.729	1.000
7.900	45.46	1548.	9785.	38075.	36664.	33841.	2492.	1.000	0.745	1.000
8.000	47.34	1579.	9671.	37652.	36257.	33467.	2483.	1.000	0.760	1.000
8.100	49.25	1610.	9556.	37223.	35845.	33088.	2475.	1.000	0.776	1.000
8.200	51.20	1641.	9439.	36791.	35430.	32707.	2466.	1.000	0.791	1.000
8.300	53.19	1671.	9323.	36357.	35013.	32323.	2458.	1.000	0.807	1.000
8.400	55.21	1701.	9206.	35922.	34594.	31938.	2450.	1.000	0.822	1.000
8.500	57.27	1730.	9089.	35486.	34175.	31554.	2442.	1.000	0.837	1.000
8.600	59.37	1759.	8972.	35051.	33757.	31169.	2434.	1.000	0.852	1.000
8.700	61.50	1788.	8847.	34584.	33303.	30756.	2426.	1.000	0.867	1.000
8.800	63.66	1816.	8688.	33996.	32743.	30237.	2416.	1.000	0.879	1.000
8.900	65.86	1844.	8515.	33356.	32128.	29671.	2406.	1.000	0.889	1.000
9.000	68.08	1871.	8334.	32686.	31484.	29080.	2395.	1.000	0.899	1.000
9.100	70.35	1898.	8148.	31998.	30823.	28472.	2384.	1.000	0.908	1.000
9.200	72.64	1924.	7960.	31300.	30152.	27856.	2373.	1.000	0.915	1.000
9.300	74.96	1949.	7770.	30598.	29477.	27235.	2362.	1.000	0.923	1.000
9.400	77.32	1974.	7581.	29896.	28802.	26615.	2351.	1.000	0.929	1.000
9.500	79.70	1998.	7392.	29197.	28131.	25999.	2339.	1.000	0.935	1.000
9.600	82.11	2021.	7206.	28506.	27466.	25388.	2328.	1.000	0.941	1.000
9.700	84.55	2044.	7022.	27823.	26810.	24764.	2316.	1.000	0.946	1.000
9.800	87.02	2067.	6840.	27150.	26163.	24190.	2305.	1.000	0.951	1.000
9.900	89.51	2088.	6662.	26489.	25528.	23606.	2293.	1.000	0.955	1.000
10.000	92.03	2110.	6488.	25840.	24905.	23033.	2282.	1.000	0.959	1.000

TIME (MS)	TRAV (IN)	VEL (FT/S)	ACC (G)	BREECH PRESS (PSI)	MEAN PRESS (PSI)	BASE PRESS (PSI)	MEAN TEMP (K)	FRAC BURN 1	FRAC BURN 2	FRAC BURN 3
10.190	94.57	2130.	6317.	25206.	24294.	22472.	2270.	1.000	0.962	1.000
10.200	97.14	2150.	6150.	24585.	23698.	21924.	2259.	1.000	0.966	1.000
10.300	99.73	2170.	5987.	23979.	23115.	21388.	2247.	1.000	0.968	1.000
10.400	102.35	2189.	5829.	23389.	22548.	20867.	2236.	1.000	0.971	1.000
10.500	104.99	2207.	5676.	22817.	21998.	20361.	2225.	1.000	0.974	1.000
10.600	107.65	2225.	5527.	22262.	21465.	19870.	2214.	1.000	0.976	1.000
10.700	110.33	2243.	5383.	21724.	20947.	19395.	2203.	1.000	0.978	1.000
10.800	113.03	2260.	5243.	21202.	20446.	18933.	2192.	1.000	0.980	1.000
10.900	115.75	2277.	5108.	20697.	19960.	18486.	2181.	1.000	0.982	1.000
11.000	118.49	2293.	4978.	20206.	19488.	18053.	2171.	1.000	0.984	1.000
11.100	121.25	2309.	4851.	19731.	19032.	17632.	2160.	1.000	0.985	1.000
11.200	124.03	2324.	4728.	19271.	18589.	17225.	2150.	1.000	0.987	1.000
11.300	126.83	2339.	4610.	18825.	18160.	16830.	2140.	1.000	0.988	1.000
11.400	129.65	2354.	4495.	18392.	17744.	16447.	2130.	1.000	0.990	1.000
11.500	132.48	2368.	4384.	17973.	17341.	16076.	2120.	1.000	0.991	1.000
11.600	135.33	2382.	4276.	17567.	16950.	15717.	2110.	1.000	0.992	1.000
11.700	138.20	2396.	4172.	17173.	16571.	15368.	2100.	1.000	0.993	1.000
11.800	141.08	2409.	4071.	16791.	16204.	15030.	2090.	1.000	0.994	1.000
11.900	143.98	2422.	3973.	16421.	15848.	14702.	2081.	1.000	0.995	1.000
12.000	146.89	2435.	3879.	16062.	15502.	14383.	2071.	1.000	0.996	1.000
12.100	149.82	2447.	3787.	15713.	15167.	14075.	2062.	1.000	0.996	1.000
12.200	152.76	2459.	3698.	15376.	14842.	13775.	2053.	1.000	0.997	1.000
12.300	155.72	2471.	3612.	15048.	14527.	13485.	2044.	1.000	0.997	1.000
12.400	158.69	2482.	3529.	14730.	14221.	13203.	2035.	1.000	0.998	1.000
12.500	161.68	2493.	3449.	14421.	13924.	12929.	2026.	1.000	0.998	1.000
12.600	164.68	2504.	3370.	14122.	13636.	12663.	2017.	1.000	0.999	1.000
12.700	167.69	2515.	3295.	13831.	13356.	12405.	2008.	1.000	0.999	1.000
12.800	170.71	2526.	3221.	13549.	13084.	12155.	1999.	1.000	0.999	1.000
12.900	173.75	2536.	3150.	13274.	12820.	11911.	1991.	1.000	1.000	1.000
13.000	176.80	2546.	3081.	13008.	12564.	11675.	1982.	1.000	1.000	1.000
13.100	179.86	2556.	3014.	12749.	12314.	11445.	1974.	1.000	1.000	1.000
13.200	182.93	2565.	2950.	12498.	12072.	11221.	1966.	1.000	1.000	1.000
13.300	186.02	2575.	2887.	12253.	11837.	11004.	1957.	1.000	1.000	1.000
13.395	188.96	2583.	2829.	12027.	11619.	10803.	1950.	1.000	1.000	1.000
PROPELLANT 2 BURNED OUT										
13.400	189.11	2584.	2826.	12016.	11608.	10795.	1949.	1.000	1.000	1.000
13.500	192.21	2593.	2767.	11785.	11386.	10588.	1941.	1.000	1.000	1.000
13.600	195.33	2602.	2710.	11562.	11171.	10389.	1933.	1.000	1.000	1.000
13.700	198.46	2610.	2654.	11345.	10962.	10196.	1926.	1.000	1.000	1.000
13.800	201.60	2619.	2598.	11134.	10759.	10009.	1918.	1.000	1.000	1.000
13.900	204.74	2627.	2542.	10929.	10562.	9829.	1910.	1.000	1.000	1.000
13.908	205.00	2628.	2537.	10912.	10546.	9814.	1910.	1.000	1.000	1.000
PROJECTILE EXIT										

CONDITIONS AT:	PHAX	MUZZLE
TIME (MS):	6.248	13.908
TRAVEL (IN):	20.21	205.00
VELOCITY (FT/S):	987.	2628.
ACCELERATION (G):	16985.	2537.
BREECH PRESS (PSI):	42556.	10912.
MEAN PRESS (PSI):	40972.	10546.
BASE PRESS (PSI):	37803.	9814.
MEAN TEMP (K):	2653.	1910.
Z CHARGE 1 (-):	1.000	1.000
Z CHARGE 2 (-):	0.484	1.000
Z CHARGE 3 (-):	1.000	1.000

GAGE	AT (IN)	PHAX (PSI)
	WRT SOM	
1	-30.00	42556.
2	0.00	40581.
3	10.00	39492.

ENERGY BALANCE SUMMARY	IN-LB	%
TOTAL CHEMICAL:	445809920.	100.00
(1) INTERNAL GAS:	283111168.	63.50
(2) WORK AND LOSSES:	162698832.	36.50
(A) PROJECTILE KINETIC:	123518720.	27.71
(B) GAS KINETIC:	11070795.	2.48
(C) PROJECTILE ROTATIONAL:	1523850.	0.34
(D) FRICTIONAL WORK TO TUBE:	0.	0.00
(E) OTHER FRICTIONAL WORK:	12313684.	2.76
(F) WORK DONE AGAINST AIR:	584053.	0.13
(G) HEAT CONVECTED TO BORE:	13687733.	3.07
(H) RECOIL ENERGY:	0.	0.00
LOADING DENSITY (G/CM3):	0.621	
CHARGE WT/PROJECTILE WT:	0.269	
PIEZOMETRIC EFFICIENCY:	0.475	
EXPANSION RATIO:	6.317	

PARAMETRIC VARIABLES: / 1/ PROP 2 CHWT

/1/	PMAX	VMU2	PMU2	Z(1)	X82=1	Z(2)	X82=1	Z(3)	X82=1
25.00	42556.	2628.	9814.	1.000	0.02	1.000	186.02	1.000	0.34
25.20	43147.	2642.	9881.	1.000	0.02	1.000	185.62	1.000	0.35
25.40	43745.	2657.	9949.	1.000	0.02	1.000	185.19	1.000	0.36
25.60	44349.	2672.	10015.	1.000	0.02	1.000	184.72	1.000	0.36
25.80	44961.	2687.	10086.	1.000	0.02	1.000	184.25	1.000	0.37
26.00	45582.	2701.	10151.	1.000	0.02	1.000	183.72	1.000	0.37
26.20	46208.	2716.	10217.	1.000	0.02	1.000	183.17	1.000	0.38
26.40	46845.	2731.	10288.	1.000	0.02	1.000	182.60	1.000	0.39
26.60	47491.	2745.	10350.	1.000	0.02	1.000	181.98	1.000	0.39
26.80	48142.	2760.	10415.	1.000	0.02	1.000	178.12	1.000	0.40
27.00	48802.	2775.	10485.	1.000	0.02	1.000	177.45	1.000	0.41

Test Case 4

This run was used in a case study for a design of an incremental charge concept. It is included because it illustrates the utility of a well-documented input deck. All keywords are in uppercase, but the comments are in lowercase and spaced appropriately. The propelling charge is quite involved, requiring five different propellant decks. It should be noted that the combustible and non-combustible tubes were modeled as a propellant in IBHVG2.

```
SCOMM
  IBHVG2 BENCHMARK TEST 4
    Showing acceptable uses of lower-case characters
    Showing five propellants, including two non-burning charges
    Shows iteration on f.fth charge web to find PMAK=45kpsi

  Changing Burning Data      M30/M9      Zone 5

  -----
  This run is to determine nominal parameter values
  by comparing the results with the "BARE INCREMENT"
  baseline.
  -----

  ** DECK as of 14 Mar, 1630 hours
  -----

SHEAT
  TSHL=0.00384

SGUN
  NAME='155-MM 198'      CHAM=1150      GRVE=6.2      LAND=6.1
  G/L=1.66 TRAV=205. TWST=20

SPROJ
  NAME='M549A1' PRWT=96

SRESI
  NPTS=8
  TRAV= 0, 0.4, 1., 1.55, 2.05, 4.5, 20, 200
  PRES=250, 2000, 3500, 2000, 1000, 500, 500, 500

SINFO
  POPT=1,1,1,0,1
  RUN='Incremental Charge Design M30-M9'

SPRIM      $ Primer
  NAME='BLK POWDER'      $ Class 5 Black Powder
  CHWT=0.0154
  GAMA=1.25 FORC=96000 COV=30 TEMP=2000

$PROP      $ Igniter Function
  NAME='BLACK POWDER' $ Bag of black powder with each increment
  CHWT=0.3125      $ 5 ozs, 1 oz per increment
  GRAN='CORD'
  LEN=0.198 DIAM=0.098 RHO=0.06 GAMA=1.25 FORC=96000
  COV=30 TEMP=2000 ALPH=0.0 BETA=50.0 EROS=0.0

$PROP      $ Inner Tube
  NAME='NC TUBE'      $ Nitrocellulose Tube (Non-Combustible)
  GRAN='1PF'
  FORC=180000 COV=30 TEMP=1553 RHO=0.034 GAMA=1.25
```

NTBL=0 ALPH=0.00001 BETA=0.00001
 LEN=5.75
 PD=1.6875
 DIAM=2.0
 WEB=0.15625
 CW=0.3125

SPROP \$ Outer Tube -- does not really exist

NAME='MC TUBE' \$ Nitrocellulose Tube (Non-Combustible)
 GRAN='1PF'
 FORC=180000 COV=30 TEMP=1553 RHO=0.034 GAMA=1.25
 NTBL=0 ALPH=0.00001 BETA=0.00001
 LEN=5.75
 DIAM=2.0
 PD=5.84
 WEB=0.005
 CHWT=0.00005 \$ effectively, this tube is fictitious

SPROP \$ M9 Propellant Charge

NAME='M9 HAIR' \$ Lot # 6961
 GRAN='CORD'
 RHO=0.06 GAMA=1.2078 FORC=392399 COV=27.365 TEMP=3860
 LEN=4.00 DIAM=0.0337
 NTBL = 4
 PR4L = 1000, 3000, 4000, 15000
 BR4L = 0.617, 1.68, 1.90, 6.13
 EROS=0.0
 CHWT=1.5

SPROP \$ M30 Propellant Charge

NAME='M30A1' \$ Lot # 7022G
 GRAN='1PF'
 RHO=0.0572 GAMA=1.243 FORC=356400 COV=28.5 TEMP=3040
 NTBL=4
 PR4L = 1000, 5000, 10000, 30000
 BR4L = 0.40, 1.25, 2.25, 5.56
 LEN=5.50
 DIAM=0.2572
 WEB=0.09235
 PD=0.0725
 CHWT=22.5

SPMAX

VARY='WEB' TRY1=0.09 TRY2=0.094 PMAX=45000. NTH=5

SEND

Producing the following output:

ERRTOL= 4.768372E-07

```
CARD 1 --> $COMM
CARD 2 --> ISHVG2 BENCHMARK TEST 4
CARD 3 --> Showing acceptable uses of lower-case characters
CARD 4 --> Showing five propellants, including two non-burning charges
CARD 5 --> Shows iteration on fifth charge web to find PHAX=45kpsi
CARD 6 -->
CARD 7 --> Changing Burning Data M30/M9 Zone 5
CARD 8 -->
CARD 9 --> -----
CARD 10 --> This run is to determine nominal parameter values
CARD 11 --> by comparing the results with the "BARE INCREMENT"
CARD 12 --> baseline.
CARD 13 --> -----
CARD 14 -->
CARD 15 --> ** DECK as of 14 Mar, 1630 hours
CARD 16 -->
CARD 17 --> -----
CARD 18 -->
CARD 19 -->
CARD 20 --> $HEAT
CARD 21 --> TSHL=0.00384
CARD 22 -->
CARD 23 --> $GUN
CARD 24 --> NAME='155-MM 198' CHAM=1150 GRVE=6.2 LANO=6.1
CARD 25 --> G/L=1.66 TRAV=205. TWST=20
CARD 26 -->
CARD 27 --> $PROJ
CARD 28 --> NAME='M549A1' PRVT=96
CARD 29 -->
CARD 30 --> $RESI
CARD 31 --> NPTS=8
CARD 32 --> TRAV= 0, 0.4, 1., 1.55, 2.05, 4.5, 20, 200
CARD 33 --> PRES=250, 2000, 3500, 2000, 1000, 500, 500, 500
CARD 34 -->
CARD 35 --> $INFO
CARD 36 --> POPT=1,1,1,0,1
CARD 37 --> RUN="Incremental Charge Design M30-M9"
CARD 38 -->
CARD 39 -->
CARD 40 -->
CARD 41 --> $PRIM $ Primer
CARD 42 -->
CARD 43 --> NAME='BLK POWDER' $ Class 5 Black Powder
CARD 44 --> CHWT=0.0154
CARD 45 --> GAMA=1.25 FORC=96000 COV=30 TEMP=2000
CARD 46 -->
CARD 47 -->
CARD 48 -->
CARD 49 --> $PROP $ Igniter Function
CARD 50 -->
CARD 51 --> NAME='BLACK POWDER' $ Bag of black powder with each increment
CARD 52 --> CHWT=0.3125 $ 5 ozs, 1 oz per increment
CARD 53 --> GRAN='CORD'
CARD 54 --> LEN=0.198 DIAM=0.098 RHO=0.06 GAMA=1.25 FORC=96000
CARD 55 --> COV=30 TEMP=2000 ALPH=0.0 BETA=50.0 EROS=0.0
```

```

CARD 56 -->
CARD 57 -->
CARD 58 -->
CARD 59 --> $PROP          $ Inner Tube
CARD 60 -->
CARD 61 --> NAME='NC TUBE'  $ Nitrocellulose Tube (Non-Combustible)
CARD 62 --> GRAN='1PF'
CARD 63 --> FORC=180000 COV=30 TEMP=1553 RHO=0.034 GAMA=1.25
CARD 64 --> NTBL=0 ALPH=0.00001 BETA=0.00001
CARD 65 --> LEN=5.75
CARD 66 --> PD=1.6875
CARD 67 --> DIAM=2.0
CARD 68 --> WEB=0.15625
CARD 69 --> CV=0.3125
CARD 70 -->
CARD 71 -->
CARD 72 -->
CARD 73 -->
CARD 74 --> $PROP          $ Outer Tube -- does not really exist
CARD 75 -->
CARD 76 --> NAME='NC TUBE'  $ Nitrocellulose Tube (Non-Combustible)
CARD 77 --> GRAN='1PF'
CARD 78 --> FORC=180000 COV=30 TEMP=1553 RHO=0.034 GAMA=1.25
CARD 79 --> NTBL=0 ALPH=0.00001 BETA=0.00001
CARD 80 --> GLEN=5.75
CARD 81 --> DIAM=5.9
CARD 82 --> PD=5.09
CARD 83 --> WEB=0.005
CARD 84 --> CHWT=0.00005 $ effectively, this tube is fictitious
CARD 85 -->
CARD 86 -->
CARD 87 -->
CARD 88 --> $PROP          $ H9 Propellant Charge
CARD 89 --> NAME='H9 HAIR'  $ Lot # 6961
CARD 90 --> GRAN='CORD'
CARD 91 --> RHO=0.06 GAMA=1.2078 FORC=392399 COV=27.365 TEMP=3860
CARD 92 --> LEN=4.00 DIAM=0.0337
CARD 93 --> NTBL = 4
CARD 94 --> PR4L = 1000, 3000, 4000, 15000
CARD 95 --> BR4L = 0.617, 1.68, 1.90, 6.13
CARD 96 --> EROS=0.0
CARD 97 --> CHWT=1.5
CARD 98 -->
CARD 99 -->
CARD 100 --> $PROP          $ H30 Propellant Charge
CARD 101 --> NAME='H30A1'  $ Lot # 70226
CARD 102 --> GRAN='1PF'
CARD 103 --> RHO=0.0572 GAMA=1.243 FORC=356400 COV=28.5 TEMP=3040
CARD 104 --> NTBL=4
CARD 105 --> PR4L = 1000, 5000, 10000, 30000
CARD 106 --> BR4L = 0.40, 1.35, 2.25, 5.56
CARD 107 --> LEN=5.50
CARD 108 --> DIAM=0.2572
CARD 109 --> WEB=0.09235
CARD 110 --> PD=0.0725

```

CARD 111 --> CWT=22.5
CARD 112 -->
CARD 113 --> SPMAX
CARD 114 -->
CARD 115 --> VARY='WEB' TRY1=0.09 TRY2=0.094 PMAX=45000. NTN=5
CARD 116 -->
CARD 117 --> SEND

----- GUN TUBE -----
 TYPE: 155-MM 190
 GROOVE DIAMETER (IN): 6.200
 TWIST (CAL/S/TURR): 20.0
 SHELL THICKNESS (IN): 0.003040
 INITIAL SWELL TEMP (K): 293.
 CHAMBER VOLUME (IN3): 1150.00
 LAND DIAMETER (IN): 6.100
 BORE AREA (IN2): 29.8275
 SHELL CP (IN-LB/LB-K): 1845.0
 AIR NO (IN-LB/IN2-S-K): 0.06480
 TRAVEL (IN): 205.00
 GROOVE/LAND RATIO (-): 1.640
 HEAT-LOSS OPTION: 1
 SHELL DENSITY (LB/IN3): 0.2840
 ----- PROJECTILE -----
 TYPE: M549A1
 TOTAL WEIGHT (LB): 96.000
 WEIGHT PREDICTOR OPTION: 0
 ----- RESISTANCE -----
 AIR RESISTANCE OPTION: 1

1	TRAVEL (IN)	PRESSURE (PSI)	WALL HEATING FRACTION:	0.000	FRICTION TABLE LENGTH:	8
1	0.00	250.	1	TRAVEL (IN)	PRESSURE (PSI)	
2	0.40	2000.	4	1.55	2000.	500.
3	1.00	3500.	5	2.05	1000.	500.
			6	4.50	500.	

 ----- GENERAL -----
 MAX TIME STEP (S): 0.000100
 PRINT OPTIONS: 1 1 1 0 1 1
 GRADIENT MODEL: LAGRANGIAN
 PRINT STEP (S): 0.000000
 STORE OPTION: 0
 MAX RELATIVE ERROR (-): 0.00200
 CONSTANT-PRESSURE OPTION: 0
 ----- RECOIL -----
 RECOIL OPTION: 0
 TYPE: 0
 RECOILING WEIGHT (LB): 0.
 ----- PRIMER -----
 TYPE: BLK POWDER
 CONVOLUME (IN3/LB): 30.000
 GAMMA (-): 1.2500
 FLAME TEMP (K): 2000.0
 FORCE (FT-LB/LB): 96000.
 WEIGHT (LB): 0.015400

- CHARGE 1 -

TYPE: BLACK POWDER
EROSIVE COEFF (-):
GRAIN LENGTH (IN):

0.000000
0.19800

GRAINS:
CHARGE IGM CODE:
GRAIN DIAMETER (IN):

3487.3
0.09800

CORD
0

WEIGHT (LB):
CHARGE IGM AT (S):

0.3125
0.00000E+00

PROPERTIES AT LAYER BOUNDARIES OF LAT SURFACES

1ST	2ND	3RD	4TH
AT DEPTH (IN):	0.00000	0.00000	0.00000
ADJACENT LAYER WT %:	100.000	100.000	100.000
DENSITY (LB/IN3):	0.06000	0.06000	0.06000
GAMMA (-):	1.2500	1.2500	1.2500
FORCE (FT-LB/LB):	96000.	96000.	96000.
COVOLUME (IN3/LB):	30.000	30.000	30.000
FLAME TEMP (K):	2000.0	2000.0	2000.0
BURNING RATE EXPS:	0.0060	0.0060	0.0060
BURNING RATE COEFFS:	50.0000000	50.0000000	50.0000000

- CHARGE 2 -

TYPE: MC TUBE
EROSIVE COEFF (-):
GRAIN LENGTH (IN):
INNER WEB (IN):

0.000000
5.75000
0.15625

GRAINS:
CHARGE IGM CODE:
GRAIN DIAMETER (IN):
WEB RATIO:

1.7662
2.00000
1.0000

1PF
0

WEIGHT (LB):
CHARGE IGM AT (S):
PERF DIAMETER (IN):

0.3125
0.00000E+00
1.68750

PROPERTIES AT LAYER BOUNDARIES OF LAT SURFACES

1ST	2ND	3RD	4TH
AT DEPTH (IN):	0.00000	0.00000	0.00000
ADJACENT LAYER WT %:	100.000	100.000	100.000
DENSITY (LB/IN3):	0.03400	0.03400	0.03400
GAMMA (-):	1.2500	1.2500	1.2500
FORCE (FT-LB/LB):	180000.	180000.	180000.
COVOLUME (IN3/LB):	30.000	30.000	30.000
FLAME TEMP (K):	1553.0	1553.0	1553.0
BURNING RATE EXPS:	0.0000	0.0000	0.0000
BURNING RATE COEFFS:	0.0000100	0.0000100	0.0000100

PROPERTIES AT LAYER BOUNDARIES OF LAT SURFACES

1ST	2ND	3RD	4TH
AT DEPTH (IN):	0.00000	0.00000	0.00000
ADJACENT LAYER WT %:	100.000	100.000	100.000
DENSITY (LB/IN3):	0.03400	0.03400	0.03400
GAMMA (-):	1.2500	1.2500	1.2500
FORCE (FT-LB/LB):	180000.	180000.	180000.
COVOLUME (IN3/LB):	30.000	30.000	30.000
FLAME TEMP (K):	1553.0	1553.0	1553.0
BURNING RATE EXPS:	0.0000	0.0000	0.0000
BURNING RATE COEFFS:	0.0000100	0.0000100	0.0000100

- CHARGE 3 -

TYPE: NC TUBE	GRAINS:	0.27619E-02	1PF	0	WEIGHT (LB):	0.0001
EROSIVE COEFF (-):	CHARGE IGN CODE:				CHARGE IGN AT (S):	0.00000E+00
GRAIN LENGTH (IN):	GRAIN DIAMETER (IN):	5.75000	5.90000		PERF DIAMETER (IN):	5.89000
INNER WEB (IN):	WEB RATIO:	0.00500	1.0000			

AT DEPTH (IN):	PROPERTIES AT LAYER BOUNDARIES OF PERF SURFACES	PROPERTIES AT LAYER BOUNDARIES OF END SURFACES
ADJACENT LAYER VT %:	1ST 2ND 3RD 4TH	1ST 2ND 3RD 4TH
DENSITY (LB/IN3):	-----	-----
GAMMA (-):	-----	-----
FORCE (FT-LB/LB):	-----	-----
COVOLUME (IN3/LB):	-----	-----
FLAME TEMP (K):	-----	-----
BURNING RATE EXPS:	-----	-----
BURNING RATE COEFFS:	-----	-----

AT DEPTH (IN):	PROPERTIES AT LAYER BOUNDARIES OF LAT SURFACES
ADJACENT LAYER VT %:	1ST 2ND 3RD 4TH
DENSITY (LB/IN3):	-----
GAMMA (-):	-----
FORCE (FT-LB/LB):	-----
COVOLUME (IN3/LB):	-----
FLAME TEMP (K):	-----
BURNING RATE EXPS:	-----
BURNING RATE COEFFS:	-----

- CHARGE 4 -

TYPE: M9 NAIR
EROSIVE COEFF (-):
GRAIN LENGTH (IN):

0.000000
4.00000

GRAINS:
CHARGE IGM CODE:
GRAIN DIAMETER (IN):

7007.0
0.03370

WEIGHT (LB):
CHARGE IGM AT (S):

1.500C
0.00000E+00

PROPERTIES AT LAYER BOUNDARIES OF END SURFACES
1ST 2ND 3RD 4TH

AT DEPTH (IN):
ADJACENT LAYER WT %:
DENSITY (LB/IN3):
GAMMA (-):
FORCE (FT-LB/LB):
COVOLUME (IN3/LB):
FLAME TEMP (K):
MEAN PRESSURES (PSI):
MEAN PRESSURES (PSI):
MEAN PRESSURES (PSI):
MEAN PRESSURES (PSI):
BURNING RATES (IN/S):
BURNING RATES (IN/S):
BURNING RATES (IN/S):

0.00000
100.000
0.06000
1.2078
392399.
27.365
3860.0
1000.0
3000.0
4000.0
15000.0
0.62
1.68
1.90
6.13

PROPERTIES AT LAYER BOUNDARIES OF LAT SURFACES
1ST 2ND 3RD 4TH

0.00000
100.000
0.06000
1.2078
392399.
27.365
3860.0
1000.0
3000.0
4000.0
15000.0
0.62
1.68
1.90
6.13

--- CHARGE 5 ---

TYPE: W30A1	GRAINS:	1518.6	1PF	WEIGHT (LB):	22.5000
EROSIVE COEFF (-):	CHARGE IGN CODE:		0	CHARGE IGN AT (S):	0.00000E+00
GRAIN LENGTH (IN):	GRAIN DIAMETER (IN):		0.25338	PERF DIAMETER (IN):	0.07250
INNER WEB (IN):	WEB RATIO:		1.0000		

	PROPERTIES AT LAYER BOUNDARIES OF PERF SURFACES	PROPERTIES AT LAYER BOUNDARIES OF END SURFACES
	1ST 2ND 3RD 4TH	1ST 2ND 3RD 4TH
AT DEPTH (IN):	---	---
ADJACENT LAYER WT %:	---	---
DENSITY (LB/IN ³):	---	---
GAMMA (-):	---	---
FORCE (FT-LB/LB):	---	---
COVOLUME (IN ³ /LB):	---	---
FLAME TEMP (K):	---	---
MEAN PRESSURES (PSI):	---	---
MEAN PRESSURES (PSI):	---	---
MEAN PRESSURES (PSI):	---	---
BURNING RATES (IN/S):	---	---
BURNING RATES (IN/S):	---	---
BURNING RATES (IN/S):	---	---

	PROPERTIES AT LAYER BOUNDARIES OF LAT SURFACES
	1ST 2ND 3RD 4TH
AT DEPTH (IN):	---
ADJACENT LAYER WT %:	---
DENSITY (LB/IN ³):	---
GAMMA (-):	---
FORCE (FT-LB/LB):	---
COVOLUME (IN ³ /LB):	---
FLAME TEMP (K):	---
MEAN PRESSURES (PSI):	---
MEAN PRESSURES (PSI):	---
MEAN PRESSURES (PSI):	---
BURNING RATES (IN/S):	---
BURNING RATES (IN/S):	---
BURNING RATES (IN/S):	---

TIME (MS)	TRAV (IN)	VEL (FT/S)	ACC (G)	BREECH PRESS (PSI)	MEAN PRESS (PSI)	BASE PRESS (PSI)	MEAN TEMP (K)	FRAC BURN 1	FRAC BURN 2	FRAC BURN 3	FRAC BURN 4	FRAC BURN 5
0.000	0.00	0.	0.	25.	25.	25.	2000.	0.000	0.000	0.000	0.000	0.000
0.100	0.00	0.	0.	172.	172.	172.	2149.	0.234	0.000	0.000	0.001	0.000
0.149	0.00	0.	0.	250.	250.	250.	2203.	0.334	0.000	0.000	0.002	0.000
SHOT-START PRESSURE ACHIEVED												
0.200	0.00	0.	25.	340.	336.	329.	2258.	0.431	0.000	0.000	0.003	0.000
0.300	0.00	0.	76.	527.	517.	496.	2359.	0.591	0.000	0.000	0.006	0.001
0.400	0.00	1.	132.	733.	715.	679.	2457.	0.720	0.000	0.000	0.011	0.002
0.500	0.00	1.	194.	961.	934.	881.	2550.	0.821	0.000	0.000	0.017	0.002
0.600	0.00	2.	262.	1214.	1178.	1106.	2639.	0.895	0.000	0.000	0.025	0.003
0.700	0.01	3.	336.	1496.	1449.	1357.	2723.	0.947	0.000	0.000	0.034	0.004
0.800	0.01	4.	418.	1810.	1753.	1638.	2801.	0.980	0.000	0.000	0.045	0.006
0.980	0.02	7.	587.	2476.	2395.	2234.	2925.	1.000	0.000	0.000	0.070	0.008
PROPELLANT 1 BURNED OUT												
1.000	0.02	7.	608.	2559.	2476.	2308.	2938.	1.000	0.000	0.000	0.073	0.009
1.100	0.03	9.	720.	3008.	2909.	2711.	2994.	1.000	0.000	0.000	0.090	0.011
1.200	0.05	12.	843.	3512.	3396.	3163.	3041.	1.000	0.000	0.000	0.110	0.013
1.300	0.06	15.	976.	4062.	3928.	3659.	3078.	1.000	0.000	0.000	0.130	0.015
1.400	0.08	18.	1118.	4666.	4512.	4205.	3109.	1.000	0.000	0.000	0.152	0.018
1.500	0.11	22.	1274.	5336.	5161.	4810.	3135.	1.000	0.000	0.000	0.177	0.021
1.600	0.13	26.	1442.	6076.	5877.	5480.	3158.	1.000	0.000	0.000	0.204	0.024
1.700	0.17	31.	1624.	6887.	6664.	6216.	3177.	1.000	0.000	0.000	0.234	0.027
1.800	0.21	37.	1819.	7774.	7523.	7023.	3193.	1.000	0.000	0.000	0.266	0.031
1.900	0.26	43.	2027.	8738.	8459.	7901.	3207.	1.000	0.000	0.000	0.301	0.036
2.000	0.31	50.	2247.	9781.	9471.	8853.	3218.	1.000	0.000	0.000	0.339	0.040
2.100	0.38	58.	2478.	10903.	10562.	9880.	3227.	1.000	0.000	0.000	0.380	0.045
2.200	0.45	66.	2749.	12115.	11737.	10980.	3234.	1.000	0.000	0.000	0.424	0.051
2.300	0.54	75.	3049.	13416.	12996.	12156.	3239.	1.000	0.000	0.000	0.469	0.057
2.400	0.63	86.	3364.	14800.	14337.	13411.	3243.	1.000	0.000	0.000	0.517	0.063
2.500	0.74	97.	3692.	16265.	15757.	14740.	3245.	1.000	0.000	0.000	0.566	0.070
2.600	0.87	109.	4031.	17805.	17250.	16140.	3245.	1.000	0.000	0.000	0.617	0.077
2.700	1.01	123.	4384.	19411.	18807.	17600.	3243.	1.000	0.000	0.000	0.668	0.086
2.800	1.16	138.	4968.	21104.	20420.	19052.	3240.	1.000	0.000	0.000	0.719	0.094
2.900	1.34	155.	5578.	22840.	22072.	20536.	3235.	1.000	0.000	0.000	0.769	0.104
3.000	1.53	174.	6211.	24604.	23749.	22038.	3229.	1.000	0.000	0.000	0.817	0.113
3.100	1.76	195.	6822.	26367.	25428.	23550.	3221.	1.000	0.000	0.000	0.862	0.124
3.200	2.00	218.	7439.	28113.	27089.	25040.	3211.	1.000	0.000	0.000	0.903	0.135
3.300	2.28	243.	7942.	29799.	28705.	26519.	3199.	1.000	0.000	0.000	0.938	0.147
3.400	2.59	269.	8402.	31410.	30253.	27939.	3186.	1.000	0.000	0.000	0.967	0.159
3.500	2.92	297.	8838.	32922.	31705.	29272.	3170.	1.000	0.000	0.000	0.987	0.171
3.600	3.30	326.	9241.	34310.	33038.	30493.	3153.	1.000	0.000	0.000	0.998	0.184
3.657	3.53	343.	9451.	35029.	33727.	31125.	3142.	1.000	0.000	0.000	1.000	0.192
PROPELLANT 4 BURNED OUT												
3.700	3.71	356.	9607.	35557.	34234.	31589.	3134.	1.000	0.000	0.000	1.000	0.198
3.800	4.15	388.	9957.	36740.	35369.	32628.	3115.	1.000	0.000	0.000	1.000	0.212
3.900	4.64	420.	10287.	37867.	36450.	33618.	3096.	1.000	0.000	0.000	1.000	0.226
4.000	5.16	454.	10578.	38925.	37469.	34556.	3077.	1.000	0.000	0.000	1.000	0.241
4.100	5.73	488.	10850.	39912.	38419.	35431.	3058.	1.000	0.000	0.000	1.000	0.255
4.200	6.34	524.	11100.	40821.	39293.	36237.	3039.	1.000	0.000	0.000	1.000	0.271
4.300	6.99	560.	11327.	41647.	40087.	36968.	3020.	1.000	0.000	0.000	1.000	0.286
4.400	7.68	597.	11530.	42385.	40797.	37622.	3001.	1.000	0.000	0.000	1.000	0.302
4.500	8.42	634.	11707.	43032.	41420.	38196.	2982.	1.000	0.000	0.000	1.000	0.318
4.600	9.20	672.	11860.	43586.	41953.	38687.	2963.	1.000	0.000	0.000	1.000	0.334
4.700	10.03	710.	11986.	44047.	42397.	39096.	2944.	1.000	0.000	0.000	1.000	0.350
4.800	10.91	749.	12087.	44415.	42751.	39422.	2926.	1.000	0.000	0.000	1.000	0.366
4.900	11.83	788.	12163.	44691.	43016.	39667.	2907.	1.000	0.000	0.000	1.000	0.382

TIME (MS)	TRAV (IN)	VEL (FT/S)	ACC (G)	BRECH PRESS (PSI)	MEAN PRESS (PSI)	BASE PRESS (PSI)	MEAN TEMP (K)	FRAC BURN 1	FRAC BURN 2	FRAC BURN 3	FRAC BURN 4	FRAC BURN 5
5.000	12.80	827.	12214.	44878.	43196.	39833.	2889.	1.000	0.000	0.000	1.000	0.399
5.100	13.81	867.	12241.	44979.	43293.	39922.	2870.	1.000	0.000	0.000	1.000	0.415
5.173	14.59	896.	12247.	45000.	43314.	39942.	2857.	1.000	0.000	0.000	1.000	0.427
LOCAL PRESSURE MAX DETECTED												
5.200	14.88	906.	12246.	44997.	43311.	39939.	2852.	1.000	0.000	0.000	1.000	0.432
5.300	15.99	946.	12229.	44938.	43254.	39887.	2834.	1.000	0.000	0.000	1.000	0.448
5.400	17.15	985.	12192.	44806.	43127.	39770.	2817.	1.000	0.000	0.000	1.000	0.465
5.500	18.35	1024.	12137.	44607.	42936.	39593.	2799.	1.000	0.000	0.000	1.000	0.481
5.600	19.61	1063.	12064.	44345.	42684.	39362.	2782.	1.000	0.000	0.000	1.000	0.498
5.700	20.91	1102.	11976.	44027.	42378.	39080.	2765.	1.000	0.000	0.000	1.000	0.514
5.800	22.25	1140.	11874.	43658.	42024.	38754.	2748.	1.000	0.000	0.000	1.000	0.530
5.900	23.64	1178.	11760.	43244.	41625.	38387.	2732.	1.000	0.000	0.000	1.000	0.546
6.000	25.08	1216.	11634.	42790.	41188.	37984.	2716.	1.000	0.000	0.000	1.000	0.562
6.100	26.56	1253.	11499.	42300.	40717.	37551.	2700.	1.000	0.000	0.000	1.000	0.577
6.200	28.09	1290.	11355.	41781.	40217.	37091.	2684.	1.000	0.000	0.000	1.000	0.593
6.300	29.66	1326.	11204.	41236.	39693.	36608.	2669.	1.000	0.000	0.000	1.000	0.608
6.400	31.27	1362.	11048.	40669.	39148.	36106.	2654.	1.000	0.000	0.000	1.000	0.623
6.500	32.92	1398.	10886.	40085.	38586.	35588.	2640.	1.000	0.000	0.000	1.000	0.638
6.600	34.62	1432.	10721.	39487.	38010.	35058.	2625.	1.000	0.000	0.000	1.000	0.653
6.700	36.36	1467.	10553.	38878.	37425.	34519.	2611.	1.000	0.000	0.000	1.000	0.668
6.800	38.14	1500.	10383.	38262.	36832.	33973.	2597.	1.000	0.000	0.000	1.000	0.682
6.900	39.96	1533.	10211.	37640.	36234.	33423.	2584.	1.000	0.000	0.000	1.000	0.696
7.000	41.82	1566.	10039.	37017.	35634.	32870.	2571.	1.000	0.000	0.000	1.000	0.710
7.100	43.72	1598.	9866.	36392.	35034.	32317.	2558.	1.000	0.000	0.000	1.000	0.724
7.200	45.66	1630.	9694.	35770.	34435.	31765.	2545.	1.000	0.000	0.000	1.000	0.738
7.300	47.63	1660.	9523.	35150.	33839.	31217.	2533.	1.000	0.000	0.000	1.000	0.751
7.400	49.64	1691.	9353.	34535.	33247.	30672.	2521.	1.000	0.000	0.000	1.000	0.764
7.500	51.69	1721.	9185.	33926.	32661.	30132.	2509.	1.000	0.000	0.000	1.000	0.777
7.600	53.77	1750.	9018.	33323.	32082.	29598.	2497.	1.000	0.000	0.000	1.000	0.790
7.700	55.89	1779.	8854.	32729.	31510.	29071.	2486.	1.000	0.000	0.000	1.000	0.803
7.800	58.04	1807.	8692.	32143.	30946.	28552.	2475.	1.000	0.000	0.000	1.000	0.815
7.900	60.23	1835.	8533.	31566.	30391.	28041.	2464.	1.000	0.000	0.000	1.000	0.828
8.000	62.44	1862.	8376.	30998.	29845.	27539.	2453.	1.000	0.000	0.000	1.000	0.840
8.100	64.69	1889.	8222.	30441.	29309.	27045.	2443.	1.000	0.000	0.000	1.000	0.852
8.200	66.98	1915.	8071.	29895.	28783.	26561.	2433.	1.000	0.000	0.000	1.000	0.863
8.300	69.29	1941.	7923.	29358.	28268.	26086.	2423.	1.000	0.000	0.000	1.000	0.875
8.400	71.63	1966.	7778.	28833.	27762.	25621.	2413.	1.000	0.000	0.000	1.000	0.886
8.500	74.01	1991.	7635.	28319.	27267.	25165.	2404.	1.000	0.000	0.000	1.000	0.897
8.600	76.41	2015.	7496.	27815.	26783.	24719.	2394.	1.000	0.000	0.000	1.000	0.908
8.700	78.84	2039.	7360.	27323.	26310.	24283.	2385.	1.000	0.000	0.000	1.000	0.919
8.800	81.31	2063.	7227.	26842.	25847.	23856.	2376.	1.000	0.000	0.000	1.000	0.930
8.900	83.79	2086.	7097.	26371.	25394.	23440.	2367.	1.000	0.000	0.000	1.000	0.940
9.000	86.31	2108.	6970.	25911.	24952.	23032.	2358.	1.000	0.000	0.000	1.000	0.951
9.100	88.85	2131.	6846.	25462.	24520.	22635.	2350.	1.000	0.000	0.000	1.000	0.961
9.200	91.42	2152.	6725.	25024.	24098.	22246.	2342.	1.000	0.000	0.000	1.000	0.971
9.300	94.02	2174.	6606.	24596.	23686.	21867.	2333.	1.000	0.000	0.000	1.000	0.981
9.400	96.64	2195.	6491.	24178.	23284.	21497.	2325.	1.000	0.000	0.000	1.000	0.991
9.496	99.18	2215.	6371.	23746.	22869.	21114.	2317.	1.000	0.000	0.000	1.000	1.000
PROPELLANT 5 BURNED OUT												
9.500	99.29	2216.	6363.	23717.	22841.	21089.	2316.	1.000	0.000	0.000	1.000	1.000
9.600	101.96	2236.	6175.	23034.	22184.	20484.	2302.	1.000	0.000	0.000	1.000	1.000
9.700	104.65	2255.	5994.	22380.	21555.	19904.	2288.	1.000	0.000	0.000	1.000	1.000
9.800	107.37	2274.	5821.	21753.	20952.	19349.	2275.	1.000	0.000	0.000	1.000	1.000
9.900	110.11	2293.	5655.	21152.	20373.	18816.	2262.	1.000	0.000	0.000	1.000	1.000
10.000	112.87	2311.	5496.	20575.	19819.	18305.	2249.	1.000	0.000	0.000	1.000	1.000

TIME (MS)	TRAV (IN)	VEL (FT/S)	ACC (G)	BREECH PRESS (PSI)	MEAN PRESS (PSI)	BASE PRESS (PSI)	MEAN TEMP (K)	FRAC BURN 1	FRAC BURN 2	FRAC BURN 3	FRAC BURN 4	FRAC BURN 5
10.100	115.66	2328.	5343.	20022.	19287.	17815.	2236.	1.000	0.000	0.000	1.000	1.000
10.200	118.46	2345.	5196.	19491.	18776.	17345.	2223.	1.000	0.000	0.000	1.000	1.000
10.300	121.28	2362.	5056.	18982.	18285.	16893.	2211.	1.000	0.000	0.000	1.000	1.000
10.400	124.13	2378.	4920.	18492.	17814.	16459.	2199.	1.000	0.000	0.000	1.000	1.000
10.500	126.99	2393.	4790.	18021.	17361.	16042.	2187.	1.000	0.000	0.000	1.000	1.000
10.600	129.87	2409.	4665.	17563.	16926.	15641.	2176.	1.000	0.000	0.000	1.000	1.000
10.700	132.77	2424.	4545.	17133.	16507.	15255.	2164.	1.000	0.000	0.000	1.000	1.000
10.800	135.69	2438.	4429.	16714.	16104.	14884.	2153.	1.000	0.000	0.000	1.000	1.000
10.900	138.62	2452.	4318.	16310.	15716.	14527.	2142.	1.000	0.000	0.000	1.000	1.000
11.000	141.57	2466.	4210.	15921.	15342.	14182.	2131.	1.000	0.000	0.000	1.000	1.000
11.100	144.54	2479.	4107.	15547.	14981.	13850.	2121.	1.000	0.000	0.000	1.000	1.000
11.200	147.52	2492.	4007.	15186.	14634.	13531.	2110.	1.000	0.000	0.000	1.000	1.000
11.300	150.52	2505.	3911.	14838.	14299.	13222.	2100.	1.000	0.000	0.000	1.000	1.000
11.400	153.53	2517.	3818.	14502.	13976.	12925.	2090.	1.000	0.000	0.000	1.000	1.000
11.500	156.56	2530.	3728.	14178.	13664.	12638.	2080.	1.000	0.000	0.000	1.000	1.000
11.600	159.61	2541.	3642.	13865.	13363.	12360.	2070.	1.000	0.000	0.000	1.000	1.000
11.700	162.66	2553.	3558.	13562.	13072.	12093.	2060.	1.000	0.000	0.000	1.000	1.000
11.800	165.73	2564.	3478.	13270.	12791.	11834.	2051.	1.000	0.000	0.000	1.000	1.000
11.900	168.82	2575.	3400.	12988.	12520.	11584.	2042.	1.000	0.000	0.000	1.000	1.000
12.000	171.91	2586.	3324.	12715.	12257.	11342.	2032.	1.000	0.000	0.000	1.000	1.000
12.100	175.02	2597.	3251.	12451.	12003.	11103.	2023.	1.000	0.000	0.000	1.000	1.000
12.200	178.15	2607.	3180.	12195.	11758.	10882.	2015.	1.000	0.000	0.000	1.000	1.000
12.300	181.28	2617.	3112.	11948.	11520.	10663.	2006.	1.000	0.000	0.000	1.000	1.000
12.400	184.43	2627.	3046.	11709.	11289.	10451.	1997.	1.000	0.000	0.000	1.000	1.000
12.500	187.59	2637.	2982.	11477.	11066.	10245.	1989.	1.000	0.000	0.000	1.000	1.000
12.600	190.76	2646.	2920.	11252.	10850.	10046.	1980.	1.000	0.000	0.000	1.000	1.000
12.700	193.94	2656.	2859.	11034.	10640.	9853.	1972.	1.000	0.000	0.000	1.000	1.000
12.800	197.13	2665.	2801.	10823.	10437.	9656.	1964.	1.000	0.000	0.000	1.000	1.000
12.900	200.33	2674.	2744.	10618.	10240.	9484.	1956.	1.000	0.000	0.000	1.000	1.000
13.000	203.55	2683.	2689.	10419.	10049.	9308.	1948.	1.000	0.000	0.000	1.000	1.000
13.045	205.00	2666.	2665.	10331.	9964.	9231.	1945.	1.000	0.000	0.000	1.000	1.000
PROJECTILE EXIT												

CONDITIONS AT:	P MAX	MUZZLE
TIME (MS):	5.173	13.045
TRAVEL (IN):	14.59	205.00
VELOCITY (FT/S):	896.	2686.
ACCELERATION (G):	12247.	2665.
BREECH PRESS (PSI):	45000.	10331.
MEAN PRESS (PSI):	43314.	9964.
BASE PRESS (PSI):	39942.	9231.
MEAN TEMP (K):	2857.	1945.
Z CHARGE 1 (-):	1.000	1.000
Z CHARGE 2 (-):	0.000	0.000
Z CHARGE 3 (-):	0.000	0.000
Z CHARGE 4 (-):	1.000	1.000
Z CHARGE 5 (-):	0.427	1.000

ENERGY BALANCE SUMMARY	IN-LB	%
TOTAL CHEMICAL:	431019520.	100.00
(1) INTERNAL GAS:	271604224.	63.01
(2) WORK AND LOSSES:	159415406.	36.99
(A) PROJECTILE KINETIC:	129055072.	29.95
(B) GAS KINETIC:	11045006.	2.56
(C) PROJECTILE ROTATIONAL:	1592645.	0.37
(D) FRICTIONAL WORK TO TUBE:	0.	0.00
(E) OTHER FRICTIONAL WORK:	3175198.	0.74
(F) WORK DONE AGAINST AIR:	612820.	0.14
(G) HEAT CONVECTED TO BORE:	13894672.	3.22
(H) RECOIL ENERGY:	0.	0.00
LOADING DENSITY (G/CM3):	0.593	
CHARGE WT/PROJECTILE WT:	0.257	
PIEZOMETRIC EFFICIENCY:	0.469	
EXPANSION RATIO:	6.317	

Test Case 5

This is another example of deterred propellant grains for the second \$PROP deck. A transition zone of 0.001 thickness is added to gain a smooth transition from the outer shell to the inner propellant. An obvious correction by the program is shown where the second propellant grain diameter is input as five inches, then corrected to 0.4837 in the form function subroutine when the web distances and perforation diameters are added.

Using the \$FIND deck, the program is directed to search for a solution where peak breech pressure is 63000 psi and muzzle velocity of the projectile is maximized. The searching method employed is a function minimization routine developed at BRL many years ago, and will be replaced by another technique in the future. The current code does find solutions when possible, but actual 'best case' may elude the algorithm. In the run output, a table of trial values follows the input card echoes where each line represents a full ballistic calculation by IBHVG2.

```

SCOMM
IBHVG2 BENCHMARK TEST CASE 5

SHOW DETERRED PROPELLANT EXAMPLE
USE 'FIND' FUNCTION TO SEARCH FOR SPECIFIC SOLUTION

SHEAT
  TSHL = 0.00450      CSHL = 1848      RSHL = 0.284
  THAL = 293          HO = 0.0648      HL = 1

SGUN
  NAME = '120MM GUN'  CHAM = 525      GRVE = 4.724
  LAND = 4.724        G/L = 1.        TRAV = 187.11
  TWST = 99

SPROJ
  NAME = 'APFSDS'     PRWT = 21.1

SRESI
  NPTS = 4            AIR = 1
  TRAV = 0, 0.8, 3.0, 187
  PRES = 100, 2500, 100, 100

SINFO
  RUN = '120 MM GUN DETERRED-120DEY'  DELT = 5E-5      DELP = 5E-5
  GRAD = 2                            POPT = 1,1,1,0,2    SOPT = 0
  EPS = 0.05                          COMP = 0

SRECO
  NAME = 'NONE'        RECO = 0          RCWT = 0

SPRIM
  NAME = 'BENITE'      CHWT = 0.00347
  GAMA = 1.25          FORC = 212500
  COV = 30             TEMP = 2000

SPROP
  NAME = 'BENITE'      CHWT = 0.06653  GRAM = 'CORD'
  RHO = 0.06           GAMA = 1.25      FORC = 212500
  COV = 30             TEMP = 2000      EROS = 0.00000
  ALPH = 0             BETA = 27        IGNC = 0
  LEN = 9.998          DIAM = 0.078

SCOMM
VARY WEB AND CHARGE WEIGHT OF SECOND PROPELLANT TO FIND
A SOLUTION AT APPROX 63KPSI AND MAXIMUM MUZZLE VELOCITY

$FIND
VARY='WEB' FROM=.070 VAL=63000 NTH=2 OUTV='PMAV' CODE=0
MIN=0.063 DECK='PROP' EPS=0.0001

$FIND

```

VARY='CHWT' DECK='PROP' NTH=2 FROM=20.0 EPS=0.01 OUTV='VMUZ'
CODE=1 MULT=0.5 MIN=18. MAX=22.

SCOMM

OUTER LAYER HAS LOW BURNING RATE (DETERRED), NEXT LAYER IS A THIN
TRANSITION ZONE, AND CORE LAYER (4) IS THE MAIN PROPELLANT

\$PROP

NAME = 'JA2-G54 0.85-0.15 19P' CHWT = 20.5 GRAN = '19PF'
RHO=0.05732 EROS = 0.0000000
LEN = 3 DIAM = 5 PD = 0.020 WEB=0.0625

GUMP=,1.2725,1.2725,1.2257 GAME=,1.2725,1.2725,1.2257
GANL=,1.2725,1.2725,1.2257

COVP=,31.17,31.17,27.48 COVE=,31.17,31.17,27.48
COVL=,31.17,31.17,27.48

TMPL=,2248,2248,3400 TMPE=,2248,2248,3400 TMPP=,2248,2248,3400

FRCL=,300417,300417,382152 FRCE=,300417,300417,382152
FRCP=,300417,300417,382152

DEPP=,0.03,0.031 DEPE=,0.03,0.031 DEPL=,0.03,0.031

NTBL=4 PR4L=2000,4000,10000,25000
BR4L=1.05,1.52,2.93,6.56
PR3L=2000,4000,10000,25000 PR2L=2000,4000,10000,25000
BR3L=0.694,1.01,1.94,4.34 BR2L=0.694,1.01,1.94,4.34
PR4P=2000,4000,10000,25000 BR4P=1.05,1.52,2.93,6.56
PR3P=2000,4000,10000,25000 BR3P=0.694,1.01,1.94,4.34
PR2P=2000,4000,10000,25000 BR2P=0.694,1.01,1.94,4.34
PR4E=2000,4000,10000,25000 BR4E=1.05,1.52,2.93,6.56
PR3E=2000,4000,10000,25000 BR3E=0.694,1.01,1.94,4.34
PR2E=2000,4000,10000,25000 BR2E=0.694,1.01,1.94,4.34

SCOMM

THIRD AND FOURTH PROPELLANTS MAKE UP A COMBUSTIBLE CARTRIDGE CASE
OF FELTED NITRO-CELLULOSE AND KRAFT PAPER

\$PROP

NAME = 'FNC CASE' CHWT = 1.41 GRAN = '1PF'
RHO = 0.04 GAMA = 1.258
FRCP = ,150000,150000 FRCE = ,150000,150000 FRCL(4)=200000
COV = 27.927 TEMP = 1610 EROS = 0.00
IGNS(3)=2 THRS(3)=200 DEPP= , 0.015 , 0.0155 DEPE= , 0.015 , 0.0155
NTBL=2
PR2P=1000,10000 BR2P=0.5,2.4 PR3P=1000,10000 BR3P=0.5,2.4
PR2E=1000,10000 BR2E=0.5,2.4 PR3E=1000,10000 BR3E=0.5,2.4
PR4L=1000,10000 BR4L=0.5,10
LEN = 18 DIAM = 6.17 PD = 6.01
WI = 0.08

\$PROP

NAME = 'KRAFT CASE' CHWT = .21 GRAN = '1PF'
RHO = 0.04 GAMA = 1.2734 FOWC = 95726
COV = 9.883 TEMP = 1054 EROS = 0.00
ALPH = 1 BETA = 0.00001 IGNC = 0
LEN = 3.4 DIAM = 6.17 PD = 6.01
WI = 0.08

SEND

Producing the following output:

ERRTOL= 4.768372E-07

```
CARD 1 --- $COMM
CARD 2 --- IBHVG2 BENCHMARK TEST CASE 5
CARD 3 ---
CARD 4 --- SHOW DETERRED PROPELLANT EXAMPLE
CARD 5 --- USE 'FIND' FUNCTION TO SEARCH FOR SPECIFIC SOLUTION
CARD 6 ---
CARD 7 --- $HEAT
CARD 8 --- TSHL = 0.00450      CSHL = 1848      RSHL = 0.284
CARD 9 --- TWAL = 293        HO = 0.0648      HL = 1
CARD 10 ---
CARD 11 --- $GUN
CARD 12 --- NAME = '120MM GUN'  CHAM = 525      GRVE = 4.724
CARD 13 --- LAND = 4.724      G/L = 1.        TRAV = 187.11
CARD 14 --- TWST = 99
CARD 15 ---
CARD 16 --- $PROJ
CARD 17 --- NAME = 'APFSDS'  PRWT = 21.1
CARD 18 ---
CARD 19 --- $RESI
CARD 20 --- NPTS = 4          AIR = 1
CARD 21 --- TRAV = 0, 0.8, 3.0 187
CARD 22 --- PRES = 100, 2500, 100, 100
CARD 23 ---
CARD 24 --- $INFO
CARD 25 --- RUN = '120 MM GUN DETERRED-120DET'  DELT = 5E-5  DCLP = 5E-5
CARD 26 --- GRAD = 2          POPT = 1,1,1,0,2  SOPT = 0
CARD 27 --- EPS = 0.05      COMP = 0
CARD 28 ---
CARD 29 --- $RECO
CARD 30 --- NAME = 'NONE'      RECO = 0          RCWT = 0
CARD 31 ---
CARD 32 --- $PRIM
CARD 33 --- NAME = 'BENITE'    CHWT = 0.00347
CARD 34 --- GAMA = 1.25      FORC = 212500
CARD 35 --- COV = 30        TEMP = 2000
CARD 36 --- $PROP
CARD 37 --- NAME = 'BENITE'    CHWT = 0.06653  GRAN = 'CORD'
CARD 38 --- RHO = 0.06      GAMA = 1.25      FORC = 212500
CARD 39 --- COV = 30        TEMP = 2000      EROS = 0.00000
CARD 40 --- ALPH = 0        BETA = 27       IGNC = 0
CARD 41 --- LEN = 9.998     DIAM = 0.078
CARD 42 ---
CARD 43 --- $COMM
CARD 44 --- VARY WEB AND CHARGE WEIGHT OF SECOND PROPELLANT TO FIND
CARD 45 --- A SOLUTION AT APPROX 63KPSI AND MAXIMUM MUZZLE VELOCITY
CARD 46 --- $FIND
CARD 47 --- VARY='WEB' FROM=.070 VAL=63000 NTH=2 OUTV='PMAX' CODE=0
CARD 48 --- MIN=0.063 DECK='PROP' EPS=0.0001
CARD 49 --- $FIND
CARD 50 --- VARY='CHWT' DECK='PROP' NTH=2 FROM=20.0 EPS=0.01 OUTV='VMUZ'
CARD 51 --- CODE=1 MULT=0.5 MIN=18. MAX=22.
CARD 52 ---
CARD 53 --- $COMM
CARD 54 --- OUTER LAYER HAS LOW BURNING RATE (DETERRED), NEXT LAYER IS A THIN
CARD 55 --- TRANSITION ZONE, AND CORE LAYER (4) IS THE MAIN PROPELLANT
```

```

CARD 56 --> $PROP
CARD 57 --> NAME = 'JA2-G54 .85-.15 19P' CHWT = 20.5 GRAM = '19PF'
CARD 58 --> RHO=0.05732 EROS = 0.0000000
CARD 59 --> LEN = 3 DIAM = 5 PD = 0.020 WEB=0.0625
CARD 60 -->
CARD 61 --> GAMP=,1.2725,1.2725,1.2257 GAME=,1.2725,1.2725,1.2257
CARD 62 --> GAHL=,1.2725,1.2725,1.2257
CARD 63 -->
CARD 64 --> COVP=,31.17,31.17,27.48 COVE=,31.17,31.17,27.48
CARD 65 --> COVL=,31.17,31.17,27.48
CARD 66 -->
CARD 67 --> TMPL=,2248,2248,3400 TMPE=,2248,2248,3400 TMPP=,2248,2248,3400
CARD 68 -->
CARD 69 --> FRCL=,300417,300417,382152 FRCE=,300417,300417,2152
CARD 70 --> FRCP=,300417,300417,382152
CARD 71 -->
CARD 72 --> DEPP=,0.03,0.031 DEPE=,0.03,0.031 DEPL=,0.03,0.031
CARD 73 -->
CARD 74 --> NTBL=4 PR4L=2000,4000,10000,25000
CARD 75 --> BR4L=1.05,1.52,2.93,6.56
CARD 76 --> PR3L=2000,4000,10000,25000 PR2L=2000,4000,10000,25000
CARD 77 --> BR3L=0.694,1.01,1.94,4.34 BR2L=0.694,1.01,1.94,4.34
CARD 78 --> PR4P=2000,4000,10000,25000 BR4P=1.05,1.52,2.93,6.56
CARD 79 --> PR3P=2000,4000,10000,25000 BR3P=0.694,1.01,1.94,4.34
CARD 80 --> PR2P=2000,4000,10000,25000 BR2P=0.694,1.01,1.94,4.34
CARD 81 --> PR4E=2000,4000,10000,25000 BR4E=1.05,1.52,2.93,6.56
CARD 82 --> PR3E=2000,4000,10000,25000 BR3E=0.694,1.01,1.94,4.34
CARD 83 --> PR2E=2000,4000,10000,25000 BR2E=0.694,1.01,1.94,4.34
CARD 84 -->
CARD 85 --> $COMM
CARD 86 --> THIRD AND FOURTH PROPELLANTS MAKE UP A COMBUSTIBLE CARTRIDGE CASE
CARD 87 --> OF FELTED NITRO-CELLULOSE AND KRAFT PAPER
CARD 88 --> $PROP
CARD 89 --> NAME = 'FNC CASE' CHWT = 1.41 GRAM = '1PF'
CARD 90 --> RHO = 0.04 GAMA = 1.258
CARD 91 --> FRCP=,150000,150000 FRCE=,150000,150000 FRCL(4)=200000
CARD 92 --> COV = 27.927 TEMP = 1610 EROS = 0.00
CARD 93 --> IGNS(3)=2 THRS(3)=200 DEPP=,0.015,0.0155 DEPE=,0.015,0.0155
CARD 94 --> NTBL=2
CARD 95 --> PR2P=1000,10000 BR2P=0.5,2.4 PR3P=1000,10000 BR3P=0.5,2.4
CARD 96 --> PR2E=1000,10000 BR2E=0.5,2.4 PR3E=1000,10000 BR3E=0.5,2.4
CARD 97 --> PR4L=1000,10000 BR4L=0.5,10
CARD 98 --> LEN = 18 DIAM = 6.17 PD = 6.01
CARD 99 --> WI = 0.08
CARD 100 --> $PROP
CARD 101 --> NAME = 'KRAFT CASE' CHWT = .21 GRAM = '1PF'
CARD 102 --> RHO = 0.04 GAMA = 1.2734 FORC = 95726
CARD 103 --> COV = 9.803 TEMP = 1054 EROS = 0.00
CARD 104 --> ALPH = 1 BETA = 0.00001 IGNC = 0
CARD 105 --> LEN = 3.4 DIAM = 6.17 PD = 6.01
CARD 106 --> WI = 0.03
CARD 107 --> $END

```


VARY / 1/ WEB	2	PROP TO HIT < 1>	PWAX	= 0.6300E+05
VARY / 2/ CHWT	2	PROP TO MAX < 2>	PWUZ	

/ 1/	< 1>	/ 2/	< 2>
0.7000E-01	0.4430E+05	20.00	3520.
0.7011E-01	0.4414E+05	20.00	3513.
0.6989E-01	0.4445E+05	20.00	3528.
0.6945E-01	0.4508E+05	20.00	3555.
0.6945E-01	0.4519E+05	20.01	3561.
0.6945E-01	0.4530E+05	20.02	3564.
0.6945E-01	0.4562E+05	20.05	3573.
0.6890E-01	0.4701E+05	20.11	3627.
0.6395E-01	0.6323E+05	20.60	4224.
0.6395E-01	0.6412E+05	20.66	4019.
0.6395E-01	0.6236E+05	20.55	4202.
0.6395E-01	0.6299E+05	20.59	4217.
0.6340E-01	0.6533E+05	20.64	4287.
0.6450E-01	0.6078E+05	20.53	415.
0.6395E-01	0.6275E+05	20.57	4214.
0.6395E-01	0.6323E+05	20.60	4224.
0.6395E-01	0.6275E+05	20.57	4214.
0.6385E-01	0.6341E+05	20.60	4231.
0.6405E-01	0.6258E+05	20.58	4201.

 - GUN TUBE -

 TYPE: 120MM GUN
 GROOVE DIAMETER (IN): 4.724
 TWIST (CALS/TURN): 99.0
 SHELL THICKNESS (IN): 0.004500
 INITIAL SHELL TEMP (K): 293.

 - PROJECTILE -

 TYPE: APFSDS

 - RESISTANCE -

 AIR RESISTANCE OPTION: 1
 I TRAVEL (IN) PRESSURE (PSI)
 1 0.00 100.
 2 0.80 2500.

 - GENERAL -

 MAX TIME STEP (S): 0.000050
 PRINT OPTIONS: 1 1 1 0 2 1
 GRADIENT MODEL: P100JACK-KENT

 - RECOIL -

 RECOIL OPTION: 0

 - PRIMER -

 TYPE: WHITE
 CONVOLUME (IN3/LB): 30.000

 CHAMBER VOLUME (IN3): 525.00
 LAND DIAMETER (IN): 4.724
 BORE AREA (IN2): 17.5271
 SHELL CP (IN-LB/LB-K): 1848.0
 AIR W0 (IN-LB/IN2-S-K): 0.06480

 TRAVEL (IN): 187.11
 GROOVE/LAND RATIO (-): 1.000
 HEAT-LOSS OPTION: 1
 SHELL DENSITY (LB/IN3): 0.2840

 TOTAL WEIGHT (LB): 21.100
 WEIGHT PREDICTOR OPTION: 0

 WALL HEATING FRACTION: 0.000
 I TRAVEL (IN) PRESSURE (PSI)
 3 3.00 100.
 4 187.00 100.

 FRICTION TABLE LENGTH: 4
 I TRAVEL (IN) PRESSURE (PSI)
 4 187.00 100.

 PRINT STEP (S): 0.000050
 STORE OPTION: 0

 TYPE: NONE

 RECOIL WEIGHT (LB): 0.

 GAMMA (-): 1.2500
 FLAME TEMP (K): 2000.0

 FORCE (FT-LB/LB): 212500.
 WEIGHT (LB): 0.003470

 - CHARGE 1 -

TYPE: BENITE	GRAINS:	23.210	CORO	0	WEIGHT (LB):	0.0665
EROSIVE COEFF (-):	CHARGE IGM CODE:		0	CHARGE IGM AT (S):	0.00000E+00	
GRAIN LENGTH (IN):	GRAIN DIAMETER (IN):	0.07800				

	PROPERTIES AT LAYER BOUNDARIES OF END SURFACES	PROPERTIES AT LAYER BOUNDARIES OF LAT SURFACES
	1ST 2ND 3RD 4TH	1ST 2ND 3RD 4TH
AT DEPTH (IN):	---	---
ADJACENT LAYER VT %:	---	---
DENSITY (LB/IN3):	---	---
GAMMA (-):	---	---
FORCE (FT-LB/LB):	---	---
COVOLUME (IN3/LB):	---	---
FLAME TEMP (K):	---	---
BURNING RATE EXPS:	---	---
BURNING RATE COEFFS:	---	---

- CHARGE 2 -

TYPE: J42-G54	.85-.15	19P	GRAINS:	673.47	19P	WEIGHT (LB):	20.5897
EROSIVE COEFF (-):	0.000000		CHARGE IGM CODE:			CHARGE IGM AT (\$):	0.00000E+00
GRAIN LENGTH (IN):	3.00000		GRAIN DIAMETER (IN):		0.48370	PERF DIAMETER (IN):	0.02000
INNER WEB (IN):	0.06395		MIDDLE WEB (IN):		0.06395	OUTER WEB (IN):	0.06395

PROPERTIES AT LAYER BOUNDARIES OF PERF SURFACES		PROPERTIES AT LAYER BOUNDARIES OF END SURFACES	
1ST	2ND	1ST	3RD
AT DEPTH (IN):	0.00000	0.03100	0.03100
ADJACENT LAYER VT %:	49.756	21.665	21.665
DENSITY (LB/IN3):	0.05732	0.05732	0.05732
GAMMA (-):	1.2725	1.2725	1.2725
FORCE (FT-LB/LB):	300417.	300417.	300417.
COVOLUME (IN3/LB):	31.170	27.480	27.480
FLAME TEMP (K):	2248.0	2248.0	2248.0
MEAN PRESSURES (PSI):	2000.0	2000.0	2000.0
MEAN PRESSURES (PSI):	4000.0	4000.0	4000.0
MEAN PRESSURES (PSI):	10000.0	10000.0	10000.0
MEAN PRESSURES (PSI):	25000.0	25000.0	25000.0
BURNING RATES (IN/S):	0.69	1.05	1.05
BURNING RATES (IN/S):	1.01	1.52	1.52
BURNING RATES (IN/S):	1.94	2.93	2.93
BURNING RATES (IN/S):	4.34	6.56	6.56

PROPERTIES AT LAYER BOUNDARIES OF LAT SURFACES

1ST	2ND	3RD	4TH
AT DEPTH (IN):	0.00000	0.03100	0.03100
ADJACENT LAYER VT %:	23.816	21.665	21.665
DENSITY (LB/IN3):	0.05732	0.05732	0.05732
GAMMA (-):	1.2725	1.2725	1.2725
FORCE (FT-LB/LB):	300417.	300417.	300417.
COVOLUME (IN3/LB):	31.170	27.480	27.480
FLAME TEMP (K):	2248.0	2248.0	2248.0
MEAN PRESSURES (PSI):	2000.0	2000.0	2000.0
MEAN PRESSURES (PSI):	4000.0	4000.0	4000.0
MEAN PRESSURES (PSI):	10000.0	10000.0	10000.0
MEAN PRESSURES (PSI):	25000.0	25000.0	25000.0
BURNING RATES (IN/S):	0.69	1.05	1.05
BURNING RATES (IN/S):	1.01	1.52	1.52
BURNING RATES (IN/S):	1.94	2.93	2.93
BURNING RATES (IN/S):	4.34	6.56	6.56

- CHARGE 3 -

TYPE: FNC CASE	0.000000	GRAINS:	1.2795	1PF	WEIGHT (LB):	1.4100
EROSIVE COEFF (-):	0	CHARGE IGM CODE:		0	CHARGE IGM AT (S):	0.00000E+00
P-SURFACE IGM CODE:	0.00000E+00	E-SURFACE IGM CODE:		0	L-SURFACE IGM CODE:	2
P-SURF IGM AT (S):	16.00000	E-SURF IGM AT (S):	0.00000E+00		L-SURF IGM AT (IN):	0.20000E+03
GRAIN LENGTH (IN):	0.08000	GRAIN DIAMETER (IN):		6.17000	PERF DIAMETER (IN):	6.01000
INNER WEB (IN):		WEB RATIO:		1.0000		

AT DEPTH (IN):	1ST	2ND	3RD	4TH	PROPERTIES AT LAYER BOUNDARIES OF PERF SURFACES	1ST	2ND	3RD	4TH	PROPERTIES AT LAYER BOUNDARIES OF END SURFACES
ADJACENT LAYER UT %:	---	0.00000	0.01500	0.01550		---	0.00000	0.01500	0.01550	
DENSITY (LB/IN3):	---	18.535	0.618	80.690		---	0.151	0.005	80.690	
GAMMA (-):	---	0.04000	0.04000	0.04000		---	0.04000	0.04000	0.04000	
FORCE (FT-LB/LB):	---	1.2580	1.2580	1.2580		---	1.2580	1.2580	1.2580	
CONVOLUME (IN3/LB):	---	150000.	150000.	200000.		---	150000.	150000.	200000.	
FLAME TEMP (K):	---	27.927	27.927	27.927		---	27.927	27.927	27.927	
MEAN PRESSURES (PSI):	---	1610.0	1610.0	1610.0		---	1610.0	1610.0	1610.0	
MEAN PRESSURES (PSI):	---	1000.0	1000.0	1000.0		---	1000.0	1000.0	1000.0	
BURNING RATES (IN/S):	---	10000.0	10070.0	10000.0		---	10000.0	10000.0	10000.0	
BURNING RATES (IN/S):	---	0.50	0.50	0.50		---	0.50	0.50	0.50	
BURNING RATES (IN/S):	---	2.40	2.40	10.00		---	2.40	2.40	10.00	

AT DEPTH (IN):	1ST	2ND	3RD	4TH	PROPERTIES AT LAYER BOUNDARIES OF LAT SURFACES
ADJACENT LAYER UT %:	---	---	---	0.00000	
DENSITY (LB/IN3):	---	---	---	80.690	
GAMMA (-):	---	---	---	0.04000	
FORCE (FT-LB/LB):	---	---	---	1.2580	
CONVOLUME (IN3/LB):	---	---	---	200000.	
FLAME TEMP (K):	---	---	---	27.927	
MEAN PRESSURES (PSI):	---	---	---	1610.0	
MEAN PRESSURES (PSI):	---	---	---	1000.0	
BURNING RATES (IN/S):	---	---	---	10000.0	
BURNING RATES (IN/S):	---	---	---	0.50	
BURNING RATES (IN/S):	---	---	---	2.40	

- CHARGE 4 -

TYPE: KRAFT CASE
EROSIVE COEFF (-):
GRAIN LENGTH (IN):
INNER WEB (IN):

0.000000
3.40000
0.08000

GRAINS:
CHARGE IGM CODE:
GRAIN DIAMETER (IN):
WEB RATIO:

1.0058
0.00000
0.00000

1PF 0
6.17000
1.0000

WEIGHT (LB):
CHANGE IGM AT (S):
PERF DIAMETER (IN):

0.2100
0.00000E+00
6.01000

PROPERTIES AT LAYER BOUNDARIES OF PERF SURFACES			
1ST	2ND	3RD	4TH
AT DEPTH (IN):	-----	-----	-----
ADJACENT LAYER WT %:	-----	-----	-----
DENSITY (LB/IN3):	-----	-----	-----
GAMMA (-):	-----	-----	-----
FORCE (FT-LB/LB):	-----	-----	-----
COVOLUME (IN3/LB):	-----	-----	-----
FLAME TEMP (K):	-----	-----	-----
BURNING RATE EXPS:	-----	-----	-----
BURNING RATE COEFFS:	-----	-----	-----
	0.000000	0.000000	0.000000
	100.000	100.000	100.000
	0.04000	0.04000	0.04000
	1.2734	1.2734	1.2734
	95726.	95726.	95726.
	9.883	9.883	9.883
	1054.0	1054.0	1054.0
	1.0000	1.0000	1.0000
	0.0000100	0.0000100	0.0000100

PROPERTIES AT LAYER BOUNDARIES OF LAT SURFACES			
1ST	2ND	3RD	4TH
AT DEPTH (IN):	-----	-----	-----
ADJACENT LAYER WT %:	-----	-----	-----
DENSITY (LB/IN3):	-----	-----	-----
GAMMA (-):	-----	-----	-----
FORCE (FT-LB/LB):	-----	-----	-----
COVOLUME (IN3/LB):	-----	-----	-----
FLAME TEMP (K):	-----	-----	-----
BURNING RATE EXPS:	-----	-----	-----
BURNING RATE COEFFS:	-----	-----	-----
	0.000000	0.000000	0.000000
	100.000	100.000	100.000
	0.04000	0.04000	0.04000
	1.2734	1.2734	1.2734
	95726.	95726.	95726.
	9.883	9.883	9.883
	1054.0	1054.0	1054.0
	1.0000	1.0000	1.0000
	0.0000100	0.0000100	0.0000100

TIME (MS)	TRAV (IN)	VEL (F1/S)	ACC (G)	BREECH PRESS (PSI)	MEAN PRESS (PSI)	MEAN PRESS (PSI)	MEAN TEMP (K)	FRAC BURN 1	FRAC BURN 2	FRAC BURN 3	FRAC BURN 4
0.000	0.00	0.	0.	71.	71.	71.	2000.	0.000	0.000	0.000	0.000
0.010	0.00	0.	0.	101.	101.	101.	2023.	0.013	0.000	0.000	0.000
SHOT-START PRESSURE ACHIEVED											
0.050	0.00	0.	73.	281.	248.	187.	2067.	0.068	0.000	0.000	0.000
0.100	0.00	0.	212.	533.	470.	355.	2093.	0.134	0.000	0.000	0.000
0.150	0.00	1.	377.	832.	734.	555.	2110.	0.198	0.001	0.000	0.000
0.200	0.00	1.	565.	1176.	1037.	784.	2122.	0.259	0.001	0.001	0.000
0.250	0.00	3.	777.	1563.	1378.	1042.	2131.	0.317	0.001	0.001	0.000
0.300	0.00	4.	1010.	1993.	1758.	1328.	2139.	0.373	0.002	0.002	0.000
0.350	0.01	6.	1264.	2465.	2174.	1643.	2145.	0.427	0.002	0.002	0.000
0.400	0.01	8.	1539.	2980.	2629.	1986.	2151.	0.478	0.003	0.003	0.000
0.450	0.02	11.	1833.	3537.	3120.	2357.	2155.	0.527	0.004	0.003	0.000
0.500	0.02	14.	2146.	4137.	3649.	2757.	2159.	0.574	0.004	0.004	0.000
0.550	0.03	18.	2478.	4779.	4215.	3185.	2162.	0.618	0.005	0.005	0.000
0.600	0.05	22.	2834.	5475.	4829.	3649.	2165.	0.659	0.006	0.006	0.000
0.650	0.06	27.	3215.	6230.	5495.	4152.	2167.	0.699	0.007	0.007	0.000
0.700	0.08	32.	3623.	7045.	6215.	4696.	2169.	0.735	0.008	0.008	0.000
0.750	0.10	39.	4056.	7924.	6989.	5281.	2171.	0.770	0.009	0.009	0.001
0.800	0.12	45.	4515.	8866.	7821.	5909.	2172.	0.802	0.011	0.010	0.001
0.850	0.15	53.	4999.	9874.	8710.	6581.	2173.	0.831	0.012	0.011	0.001
0.900	0.19	62.	5508.	10948.	9657.	7296.	2173.	0.859	0.014	0.013	0.001
0.950	0.23	71.	6042.	12092.	10666.	8059.	2173.	0.883	0.015	0.014	0.001
1.000	0.27	81.	6610.	13322.	11752.	8879.	2173.	0.906	0.017	0.016	0.001
1.050	0.33	92.	7211.	14643.	12916.	9759.	2172.	0.926	0.019	0.017	0.001
1.100	0.38	104.	7847.	16057.	14164.	10701.	2171.	0.943	0.021	0.019	0.001
1.150	0.45	117.	8517.	17566.	15495.	11707.	2169.	0.959	0.023	0.021	0.002
1.200	0.53	132.	9220.	19172.	16912.	12777.	2167.	0.972	0.026	0.023	0.002
1.250	0.61	147.	9954.	20876.	18414.	13912.	2164.	0.982	0.029	0.026	0.002
1.300	0.70	164.	10718.	22675.	20002.	15112.	2161.	0.990	0.031	0.028	0.002
1.350	0.81	182.	11527.	24570.	21673.	16375.	2157.	0.996	0.035	0.030	0.003
1.400	0.92	201.	12730.	26556.	23425.	17698.	2153.	0.999	0.038	0.033	0.003
1.444	1.03	220.	13848.	28392.	25045.	18922.	2148.	1.000	0.041	0.035	0.003
PROPELLANT 1 BURNED OUT											
1.450	1.05	223.	13991.	28626.	25251.	19078.	2148.	1.000	0.042	0.036	0.003
1.500	1.19	246.	15307.	30774.	27146.	20509.	2142.	1.000	0.046	0.039	0.004
1.550	1.34	272.	16674.	32991.	29101.	21986.	2136.	1.000	0.050	0.042	0.004
1.600	1.51	300.	18086.	35261.	31103.	23499.	2129.	1.000	0.054	0.045	0.004
1.650	1.70	330.	19534.	37569.	33139.	25037.	2121.	1.000	0.059	0.048	0.005
1.700	1.91	363.	21010.	39895.	35191.	26588.	2113.	1.000	0.065	0.052	0.005
1.750	2.14	398.	22502.	42220.	37241.	28137.	2104.	1.000	0.070	0.055	0.006
1.800	2.39	435.	24000.	44518.	39269.	29668.	2094.	1.000	0.076	0.059	0.006
1.850	2.66	475.	25491.	46766.	41252.	31167.	2083.	1.000	0.082	0.063	0.007
1.900	2.96	517.	26963.	48939.	43168.	32614.	2072.	1.000	0.089	0.067	0.007
1.950	3.28	562.	28145.	51012.	44997.	33996.	2060.	1.000	0.095	0.071	0.008
2.000	3.63	608.	29224.	52963.	46718.	35296.	2048.	1.000	0.103	0.075	0.008
2.050	4.01	656.	30224.	54772.	48314.	36502.	2035.	1.000	0.110	0.079	0.009
2.100	4.42	705.	31137.	56423.	49771.	37602.	2021.	1.000	0.118	0.084	0.010
2.150	4.86	756.	31953.	57901.	51074.	38587.	2008.	1.000	0.126	0.088	0.010
2.200	5.33	808.	32668.	59196.	52216.	39450.	1994.	1.000	0.134	0.093	0.011
2.250	5.83	861.	33278.	60300.	53190.	40186.	1979.	1.000	0.143	0.097	0.011
2.300	6.36	915.	33780.	61210.	53993.	40792.	1965.	1.000	0.152	0.102	0.012
2.350	6.93	970.	34175.	61927.	54625.	41270.	1951.	1.000	0.161	0.107	0.013
2.400	7.53	1025.	34464.	62454.	55090.	41621.	1936.	1.000	0.170	0.112	0.014
2.450	8.16	1081.	34653.	62798.	55393.	41850.	1922.	1.000	0.179	0.116	0.014
2.500	8.82	1137.	34745.	62968.	55544.	41964.	1908.	1.000	0.188	0.121	0.015

TIME (MS)	TRAV (IN)	VEL (FT/S)	ACC (G)	BREECH PRESS (PSI)	MEAN PRESS (PSI)	BASE PRESS (PSI)	MEAN TEMP (K)	FRAC BURN 1	FRAC BURN 2	FRAC BURN 3	FRAC BURN 4
2.527	9.20	1167.	34756.	62991.	55564.	41979.	1900.	1.000	0.194	0.124	0.015
LOCAL PRESSURE MAX DETECTED											
2.550	9.52	1193.	34746.	62975.	55550.	41969.	1894.	1.000	0.199	0.126	0.016
2.600	10.26	1249.	34665.	62832.	55424.	41873.	1880.	1.000	0.208	0.131	0.016
2.650	11.02	1304.	34507.	62552.	55176.	41686.	1866.	1.000	0.218	0.136	0.017
2.700	11.82	1360.	34281.	62148.	54821.	41418.	1853.	1.000	0.228	0.140	0.018
2.750	12.65	1415.	33995.	61636.	54368.	41076.	1840.	1.000	0.238	0.145	0.019
2.800	13.52	1469.	33656.	61028.	53832.	40671.	1827.	1.000	0.248	0.150	0.019
2.850	14.42	1523.	33271.	60338.	53223.	40211.	1815.	1.000	0.258	0.155	0.020
2.900	15.35	1576.	32848.	59578.	52553.	39704.	1803.	1.000	0.268	0.159	0.021
2.950	16.31	1629.	32392.	58760.	51832.	39160.	1791.	1.000	0.278	0.164	0.021
3.000	17.30	1680.	31910.	57895.	51069.	38583.	1780.	1.000	0.288	0.168	0.022
3.050	18.32	1731.	31408.	56993.	50273.	37982.	1768.	1.000	0.298	0.173	0.023
3.100	19.38	1782.	30890.	56062.	49452.	37361.	1758.	1.000	0.308	0.177	0.023
3.150	20.46	1831.	30360.	55110.	48612.	36727.	1747.	1.000	0.318	0.182	0.024
3.200	21.57	1879.	29823.	54145.	47761.	36084.	1737.	1.000	0.328	0.186	0.024
3.221	22.05	1900.	29586.	53719.	47385.	35800.	1733.	1.000	0.332	0.187	0.025
LAYER TRANSITION 2 TO 3 ON PERF SURFACE OF PROPELLANT 3											
LAYER TRANSITION 2 TO 3 ON END SURFACE OF PROPELLANT 3											
3.239	22.45	1916.	29419.	53420.	47121.	35601.	1730.	1.000	0.335	0.193	0.025
LAYER TRANSITION 3 TO 4 ON PERF SURFACE OF PROPELLANT 3											
LAYER TRANSITION 3 TO 4 ON END SURFACE OF PROPELLANT 3											
3.250	22.72	1927.	29348.	53292.	47009.	35516.	1727.	1.000	0.338	0.204	0.025
3.300	23.89	1974.	29024.	52712.	46497.	35129.	1717.	1.000	0.347	0.250	0.026
3.350	25.08	2020.	28684.	52105.	45961.	34724.	1707.	1.000	0.357	0.296	0.026
3.400	26.31	2066.	28332.	51474.	45405.	34304.	1698.	1.000	0.367	0.341	0.027
3.450	27.56	2112.	27970.	50826.	44833.	33872.	1689.	1.000	0.376	0.385	0.027
3.500	28.84	2156.	27601.	50163.	44249.	33431.	1680.	1.000	0.386	0.429	0.028
3.550	30.15	2200.	27225.	49490.	43654.	32982.	1672.	1.000	0.396	0.472	0.029
3.600	31.48	2244.	26844.	48809.	43054.	32528.	1664.	1.000	0.405	0.514	0.029
3.650	32.84	2287.	26461.	48123.	42448.	32071.	1656.	1.000	0.415	0.555	0.030
3.700	34.23	2329.	26077.	47434.	41841.	31612.	1648.	1.000	0.424	0.596	0.030
3.750	35.64	2371.	25693.	46746.	41234.	31153.	1641.	1.000	0.434	0.636	0.031
3.800	37.07	2412.	25310.	46059.	40628.	30695.	1634.	1.000	0.443	0.675	0.031
3.850	38.53	2452.	24928.	45375.	40025.	30240.	1627.	1.000	0.452	0.713	0.032
3.900	40.02	2492.	24549.	44697.	39426.	29787.	1621.	1.000	0.461	0.751	0.032
3.950	41.52	2531.	24174.	44024.	38833.	29339.	1615.	1.000	0.471	0.788	0.033
4.000	43.05	2570.	23802.	43359.	38246.	28896.	1609.	1.000	0.480	0.824	0.033
4.050	44.61	2608.	23435.	42701.	37666.	28458.	1603.	1.000	0.489	0.860	0.034
4.100	46.18	2646.	23073.	42053.	37094.	28025.	1597.	1.000	0.498	0.895	0.034
4.150	47.78	2682.	22716.	41413.	36530.	27599.	1591.	1.000	0.507	0.929	0.035
4.200	49.40	2719.	22364.	40784.	35975.	27180.	1586.	1.000	0.516	0.962	0.035
4.257	51.29	2760.	21973.	40084.	35357.	26713.	1580.	1.000	0.526	1.000	0.036
PROPELLANT 3 BURNED OUT											
4.300	52.71	2790.	21615.	39443.	34792.	26286.	1576.	1.000	0.533	1.000	0.036
4.350	54.39	2824.	21206.	38709.	34145.	25797.	1571.	1.000	0.542	1.000	0.036
4.400	56.10	2858.	20808.	37996.	33516.	25322.	1566.	1.000	0.550	1.000	0.037
4.450	57.82	2891.	20422.	37303.	32905.	24860.	1561.	1.000	0.559	1.000	0.037
4.500	59.57	2924.	20046.	36629.	32310.	24411.	1556.	1.000	0.567	1.000	0.038
4.550	61.33	2956.	19680.	35975.	31733.	23975.	1551.	1.000	0.575	1.000	0.038
4.600	63.11	2987.	19325.	35338.	31172.	23551.	1547.	1.000	0.583	1.000	0.039
4.650	64.91	3018.	18980.	34720.	30626.	23139.	1543.	1.000	0.592	1.000	0.039
4.700	66.73	3048.	18644.	34119.	30096.	22738.	1538.	1.000	0.600	1.000	0.039
4.750	68.57	3078.	18318.	33535.	29581.	22349.	1534.	1.000	0.607	1.000	0.040
4.800	70.43	3107.	18001.	32968.	29080.	21971.	1530.	1.000	0.615	1.000	0.040

TIME (MS)	TRAV (IN)	VEL (FT/S)	ACC (G)	BREECH PRESS (PSI)	MEAN PRESS (PSI)	BASE PRESS (PSI)	MEAN TEMP (K)	FRAC BURN 1	FRAC BURN 2	FRAC BURN 3	FRAC BURN 4
4.850	72.30	3136.	17693.	32416.	28594.	21603.	1526.	1.000	0.623	1.000	0.040
4.900	74.19	3164.	17393.	31879.	28120.	21246.	1522.	1.000	0.631	1.000	0.041
4.950	76.10	3192.	17101.	31358.	27660.	20898.	1519.	1.000	0.638	1.000	0.041
5.000	78.02	3219.	16818.	30851.	27213.	20560.	1515.	1.000	0.646	1.000	0.042
5.050	79.96	3246.	16542.	30357.	26778.	20231.	1511.	1.000	0.653	1.000	0.042
5.100	81.92	3272.	16274.	29878.	26355.	19912.	1508.	1.000	0.661	1.000	0.042
5.150	83.89	3298.	16012.	29411.	25943.	19601.	1504.	1.000	0.668	1.000	0.043
5.200	85.87	3324.	15758.	28957.	25543.	19298.	1501.	1.000	0.675	1.000	0.043
5.250	87.88	3349.	15511.	28515.	25153.	19003.	1497.	1.000	0.682	1.000	0.043
5.300	89.89	3374.	15270.	28085.	24773.	18717.	1494.	1.000	0.689	1.000	0.043
5.350	91.92	3398.	15036.	27666.	24404.	18437.	1491.	1.000	0.696	1.000	0.044
5.400	93.97	3422.	14807.	27258.	24044.	18166.	1488.	1.000	0.703	1.000	0.044
5.450	96.03	3446.	14585.	26861.	23694.	17901.	1485.	1.000	0.710	1.000	0.044
5.500	98.11	3469.	14368.	26474.	23352.	17643.	1482.	1.000	0.717	1.000	0.045
5.550	100.19	3492.	14157.	26097.	23020.	17392.	1479.	1.000	0.724	1.000	0.045
5.600	102.30	3515.	13951.	25729.	22695.	17147.	1475.	1.000	0.731	1.000	0.045
5.650	104.41	3537.	13750.	25371.	22379.	16908.	1473.	1.000	0.737	1.000	0.046
5.700	106.54	3559.	13554.	25022.	22071.	16675.	1470.	1.000	0.744	1.000	0.046
5.741	108.28	3577.	13399.	24745.	21827.	16491.	1468.	1.000	0.749	1.000	0.046
LAYER TRANSITION 2 TO 3 ON PERF SURFACE OF PROPELLANT 2											
LAYER TRANSITION 2 TO 3 ON END SURFACE OF PROPELLANT 2											
LAYER TRANSITION 2 TO 3 ON LAT SURFACE OF PROPELLANT 2											
5.750	108.68	3581.	13364.	24683.	21773.	16450.	1468.	1.000	0.750	1.000	0.046
5.800	110.84	3602.	13198.	24387.	21512.	16252.	1467.	1.000	0.757	1.000	0.046
5.850	113.00	3623.	13069.	24159.	21310.	16100.	1469.	1.000	0.765	1.000	0.047
5.900	115.18	3644.	12983.	24009.	21178.	16000.	1474.	1.000	0.773	1.000	0.047
5.954	117.37	3667.	12949.	23951.	21127.	15962.	1486.	1.000	0.783	1.000	0.047
LAYER TRANSITION 3 TO 4 ON PERF SURFACE OF PROPELLANT 2											
LAYER TRANSITION 3 TO 4 ON END SURFACE OF PROPELLANT 2											
LAYER TRANSITION 3 TO 4 ON LAT SURFACE OF PROPELLANT 2											
6.000	119.58	3686.	12949.	23954.	21130.	15964.	1498.	1.000	0.792	1.000	0.047
LOCAL PRESSURE MIN DETECTED											
6.050	121.80	3707.	12947.	23956.	21131.	15965.	1511.	1.000	0.802	1.000	0.048
6.061	122.39	3711.	12947.	23956.	21131.	15966.	1514.	1.000	0.804	1.000	0.048
LOCAL PRESSURE MAX DETECTED											
6.100	124.03	3728.	12945.	23955.	21131.	15965.	1524.	1.000	0.812	1.000	0.048
6.150	126.27	3749.	12931.	23935.	21113.	15952.	1536.	1.000	0.821	1.000	0.048
6.200	128.53	3769.	12878.	23843.	21032.	15891.	1545.	1.000	0.830	1.000	0.049
6.250	130.80	3790.	12804.	23714.	20918.	15805.	1553.	1.000	0.838	1.000	0.049
6.300	133.08	3811.	12715.	23559.	20781.	15701.	1559.	1.000	0.845	1.000	0.049
6.350	135.37	3831.	12616.	23383.	20626.	15584.	1564.	1.000	0.852	1.000	0.049
6.400	137.67	3851.	12507.	23192.	20457.	15457.	1569.	1.000	0.858	1.000	0.050
6.450	139.99	3871.	12391.	22987.	20276.	15320.	1573.	1.000	0.864	1.000	0.050
6.500	142.32	3891.	12269.	22771.	20086.	15176.	1576.	1.000	0.870	1.000	0.050
6.550	144.66	3911.	12142.	22546.	19887.	15026.	1579.	1.000	0.875	1.000	0.050
6.600	147.01	3930.	12011.	22313.	19682.	14871.	1581.	1.000	0.881	1.000	0.051
6.650	149.38	3949.	11877.	22074.	19471.	14712.	1583.	1.000	0.886	1.000	0.051
6.700	151.75	3968.	11739.	21831.	19256.	14550.	1584.	1.000	0.890	1.000	0.051
6.750	154.14	3987.	11600.	21583.	19038.	14385.	1585.	1.000	0.895	1.000	0.051
6.800	156.54	4006.	11459.	21332.	18817.	14218.	1585.	1.000	0.899	1.000	0.052
6.850	158.95	4024.	11316.	21079.	18593.	14049.	1585.	1.000	0.903	1.000	0.052
6.900	161.37	4042.	11173.	20824.	18368.	13879.	1585.	1.000	0.907	1.000	0.052
6.950	163.80	4060.	11028.	20567.	18142.	13708.	1585.	1.000	0.911	1.000	0.052
7.000	166.24	4078.	10884.	20310.	17915.	13537.	1584.	1.000	0.914	1.000	0.053
7.050	168.69	4095.	10739.	20053.	17689.	13366.	1583.	1.000	0.918	1.000	0.053

TIME (MS)	TRAV (IN)	VEL (FT/E)	ACC (G)	BRECH PRESS (PSI)	NEAR PRESS (PSI)	BASE PRESS (PSI)	NEAR TEMP (K)	FRAC BURN 1	FRAC BURN 2	FRAC BURN 3	FRAC BURN 4
7.100	171.15	4112.	10595.	19797.	17462.	13195.	1582.	1.000	0.921	1.000	0.053
7.150	173.63	4129.	10431.	19541.	17236.	13024.	1580.	1.000	0.924	1.000	0.053
7.200	176.11	4146.	10307.	19285.	17011.	12854.	1579.	1.000	0.927	1.000	0.054
7.250	178.60	4162.	10165.	19031.	16787.	12685.	1577.	1.000	0.930	1.000	0.054
7.300	181.10	4179.	10023.	18779.	16564.	12516.	1575.	1.000	0.932	1.000	0.054
7.350	183.62	4195.	9862.	18528.	16343.	12349.	1573.	1.000	0.935	1.000	0.054
7.400	186.14	4211.	9742.	18279.	16124.	12183.	1570.	1.000	0.937	1.000	0.054
7.419	187.11	4217.	9689.	18185.	16040.	12120.	1569.	1.000	0.938	1.000	0.054
PROJECTILE EXIT											

CONDITIONS AT:	P MAX	MUZZLE
TIME (MS):	2.527	7.419
TRAVEL (IN):	9.20	187.11
VELOCITY (FT/S):	1167.	4217.
ACCELERATION (G):	34756.	9689.
BREECH PRESS (PSI):	62991.	18185.
MEAN PRESS (PSI):	55564.	16040.
BASE PRESS (PSI):	41979.	12120.
MEAN TEMP (K):	1900.	1569.
Z CHARGE 1 (-):	1.000	1.000
Z CHARGE 2 (-):	0.194	0.938
Z CHARGE 3 (-):	0.124	1.000
Z CHARGE 4 (-):	0.015	0.054

ENERGY BALANCE SUMMARY	IN-LB	%
TOTAL CHEMICAL:	293665792.	100.00
(1) INTERNAL GAS:	191603776.	65.25
(2) WORK AND LOSSES:	102062016.	34.75
(A) PROJECTILE KINETIC:	69901328.	23.80
(B) GAS KINETIC:	22608000.	7.70
(C) PROJECTILE ROTATIONAL:	35195.	0.01
(D) FRICTIONAL WORK TO TUBE:	0.	0.00
(E) OTHER FRICTIONAL WORK:	391065.	0.13
(F) WORK DONE AGAINST AIR:	725224.	0.25
(G) HEAT CONVECTED TO BORE:	8401203.	2.86
(H) RECOIL ENERGY:	0.	0.00
LOADING DENSITY (G/CM3):	1.175	
CHARGE WT/PROJECTILE WT:	1.056	
PIEZOMETRIC EFFICIENCY:	0.338	
EXPANSION RATIO:	7.247	

Test Case 6

Test case 6 is a two-part run with a \$PMAX calculation in the first portion. The inputs are saved and re-used for a \$PARA study on charge weight (second propellant deck) as a further set of calculations.

The \$PMAX deck attempts to vary the web distance of the second propellant to reach a maximum breech pressure of 75 kpsi. Initial tries for the iterative solution are WEB=0.070 and WEB=0.075; these values establish a direction of search (WEB to increase or decrease). During execution, no output (other than input deck echoes) is printed until a solution has been found.

Ignition variations are in effect on propellant 2. The perforation surfaces are considered ignited at the start of calculation, end surfaces ignite at 0.2 milliseconds, and lateral surface when mean pressure reaches 2000 psi.

After the first solution has been found, IBHVG2 saves inputs to use for the second series of runs; namely, a \$PARA study on charge weight for the second propellant. Values to be printed in the table at the end of the trajectory output have been specified in the first deck, and the \$PMAX is still in effect to search for 75 kpsi maximum breech pressure by varying web distance.

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SCOMM      IBHVG2 BENCHMARK TEST CASE 6
           SHOW IGNITION CODE VARIATIONS - PMAX .VS. PARA,PMAX

SHEAT      TSHL = 0.00450      CSHL = 1048      RSHL = 0.284
           TWAL = 293          HO  = 0.0648      HL   = 1

SGUN       NAME = '120MM GUN TEST CASE'  CHAM = 607      GRVE = 4.724
           LAND = 4.724      G/L = 1.      TRAV = 187.11
           TWST = 99

SPROJ      NAME = 'APFSOR'  PMVT = 15.65

SCOMM      'PDIS' VALUES USED WITH PARAMETRIC PRINT OPTION POPT(5)=2
SPDIS      SHOW='PMAX' DECK='OUT'
SPDIS      SHOW='CHWT' DECK='PROP' NTH=2
SPDIS      SHOW='DIAM' DECK='PROP' NTH=2
SPDIS      SHOW='PD' DECK='PROP' NTH=2
SPDIS      SHOW='WEB' DECK='PROP' NTH=2
SPDIS      SHOW='VMUZ' DECK='OUT'
SPDIS      SHOW='ZMUZ(2)' DECK='OUT'
SPDIS      SHOW='LDEN' DECK='OUT'

SRESI      NPTS = 4          AIR = 1
           TRAY = 0, 0.8, 3.0, 187
           PRES = 100, 2500, 100, 100

SINFO      RUN = '120MM IGNITION DELAY EXPERIMENT'  DELT = 5E-5  Delp = 5E-5
           GRAD = 2          POPT = 1,1,1,0,2  SOPT = 0
```

```

EPS = 0.05

$RECO
NAME = 'NONE'      RECO = 0      RCWT = 0

$SPRIN
NAME = 'BENITE'    CHWT = 0.00347
                  GAMA = 1.25    FORC = 212500
COV = 30          TEMP = 2000

$SPROP
NAME = 'JA2 7P'    CHWT = 10.00   GRAN = '7PF'
RHO = 0.05732      GAMA = 1.2257   FORC = 382152
COV = 27.48        TEMP = 3400     EROS = 0.0000000
NTBL=4 PR4L= 2000,4000,10000,25000 BR4L= 1.05,1.52,2.93,6.56
LEN = 0.643        DIAM = 0.420    PD = 0.020
WI = 0.076         WO = 0.074

$SCOMM
PROPELLANT IGNITION CODES:
PERF  IGNITES AT START OF CALCULATION
END   IGNITES AT TIME=.2 MILLISECOND
LATERAL IGNITES WHEN MEAN PRESSURE REACHES 2KPSI

$SPROP
NAME = 'JA2 7P'    CHWT = 7.5     GRAN = '7PF'
RHO = 0.05732      GAMA = 1.2257   FORC = 382152
COV = 27.48        TEMP = 3400     EROS = 0.0000000
NTBL=4 PR4L= 2000,4000,10000,25000 BR4L= 1.05,1.52,2.93,6.56
LEN = 0.643        DIAM = 0.420    PD = 0.020
WEB = 0.075
IGNS=0,1,3 THRS=0.,.0002,2000.

$SCOMM
PROGRAM ITERATES WEB OF SECOND PROPELLANT UNTIL PMAX=75000 REACHED
INITIAL GUESSES OF WEB ARE .070 AND .075 INCHES

$SPMAX
VARY='WEB' NTH=2 PMAX=75000 TRY1=.070 TRY2=.075

$SEND

$SAVE

$SCOMM
VARY CHARGE WEIGHT OF SECOND PROPELLANT FROM 6 TO 8 POUNDS
BY INCREMENTS OF .5 POUNDS
ALL OTHER OPTIONS STILL IN FORCE AS IN PREVIOUS DECK

$SPARA
VARY='CW' NTH=2 FROM=6 TO=8 BY=.5 DECK='PROP'

$SEND

```

Producing the following output:

ERRTOL= 4.768372E-07

```
CARD 1 --> SCONH
CARD 2 --> IBHVQ2 BENCHMARK TEST CASE 6
CARD 3 -->
CARD 4 --> SHOW IGNITION CODE VARIATIONS - PMAX .VS. PARA,PMAX
CARD 5 -->
CARD 6 --> SHEAT
CARD 7 --> TSHL = 0.00450      CSHL = 1848      RSHL = 0.284
CARD 8 --> THAL = 293      NO = 0.0648      NL = 1
CARD 9 --> SGUN
CARD 10 --> NAME = '120MM GUN TEST CASE'  CHAM = 607      GRVE = 4.724
CARD 11 --> LAND = 4.724      G/L = 1.      TRAV = 187.11
CARD 12 --> TWST = 99
CARD 13 --> SPROJ
CARD 14 --> NAME = 'APFSDS'  PRWT = 15.65
CARD 15 --> SCONH
CARD 16 --> 'POIS' VALUES USED WITH PARAMETRIC PRINT OPTION POPT(5)=2
CARD 17 --> SPDIS
CARD 18 --> SHOW='PMAX' DECK='OUT'
CARD 19 --> SPDIS
CARD 20 --> SHOW='CHWT' DECK='PROP' NTH=2
CARD 21 --> SPDIS
CARD 22 --> SHOW='DIAM' DECK='PROP' NTH=2
CARD 23 --> SPDIS
CARD 24 --> SHOW='PD' DECK='PROP' NTH=2
CARD 25 --> SPDIS
CARD 26 --> SHOW='WEB' DECK='PROP' NTH=2
CARD 27 --> SPDIS
CARD 28 --> SHOW='MUZ' DECK='OUT'
CARD 29 --> SPDIS
CARD 30 --> SHOW='ZMUZ(2)' DECK='OUT'
CARD 31 --> SPDIS
CARD 32 --> SHOW='LDEN' DECK='OUT'
CARD 33 -->
CARD 34 --> SRESI
CARD 35 --> NPTS = 4      AIR = 1
CARD 36 --> TRAV = 0, 0.8, 3.0, 187
CARD 37 --> PRES = 100, 2500, 100, 100
CARD 38 -->
CARD 39 --> SINFO
CARD 40 --> RUN = '120MM IGNITION DELAY EXPERIMENT'  DELT = 5E-5  DELP = 5E-5
CARD 41 --> GRAD = 2      POPT = 1,1,1,0,2  SOPT = 0
CARD 42 --> EPS = 0.05
CARD 43 -->
CARD 44 --> SRECO
CARD 45 --> NAME = 'NONE'      RECO = 0      RCWT = 0
CARD 46 -->
CARD 47 --> SPRIM
CARD 48 --> NAME = 'BENITE'  CHWT = 0.00347
CARD 49 --> GAMA = 1.25      FORC = 212500
CARD 50 --> COV = 30      TEMP = 2000
CARD 51 --> SPROP
CARD 52 --> NAME = 'JA2 7P'  CHWT = 10.00      GRAN = '7PF'
CARD 53 --> RHO = 0.05732      GAMA = 1.2257      FORC = 382152
CARD 54 --> COV = 27.48      TEMP = 3400      EROS = 0.0000000
CARD 55 --> NYBL=4 PR4L= 2000,4000,10000,25000 BR4L= 1.05,1.52,2.93,6.56
```

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CARD 56 -->      LEN = 0.643      DIAM = 0.420      PD = 0.020
CARD 57 -->      WI = 0.076      WO = 0.074
CARD 58 -->
CARD 59 --> $CONH
CARD 60 -->      PROPELLANT IGNITION CODES:
CARD 61 -->      PERF  IGNITES AT START OF CALCULATION
CARD 62 -->      ENO   IGNITES AT TIME=.2 MILLISECOND
CARD 63 -->      LATERAL IGNITES WHEN MEAN PRESSURE REACHES 2KPSI
CARD 64 -->
CARD 65 --> $PROP
CARD 66 -->      NAME = 'JA2 7P'      CHWT = 7.5      GRAN = '7PF'
CARD 67 -->      RHO = 0.05732      GAMA = 1.2257      FORC = 382152
CARD 68 -->      COV = 27.48      TEMP = 3400      EROS = 0.0000000
CARD 69 -->      NTBL=4 PR4L= 2000,4000,10000,25000 BR4L= 1.05,1.52,2.93,6.56
CARD 70 -->      LEN = 0.643      DIAM = 0.420      PD = 0.020
CARD 71 -->      WEB = 0.075
CARD 72 -->      IGNS=0,1,3 THRS=0.,.0002,2000.
CARD 73 -->
CARD 74 --> $CONH
CARD 75 -->      PROGRAM ITERATES WEB OF SECOND PROPELLANT UNTIL PHAX=75000 REACHED
CARD 76 -->      INITIAL GUESSES OF WEB ARE .070 AND .075 INCHES
CARD 77 --> $PMAX
CARD 78 -->      VARY='WEB' NTH=2 PHAX=75000 TRY1=0.070 TRY2=0.075
CARD 79 --> $END

```

 - GUN TUBE -

 TYPE: 120MM GUN TEST CASE
 GROOVE/LAND RATIO: 187.11
 LAND DIAMETER (IN): 4.724
 BORE AREA (IN²): 17.5271
 SHELL CP (IN-LB/LB-K): 1848.0
 INIT. SHELL TEMP (K): 293.0
 AIR NO (IN-LB/IN²-S-K): 0.06480
 CHAMBER VOLUME (IN³): 607.00
 TOTAL WEIGHT (LB): 15.650
 WEIGHT PREDICTOR OPTION: 0
 TYPE: APFSDS
 TYPE: RESISTANCE -

 AIR RESISTANCE OPTION: 1
 1 TRAVEL (IN) PRESSURE (PSI) 100. 2500.
 2 0.00 0.80

 - GENERAL -

 MAX TIME STEP (S): 0.000050
 PRINT OPTIONS: 1 1 1 0 2 1
 GRAUENT MODEL: PIDOUCK-KENT
 MAX RELATIVE ERROR (-): 0.05000
 CONSTANT-PRESSURE OPTION: 0

 - RECOIL -

 RECOIL OPTION: 0
 TYPE: NONE
 RECOILING WEIGHT (LB): 0.

 - INNER -

 TYPE: BENITE
 COVOLUME (IN³/LB): 30.000
 GAMMA (-): 1.2500
 FLAME TEMP (K): 2000.0
 FORCE (FT-LB/LB): 212500.
 WEIGHT (LB): 0.003470

- CHARGE 1 -

TYPE: JA2 7p	GRAINS:	2724.4	7PF	WEIGHT (LB):	
EROSIVE COEFF (-):	CHARGE IGM CODE:		0	CHARGE IGM AT (S):	10.0000
GRAIN LENGTH (IN):	GRAIN DIAMETER (IN):		0.36000	PERF DIAMETER (IN):	0.00000E+00
INNER WEB (IN):	OUTER WEB (IN):		0.07400		0.02000

	PROPERTIES AT LAYER BOUNDARIES OF PERF SURFACES	PROPERTIES AT LAYER BOUNDARIES OF END SURFACES
	2ND 3RD 4TH	1ST 2ND 3RD 4TH
AT DEPTH (IN):	0.00000	0.00000
ADJACENT LAYER WT %:	100.000	100.000
DENSITY (LB/IN3):	0.05732	0.05732
GAMMA (-):	1.2257	1.2257
FORCE (FT-LB/LB):	382152.	382152.
COVOLUME (IN3/LB):	27.480	27.480
FLAME TEMP (K):	3400.0	3400.0
MEAN PRESSURES (PSI):	2000.0	2000.0
MEAN PRESSURES (PSI):	4000.0	4000.0
MEAN PRESSURES (PSI):	10000.0	10000.0
MEAN PRESSURES (PSI):	25000.0	25000.0
BURNING RATES (IN/S):	1.05	1.05
BURNING RATES (IN/S):	1.52	1.52
BURNING RATES (IN/S):	2.93	2.93
BURNING RATES (IN/S):	6.56	6.56

PROPERTIES AT LAYER BOUNDARIES OF LAT SURFACES

	2ND 3RD 4TH
AT DEPTH (IN):	0.00000
ADJACENT LAYER WT %:	100.000
DENSITY (LB/IN3):	0.05732
GAMMA (-):	1.2257
FORCE (FT-LB/LB):	382152.
COVOLUME (IN3/LB):	27.480
FLAME TEMP (K):	3400.0
MEAN PRESSURES (PSI):	2000.0
MEAN PRESSURES (PSI):	4000.0
MEAN PRESSURES (PSI):	10000.0
MEAN PRESSURES (PSI):	25000.0
BURNING RATES (IN/S):	1.05
BURNING RATES (IN/S):	1.52
BURNING RATES (IN/S):	2.93
BURNING RATES (IN/S):	6.56

TYPE: JAZ 7		GRAINS:		3203.5		7PF		WEIGHT (LB):	
EROSIVE COEFF (-):	0.000000	CHARGE IGM CODE:	0			L-SURFACE IGM AT (S):			7.5060
P-SURFACE IGM CODE:	0	E-SURF IGM CODE:	1			L-SURFACE IGM CODE:			0.00000E+00
P-SURF IGM AT (S):	0.00000E+00	E-SURF IGM AT (S):	0.20000E-03			L-SURF IGM AT (PSI):			3
GRAIN LENGTH (IN):	0.64300	GRAIN DIAMETER (IN):	0.28585			PERF DIAMETER (IN):			0.27000E+04
INNER WEB (IN):	0.05646	OUTER WEB (IN):	0.05646						0.02000

	PROPERTIES AT LAYER BOUNDARIES OF PERF SURFACES			PROPERTIES AT LAYER BOUNDARIES OF END SURFACES		
	1ST	2ND	4TH	1ST	2ND	4TH
AT DEPTH (IN):	-----	-----	0.00000	-----	-----	0.00000
ADJACENT LAYER WT %:	-----	-----	160.000	-----	-----	100.000
DENSITY (LB/IN3):	-----	-----	0.05732	-----	-----	0.05732
GAMMA (-):	-----	-----	1.2257	-----	-----	1.2257
FORCE (FT-LB/LB):	-----	-----	382152.	-----	-----	382152.
COVOLUME (IN3/LB):	-----	-----	27.480	-----	-----	27.480
FLAME TEMP (K):	-----	-----	3400.0	-----	-----	3400.0
MEAN PRESSURES (PSI):	-----	-----	2000.0	-----	-----	2000.0
MEAN PRESSURES (PSI):	-----	-----	4000.0	-----	-----	4000.0
MEAN PRESSURES (PSI):	-----	-----	10000.0	-----	-----	10000.0
MEAN PRESSURES (PSI):	-----	-----	25000.0	-----	-----	25000.0
BURNING RATES (IN/S):	-----	-----	1.05	-----	-----	1.05
BURNING RATES (IN/S):	-----	-----	1.52	-----	-----	1.52
BURNING RATES (IN/S):	-----	-----	2.93	-----	-----	2.93
BURNING RATES (IN/S):	-----	-----	6.56	-----	-----	6.56

PROPERTIES AT LAYER BOUNDARIES OF		LAT	SURFACES
18T	2ND	3RD	4TH
AT DEPTH (IN):	-----	-----	0.00000
ADJACENT LAYER WT %:	-----	-----	100.000
DENSITY (LB/IN ³):	-----	-----	0.05732
GAMMA (-):	-----	-----	1.2257
FORCE (FT-LB/LB):	-----	-----	382152.
COVOLUME (IN ³ /LB):	-----	-----	27.480
FLAME TEMP (F):	-----	-----	3400.0
MEAN PRESSURES (PSI):	-----	-----	2000.0
MEAN PRESSURES (PSI):	-----	-----	4000.0
MEAN PRESSURES (PSI):	-----	-----	10000.0
MEAN PRESSURES (PSI):	-----	-----	25000.0
BURNING RATES (IN/S):	-----	-----	1.05
BURNING RATES (IN/S):	-----	-----	1.52
BURNING RATES (IN/S):	-----	-----	2.93
BURNING RATES (IN/S):	-----	-----	6.56

TIME (MS)	TRAV (IN)	VEL (FT/S)	ACC (G)	BREECH PRESS (PSI)	MEAN PRESS (PSI)	BASE PRESS (PSI)	MEAN TEMP (K)	FRAC BURN 1	FRAC BURN 2
0.000	0.00	0.	0.	29.	29.	29.	2000.	0.000	0.000
0.050	0.00	0.	0.	54.	54.	54.	2490.	0.000	0.000
0.100	0.00	0.	0.	87.	87.	87.	2779.	0.000	0.000
0.120	0.00	0.	0.	102.	102.	102.	2859.	0.000	0.000
SHOT-START PRESSURE ACHIEVED									
0.150	0.00	0.	-6.	145.	127.	95.	2954.	0.000	0.000
0.202	0.00	0.	37.	203.	178.	133.	3072.	0.001	0.000
PROPELLANT 2 IGNITED ON END SURFACE									
0.250	0.00	0.	88.	273.	240.	179.	3151.	0.001	0.000
0.300	0.00	0.	149.	357.	313.	234.	3207.	0.001	0.001
0.350	0.00	1.	219.	454.	398.	297.	3247.	0.002	0.001
0.400	0.00	1.	297.	562.	493.	368.	3275.	0.002	0.001
0.450	0.00	2.	384.	684.	600.	448.	3297.	0.003	0.001
0.500	0.00	2.	478.	818.	718.	535.	3313.	0.003	0.002
0.550	0.00	3.	581.	966.	847.	632.	3326.	0.004	0.002
0.600	0.01	4.	691.	1126.	988.	737.	3337.	0.005	0.002
0.650	0.01	5.	809.	1300.	1141.	851.	3345.	0.005	0.003
0.700	0.01	7.	935.	1488.	1305.	974.	3351.	0.006	0.003
0.750	0.02	8.	1067.	1690.	1482.	1106.	3357.	0.007	0.004
0.800	0.02	10.	1207.	1905.	1671.	1247.	3362.	0.008	0.004
0.850	0.03	12.	1352.	2135.	1873.	1397.	3365.	0.009	0.005
0.880	0.03	14.	1442.	2278.	1998.	1491.	3367.	0.009	0.005
PROPELLANT 2 IGNITED ON LAT SURFACE									
0.900	0.04	15.	1534.	2420.	2123.	1584.	3369.	0.010	0.005
0.950	0.05	17.	1773.	2790.	2447.	1826.	3373.	0.011	0.007
1.000	0.06	20.	2028.	3188.	2797.	2087.	3375.	0.012	0.008
1.050	0.07	24.	2297.	3615.	3172.	2366.	3378.	0.013	0.010
1.100	0.09	28.	2579.	4071.	3572.	2665.	3379.	0.014	0.012
1.150	0.11	32.	2874.	4556.	3997.	2982.	3381.	0.016	0.014
1.200	0.13	37.	3185.	5075.	4452.	3322.	3382.	0.017	0.016
1.250	0.15	42.	3516.	5635.	4944.	3689.	3382.	0.019	0.018
1.300	0.18	48.	3866.	6238.	5472.	4083.	3382.	0.021	0.020
1.350	0.21	55.	4236.	6884.	6039.	4506.	3383.	0.023	0.023
1.400	0.24	62.	4626.	7576.	6646.	4959.	3382.	0.025	0.025
1.450	0.28	70.	5035.	8316.	7295.	5443.	3382.	0.027	0.028
1.500	0.33	78.	5463.	9103.	7986.	5958.	3381.	0.029	0.031
1.550	0.38	87.	5910.	9941.	8720.	6507.	3380.	0.032	0.034
1.600	0.43	97.	6375.	10829.	9499.	7088.	3379.	0.034	0.038
1.650	0.49	108.	6858.	11769.	10324.	7703.	3378.	0.037	0.042
1.700	0.56	119.	7366.	12775.	11206.	8361.	3376.	0.040	0.046
1.750	0.64	132.	7901.	13850.	12149.	9065.	3374.	0.043	0.050
1.800	0.72	145.	8464.	14998.	13157.	9817.	3372.	0.047	0.055
1.850	0.81	159.	9101.	16223.	14231.	10618.	3370.	0.051	0.060
1.900	0.91	174.	10178.	17526.	15375.	11472.	3367.	0.055	0.065
1.950	1.02	192.	11326.	18911.	16589.	12378.	3364.	0.059	0.071
2.000	1.14	211.	12549.	20378.	17876.	13338.	3361.	0.064	0.077
2.050	1.27	232.	13848.	21929.	19237.	14353.	3358.	0.069	0.084
2.100	1.42	255.	15224.	23565.	20671.	15424.	3354.	0.074	0.091
2.150	1.58	281.	16680.	25283.	22179.	16549.	3349.	0.080	0.098
2.200	1.76	309.	18215.	27084.	23758.	17727.	3344.	0.086	0.107
2.250	1.95	340.	19830.	28963.	25407.	18957.	3339.	0.092	0.115
2.300	2.17	373.	21523.	30919.	27123.	20237.	3333.	0.099	0.125
2.350	2.40	409.	23294.	32944.	28900.	21563.	3326.	0.107	0.134
2.400	2.66	448.	25138.	35033.	30732.	22930.	3319.	0.115	0.145
2.450	2.94	490.	27053.	37178.	32614.	24334.	3312.	0.123	0.156

TIME (MS)	TRAV (IN)	VEL (FT/S)	ACC (G)	ORGECH PRESS (PSI)	MEAN PRESS (PSI)	BASE PRESS (PSI)	MEAN TEMP (K)	FRAC BURN 1	FRAC BURN 2
2.500	3.25	535.	28732.	39369.	34535.	25768.	3304.	0.132	0.168
2.550	3.58	583.	30363.	41595.	36488.	27225.	3295.	0.141	0.180
2.600	3.95	633.	32011.	43846.	38463.	28699.	3285.	0.151	0.193
2.650	4.34	686.	33668.	46110.	40449.	30180.	3276.	0.161	0.207
2.700	4.77	741.	35324.	48372.	42433.	31661.	3265.	0.172	0.222
2.750	5.23	800.	36969.	50619.	44404.	33132.	3254.	0.183	0.237
2.800	5.73	860.	38592.	52837.	46350.	34583.	3243.	0.195	0.253
2.850	6.26	924.	40182.	55010.	48256.	36006.	3231.	0.207	0.270
2.900	6.84	990.	41729.	57125.	50111.	37390.	3218.	0.220	0.288
2.950	7.45	1058.	43222.	59166.	51902.	38726.	3205.	0.233	0.306
3.000	8.11	1129.	44651.	61121.	53617.	40005.	3192.	0.247	0.325
3.050	8.81	1202.	46007.	62976.	55244.	41220.	3178.	0.262	0.344
3.100	9.55	1277.	47281.	64720.	56774.	42361.	3165.	0.277	0.365
3.150	10.34	1354.	48466.	66343.	58198.	43423.	3150.	0.292	0.386
3.200	11.18	1433.	49556.	67836.	59508.	44401.	3136.	0.308	0.407
3.250	12.06	1514.	50545.	69193.	60698.	45289.	3121.	0.324	0.429
3.300	12.99	1596.	51430.	70409.	61764.	46084.	3107.	0.340	0.452
3.350	13.97	1679.	52209.	71479.	62703.	46785.	3092.	0.357	0.476
3.400	15.01	1764.	52880.	72404.	63514.	47390.	3077.	0.374	0.499
3.450	16.09	1849.	53444.	73182.	64197.	47900.	3062.	0.392	0.524
3.500	17.23	1936.	53901.	73816.	64753.	48315.	3048.	0.410	0.548
3.550	18.41	2023.	54255.	74309.	65186.	48638.	3033.	0.428	0.573
3.600	19.65	2110.	54509.	74666.	65499.	48871.	3018.	0.446	0.599
3.650	20.95	2198.	54666.	74891.	65697.	49019.	3004.	0.464	0.624
3.700	22.29	2286.	54731.	74992.	65785.	49085.	2989.	0.483	0.650
3.718	22.78	2310.	54734.	75000.	65792.	49090.	2984.	0.489	0.659
LOCAL PRESSURE MAX DETECTED									
3.718	22.78	2318.	54734.	75000.	65792.	49090.	2984.	0.489	0.659
LOCAL PRESSURE MIN DETECTED									
3.718	22.78	2318.	54734.	75000.	65792.	49090.	2984.	0.489	0.659
LOCAL PRESSURE MAX DETECTED									
3.750	23.69	2375.	54711.	74976.	65771.	49074.	2975.	0.501	0.676
3.800	25.14	2463.	54609.	74850.	65660.	48991.	2961.	0.520	0.703
3.850	26.65	2550.	54432.	74622.	65460.	48842.	2947.	0.539	0.729
3.900	28.20	2638.	54186.	74300.	65177.	48631.	2934.	0.558	0.756
3.950	29.81	2725.	53777.	73892.	64820.	48364.	2920.	0.577	0.782
4.000	31.47	2811.	53111.	73406.	64394.	48047.	2907.	0.596	0.809
4.050	33.18	2897.	53093.	72851.	63907.	47683.	2894.	0.615	0.836
4.100	34.95	2982.	52620.	72220.	63353.	47270.	2881.	0.634	0.862
4.150	36.76	3066.	51925.	71287.	62535.	46660.	2868.	0.652	0.884
4.200	38.63	3149.	51047.	70104.	61497.	45885.	2853.	0.671	0.902
4.250	40.54	3231.	50062.	68770.	60332.	45016.	2838.	0.690	0.917
4.300	42.50	3310.	49000.	67350.	59081.	44082.	2822.	0.708	0.930
4.350	44.51	3388.	47900.	65858.	57772.	43106.	2807.	0.726	0.941
4.400	46.57	3465.	46765.	64324.	56426.	42102.	2791.	0.744	0.950
4.450	48.67	3539.	45611.	62766.	55060.	41082.	2776.	0.761	0.958
4.500	50.82	3611.	44451.	61199.	53685.	40056.	2760.	0.778	0.965
4.550	53.00	3682.	43295.	59636.	52314.	39033.	2745.	0.795	0.970
4.600	55.23	3751.	42155.	58097.	50964.	38026.	2730.	0.811	0.975
4.650	57.51	3818.	41038.	56587.	49639.	37038.	2715.	0.827	0.980
4.700	59.82	3883.	39944.	55109.	48343.	36071.	2701.	0.843	0.983
4.750	62.16	3947.	38876.	53667.	47078.	35127.	2686.	0.859	0.987
4.800	64.55	4008.	37808.	52224.	45812.	34182.	2672.	0.873	0.990
4.850	66.97	4068.	36739.	50780.	44545.	33237.	2657.	0.886	0.992
4.900	69.43	4127.	35653.	49313.	43258.	32276.	2642.	0.897	0.994

TIME (MS)	TRAV (IN)	VEL (FT/S)	ACC (G)	BREECH PRESS (PSI)	MEAN PRESS (PSI)	BASE PRESS (PSI)	MEAN TEMP (K)	FRAC BURN 1	FRAC BURN 2
4.950	71.93	4183.	34568.	47846.	41972.	31317.	2627.	0.907	0.996
5.000	74.45	4238.	33499.	46401.	40705.	30371.	2611.	0.916	0.997
5.050	77.01	4291.	32452.	44987.	39464.	29445.	2596.	0.923	0.998
5.100	79.60	4342.	31432.	43608.	38254.	28543.	2581.	0.930	0.999
5.150	82.22	4392.	30440.	42268.	37079.	27666.	2565.	0.936	0.999
5.200	84.87	4440.	29479.	40969.	35939.	26816.	2550.	0.942	1.000
5.250	87.55	4487.	28549.	39713.	34837.	25901.	2535.	0.947	1.000
5.251	87.61	4488.	28528.	39684.	34812.	25901.	2535.	0.947	1.000
PROPELLANT 2 BURNED OUT									
5.300	90.25	4532.	27652.	38501.	33774.	25200.	2520.	0.952	1.000
5.350	92.99	4576.	26789.	37335.	32751.	24437.	2505.	0.956	1.000
5.400	95.75	4619.	25956.	36214.	31768.	23703.	2491.	0.960	1.000
5.450	98.53	4660.	25161.	35137.	30823.	22978.	2476.	0.963	1.000
5.500	101.34	4700.	24394.	34102.	29915.	22321.	2462.	0.966	1.000
5.550	104.17	4738.	23657.	33107.	29042.	21670.	2448.	0.969	1.000
5.600	107.02	4776.	22949.	32152.	28204.	21044.	2434.	0.972	1.000
5.650	109.90	4812.	22269.	31234.	27399.	20444.	2421.	0.974	1.000
5.700	112.80	4848.	21615.	30352.	26626.	19867.	2407.	0.976	1.000
5.750	115.72	4882.	20988.	29506.	25884.	19313.	2394.	0.978	1.000
5.800	118.65	4915.	20386.	28695.	25172.	18781.	2381.	0.980	1.000
5.850	121.61	4947.	19808.	27916.	24488.	18272.	2369.	0.982	1.000
5.900	124.59	4979.	19253.	27168.	23832.	17782.	2356.	0.983	1.000
5.950	127.59	5009.	18720.	26450.	23202.	17312.	2344.	0.985	1.000
6.000	130.60	5039.	18208.	25760.	22597.	16861.	2332.	0.986	1.000
6.050	133.64	5068.	17716.	25097.	22015.	16427.	2320.	0.987	1.000
6.100	136.68	5096.	17242.	24459.	21456.	16009.	2309.	0.988	1.000
6.150	139.75	5124.	16787.	23846.	20918.	15608.	2297.	0.989	1.000
6.200	142.83	5150.	16348.	23256.	20400.	15222.	2286.	0.990	1.000
6.250	145.93	5176.	15926.	22688.	19902.	14850.	2275.	0.991	1.000
6.300	149.04	5202.	15519.	22141.	19422.	14492.	2264.	0.992	1.000
6.350	152.17	5226.	15128.	21613.	18960.	14147.	2253.	0.993	1.000
6.400	155.32	5250.	14750.	21105.	18514.	13814.	2243.	0.994	1.000
6.450	158.47	5274.	14385.	20616.	18085.	13494.	2232.	0.994	1.000
6.500	161.64	5297.	14034.	20143.	17670.	13184.	2222.	0.995	1.000
6.550	164.83	5319.	13695.	19687.	17270.	12866.	2212.	0.996	1.000
6.600	168.03	5341.	13367.	19247.	16884.	12598.	2202.	0.996	1.000
6.650	171.24	5362.	13051.	18822.	16512.	12320.	2192.	0.997	1.000
6.700	174.46	5383.	12745.	18412.	16151.	12051.	2182.	0.997	1.000
6.750	177.70	5403.	12450.	18015.	15803.	11792.	2173.	0.997	1.000
6.800	180.94	5423.	12164.	17632.	15467.	11541.	2164.	0.998	1.000
6.850	184.20	5442.	11888.	17261.	15142.	11298.	2154.	0.998	1.000
6.894	187.11	5459.	11650.	16942.	14862.	11089.	2146.	0.998	1.000
PROJECTILE EXIT									

CONDITIONS AT:	PMAX	MUZZLE
TIME (MS):	3.718	6.894
TRAVEL (IN):	22.78	187.11
VELOCITY (FT/S):	2318.	5459.
ACCELERATION (G):	54734.	11650.
BREECH PRESS (PSI):	75000.	16942.
MEAN PRESS (PSI):	65792.	14862.
BASE PRESS (PSI):	49090.	11089.
MEAN TEMP (K):	2984.	2146.
Z CHARGE 1 (-):	0.489	0.998
Z CHARGE 2 (-):	0.659	1.000

ENERGY BALANCE SUMMARY	IN-LB	%
TOTAL CHEMICAL:	355233280.	100.00
(1) INTERNAL GAS:	224251200.	63.13
(2) WORK AND LOSSES:	130982080.	36.87
(A) PROJECTILE KINETIC:	86906272.	24.46
(B) GAS KINETIC:	29568784.	8.32
(C) PROJECTILE ROTATIONAL:	43757.	0.01
(D) FRICTIONAL WORK TO TUBE:	0.	0.00
(E) OTHER FRICTIONAL WORK:	391060.	0.11
(F) WORK DONE AGAINST AIR:	1221806.	0.34
(G) HEAT CONVECTED TO BORE:	12850402.	3.62
(H) RECOIL ENERGY:	0.	0.00

LOADING DENSITY (G/CM3):	0.798
CHARGE WT/PROJECTILE WT:	1.118
PNEUMATIC EFFICIENCY:	0.353
EXPANSION RATIO:	6.403

CARD 80 -->
 CARD 81 --> \$SAVE
 CARD 82 -->
 CARD 83 --> \$COMM
 CARD 84 --> VARY CHARGE WEIGHT OF SECOND PROPELLANT FROM 6 TO 8 POUNDS
 CARD 85 --> BY INCREMENTS OF .5 POUNDS
 CARD 86 --> ALL OTHER OPTIONS STILL IN FORCE AS IN PREVIOUS DECK
 CARD 87 --> \$PARA
 CARD 88 --> VARY='CW' NTH=2 FROM=6 TO=8 BY=0.5 DECK='PROP'
 CARD 89 --> SEND

TYPE: 12MM GUN TEST CASE					
GROOVE DIAMETER (IN):	4.726	LAND DIAMETER (IN):	607.00	TRAVEL (IN):	187.11
TWIST (CAL/S TURN):	99.0	BORE AREA (IN ²):	17.5271	GROOVE/LAND RATIO (-):	1.000
SHELL THICKNESS (IN):	0.004500	SHELL CP (IN-LB/LB-K):	1843.0	HEAT-LOSS OPTION:	1
INITIAL SHELL TEMP (K):	293.	AIR HO (IN-LB/IN ² -S-K):	0.06480	SHELL DENSITY (LB/IN ³):	0.2640

- PROJECTILE -

TYPE: APFSDS	TOTAL WEIGHT (LB):	15.650	WEIGHT PREDICTOR OPTION:	0
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- RESISTANCE -

AIR RESISTANCE OPTION:		WALL HEATING FRACTION:		FRICTION TABLE LENGTH:	
I	TRAVEL (IN)	PRESSURE (PSI)	I	TRAVEL (IN)	PRESSURE (PSI)
1	0.00	100.	3	3.00	100.
2	0.80	2500.			
			4	187.00	100.

- GENERAL -

MAX TIME STEP (\$):	0.000050	PRINT STEP (\$):	0.000050	MAX RELATIVE ERROR (-):	0.050000
PRINT OPTIONS:	1 1 1 0 2 1	STORE OPTION:	0	CONSTANT-PRESSURE OPTION:	0
GRADIENT MODEL: PISOQUICK-KENT					

- RECOLL -

RECOIL OPTION:	0	TYPE: NONE	RECOILING WEIGHT (LB):	0.
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- PRIMER -

TYPE: BENITE	GAMMA (-):	1.2500	FORCE (FT-LB/LB):	212500.
COVOLUME (IN3/LB):	FLAME TEMP (K):	30.000	WEIGHT (LB):	0.003470

- CHARGE 1 -

TYPE: JAZ 7P	GRAINS:	2724.4	7PF	WEIGHT (LB):	10.0000
EROSIVE COEFF (-):	CHARGE IGM CODE:		0	CHARGE IGM AT (S):	0.00000E+00
GRAIN LENGTH (IN):	GRAIN DIAMETER (IN):		0.34000	PERF DIAMETER (IN):	0.02000
INNER WEB (IN):	OUTER WEB (IN):		0.07400		

PROPERTIES AT LAYER BOUNDARIES OF PERF SURFACES		PROPERTIES AT LAYER BOUNDARIES OF END SURFACES	
1ST	2ND	3RD	4TH
AT DEPTH (IN):	---	---	---
ADJACENT LAYER WT %:	---	---	---
DENSITY (LB/IN3):	---	---	---
GAMMA (-):	---	---	---
FORCE (FT-LB/LB):	---	---	---
COVOLUME (IN3/LB):	---	---	---
FLAME TEMP (K):	---	---	---
MEAN PRESSURES (PSI):	---	---	---
MEAN PRESSURES (PSI):	---	---	---
MEAN PRESSURES (PSI):	---	---	---
BURNING RATES (IN/S):	---	---	---
BURNING RATES (IN/S):	---	---	---
BURNING RATES (IN/S):	---	---	---

PROPERTIES AT LAYER BOUNDARIES OF LAT SURFACES

1ST	2ND	3RD	4TH
AT DEPTH (IN):	---	---	---
ADJACENT LAYER WT %:	---	---	---
DENSITY (LB/IN3):	---	---	---
GAMMA (-):	---	---	---
FORCE (FT-LB/LB):	---	---	---
COVOLUME (IN3/LB):	---	---	---
FLAME TEMP (K):	---	---	---
MEAN PRESSURES (PSI):	---	---	---
MEAN PRESSURES (PSI):	---	---	---
MEAN PRESSURES (PSI):	---	---	---
BURNING RATES (IN/S):	---	---	---
BURNING RATES (IN/S):	---	---	---
BURNING RATES (IN/S):	---	---	---

- CHARGE 2 -

TYPE: JAZ 7P	0.000000	4241.2	7PF	WEIGHT (LB):	6.0000
EROSIVE COEFF (-):	0		0	CHARGE IGM AT (S):	0.00000E+00
P-SURF IGM CODE:	0.00000E+00		1	L-SURF IGM CODE:	3
P-SURF IGM AT (S):	0.00000E+00	0.20000E-03		L-SURF IGM AT (PSI):	0.2000E+04
GRAIN LENGTH (IN):	0.64300		0.22731	PERF DIAMETER (IN):	0.02000
INNER WEB (IN):	0.04183		0.04183		

PROPERTIES AT LAYER BOUNDARIES OF PERF SURFACES		PROPERTIES AT LAYER BOUNDARIES OF END SURFACES	
1ST	2ND	1ST	4TH
AT DEPTH (IN):	---	---	---
ADJACENT LAYER WT %:	---	---	---
DENSITY (LB/IN3):	---	---	---
GAMMA (-):	---	---	---
FORCE (FT-LB/LB):	---	---	---
CONVOLUME (IN3/LB):	---	---	---
FLAME TEMP (K):	---	---	---
MEAN PRESSURES (PSI):	---	---	---
MEAN PRESSURES (PSI):	---	---	---
MEAN PRESSURES (PSI):	---	---	---
BURNING RATES (IN/S):	---	---	---
BURNING RATES (IN/S):	---	---	---
BURNING RATES (IN/S):	---	---	---

PROPERTIES AT LAYER BOUNDARIES OF LAT SURFACES	
1ST	4TH
AT DEPTH (IN):	---
ADJACENT LAYER WT %:	---
DENSITY (LB/IN3):	---
GAMMA (-):	---
FORCE (FT-LB/LB):	---
CONVOLUME (IN3/LB):	---
FLAME TEMP (K):	---
MEAN PRESSURES (PSI):	---
MEAN PRESSURES (PSI):	---
MEAN PRESSURES (PSI):	---
BURNING RATES (IN/S):	---
BURNING RATES (IN/S):	---
BURNING RATES (IN/S):	---

TIME (MS)	TRAV (IN)	VEL (FT/S)	ACC (G)	BREECH PRESS (PSI)	MEAN PRESS (PSI)	BASE PRESS (PSI)	MEAN TEMP (K)	FRAC BURN 1	FRAC BURN 2
0.000	0.00	0.	0.	27.	27.	27.	2000.	0.000	0.000
0.050	0.00	0.	0.	50.	50.	50.	2496.	0.000	0.000
0.100	0.00	0.	0.	81.	81.	81.	2786.	0.000	0.000
0.126	0.00	0.	0.	100.	100.	100.	2837.	0.000	0.000
SHOT-START PRESSURE ACHIEVED									
0.149	0.00	0.	-11.	134.	119.	90.	2960.	0.000	0.000
0.201	0.00	0.	30.	189.	167.	127.	3078.	0.001	0.000
PROPELLANT 2 IGNITED ON END SURFACE									
0.250	0.00	0.	79.	254.	224.	171.	3155.	0.001	0.001
0.300	0.00	0.	137.	331.	293.	223.	3210.	0.001	0.001
0.350	0.00	1.	203.	419.	371.	282.	3248.	0.002	0.001
0.400	0.00	1.	276.	518.	459.	349.	3277.	0.002	0.002
0.450	0.00	1.	358.	629.	557.	424.	3298.	0.003	0.002
0.500	0.00	2.	447.	752.	665.	507.	3314.	0.003	0.002
0.550	0.00	3.	543.	886.	784.	597.	3327.	0.004	0.003
0.600	0.01	4.	647.	1033.	914.	696.	3337.	0.004	0.003
0.650	0.01	5.	758.	1192.	1054.	803.	3345.	0.005	0.004
0.700	0.01	6.	875.	1363.	1205.	918.	3352.	0.006	0.004
0.750	0.02	8.	1000.	1546.	1368.	1042.	3357.	0.007	0.005
0.800	0.02	10.	1130.	1743.	1542.	1174.	3362.	0.007	0.006
0.850	0.03	11.	1267.	1952.	1727.	1315.	3365.	0.008	0.006
0.900	0.04	14.	1409.	2174.	1923.	1464.	3369.	0.009	0.007
0.919	0.04	14.	1463.	2259.	1999.	1522.	3370.	0.010	0.007
PROPELLANT 2 IGNITED ON LAT SURFACE									
0.950	0.04	16.	1603.	2470.	2185.	1664.	3372.	0.010	0.009
1.000	0.05	19.	1836.	2826.	2499.	1903.	3375.	0.011	0.010
1.050	0.07	22.	2083.	3207.	2837.	2160.	3377.	0.013	0.013
1.100	0.08	25.	2343.	3614.	3197.	2435.	3379.	0.014	0.015
1.150	0.10	29.	2614.	4048.	3581.	2727.	3381.	0.015	0.017
1.200	0.12	34.	2897.	4508.	3988.	3037.	3382.	0.016	0.020
1.250	0.14	39.	3195.	4999.	4422.	3368.	3383.	0.018	0.022
1.300	0.16	44.	3509.	5527.	4889.	3723.	3383.	0.020	0.025
1.350	0.19	50.	3842.	6094.	5390.	4105.	3383.	0.021	0.028
1.400	0.22	57.	4192.	6700.	5927.	4514.	3383.	0.023	0.032
1.450	0.26	64.	4559.	7349.	6500.	4950.	3383.	0.025	0.035
1.500	0.30	71.	4944.	8039.	7111.	5415.	3383.	0.027	0.039
1.550	0.34	80.	5346.	8773.	7761.	5910.	3382.	0.030	0.043
1.600	0.40	88.	5765.	9553.	8451.	6435.	3381.	0.032	0.047
1.650	0.45	98.	6200.	10379.	9181.	6992.	3380.	0.035	0.052
1.700	0.51	108.	6650.	11252.	9953.	7580.	3379.	0.037	0.057
1.750	0.58	120.	7120.	12179.	10773.	8204.	3377.	0.040	0.062
1.800	0.66	131.	7613.	13168.	11649.	8871.	3376.	0.044	0.068
1.850	0.74	144.	8132.	14224.	12583.	9582.	3374.	0.047	0.074
1.900	0.83	158.	8813.	15348.	13577.	10340.	3372.	0.051	0.081
1.950	0.93	173.	9836.	16544.	14635.	11145.	3369.	0.054	0.088
2.000	1.04	189.	10926.	17813.	15758.	12000.	3366.	0.059	0.095
2.050	1.16	208.	12085.	19158.	16947.	12906.	3364.	0.063	0.103
2.100	1.29	228.	13317.	20580.	18205.	13864.	3360.	0.068	0.112
2.150	1.43	251.	14622.	22078.	19531.	14873.	3357.	0.073	0.121
2.200	1.59	275.	16004.	23655.	20925.	15936.	3353.	0.078	0.131
2.250	1.76	302.	17463.	25309.	22388.	17050.	3348.	0.084	0.142
2.300	1.95	332.	18999.	27039.	23919.	18215.	3343.	0.090	0.153
2.350	2.16	364.	20613.	28842.	25514.	19430.	3338.	0.097	0.165
2.400	2.39	398.	22305.	30715.	27171.	20692.	3332.	0.104	0.178
2.450	2.64	435.	24072.	32654.	28886.	21998.	3326.	0.111	0.191

TIME (MS)	TRAV (IN)	VEL (FT/S)	ACC (G)	BREECH PRESS (PSI)	MEAN PRESS (PSI)	BASE PRESS (PSI)	MEAN TEMP (K)	FRAC BURN 1	FRAC BURN 2
2.500	2.91	476.	25912.	34653.	30654.	23345.	3319.	0.119	0.206
2.550	3.21	519.	27567.	36705.	32469.	24727.	3311.	0.127	0.222
2.600	3.53	564.	29147.	38802.	34324.	26139.	3303.	0.136	0.237
2.650	3.89	613.	30756.	40936.	36212.	27577.	3295.	0.145	0.254
2.700	4.27	663.	32384.	43097.	38124.	29033.	3286.	0.155	0.273
2.750	4.68	717.	34025.	45275.	40051.	30500.	3276.	0.165	0.292
2.800	5.13	773.	35671.	47459.	41982.	31971.	3266.	0.176	0.312
2.850	5.61	832.	37311.	49636.	43908.	33438.	3256.	0.187	0.333
2.900	6.13	893.	38936.	51795.	45818.	34892.	3245.	0.199	0.355
2.950	6.69	957.	40538.	53921.	47699.	36325.	3233.	0.211	0.378
3.000	7.28	1024.	42106.	56003.	49541.	37727.	3222.	0.224	0.403
3.050	7.91	1093.	43630.	58028.	51332.	39091.	3209.	0.237	0.428
3.100	8.59	1164.	45101.	59984.	53062.	40409.	3197.	0.251	0.454
3.150	9.31	1238.	46511.	61858.	54719.	41671.	3184.	0.265	0.482
3.200	10.08	1314.	47850.	63639.	56296.	42871.	3171.	0.280	0.510
3.250	10.89	1392.	49113.	65319.	57781.	44003.	3157.	0.295	0.540
3.300	11.75	1472.	50291.	66888.	59169.	45059.	3144.	0.311	0.570
3.350	12.66	1554.	51380.	68338.	60452.	46037.	3130.	0.327	0.602
3.400	13.61	1637.	52374.	69664.	61625.	46930.	3116.	0.343	0.634
3.450	14.62	1722.	53271.	70862.	62685.	47737.	3102.	0.360	0.667
3.500	15.68	1809.	54069.	71928.	63627.	48455.	3088.	0.377	0.701
3.550	16.79	1896.	54765.	72860.	64453.	49083.	3074.	0.395	0.735
3.600	17.96	1985.	55361.	73660.	65160.	49622.	3059.	0.413	0.771
3.650	19.17	2075.	55856.	74327.	65750.	50071.	3045.	0.431	0.807
3.700	20.45	2165.	56253.	74864.	66225.	50433.	3031.	0.449	0.844
3.729	21.21	2218.	56351.	75000.	66345.	50525.	3023.	0.460	0.863
LOCAL PRESSURE MAX DETECTED									
3.729	21.21	2218.	56351.	75000.	66345.	50525.	3023.	0.460	0.863
LOCAL PRESSURE MIN DETECTED									
3.729	21.21	2218.	56351.	75000.	66345.	50525.	3023.	0.460	0.863
LOCAL PRESSURE MAX DETECTED									
3.750	21.77	2256.	56305.	74944.	66296.	50487.	3016.	0.468	0.875
3.800	23.15	2346.	55943.	74476.	65882.	50172.	3000.	0.487	0.900
3.850	24.59	2436.	55323.	73668.	65167.	49627.	2982.	0.505	0.920
3.900	26.07	2524.	54512.	72605.	64227.	48911.	2964.	0.524	0.936
3.950	27.62	2611.	53552.	71345.	63112.	48062.	2946.	0.542	0.949
4.000	29.21	2696.	52476.	69932.	61862.	47110.	2927.	0.561	0.960
4.050	30.85	2780.	51317.	68409.	60515.	46084.	2909.	0.579	0.969
4.100	32.54	2862.	50116.	66830.	59118.	45021.	2890.	0.596	0.976
4.150	34.28	2941.	48889.	65218.	57692.	43935.	2872.	0.614	0.982
4.200	36.07	3019.	47649.	63586.	56249.	42836.	2854.	0.631	0.987
4.250	37.91	3095.	46404.	61950.	54801.	41733.	2836.	0.648	0.991
4.300	39.79	3168.	45163.	60318.	53358.	40634.	2819.	0.664	0.994
4.350	41.71	3240.	43933.	58701.	51927.	39545.	2801.	0.680	0.997
4.400	43.67	3310.	42719.	57105.	50516.	38470.	2784.	0.696	0.998
4.450	45.68	3378.	41526.	55537.	49128.	37413.	2768.	0.712	0.999
4.500	47.73	3444.	40357.	54000.	47769.	36378.	2751.	0.727	1.000
4.511	48.19	3458.	40096.	53658.	47466.	36147.	2748.	0.731	1.000
PROPELLANT 2 BURNED OUT									
4.549	49.76	3506.	39245.	52539.	46476.	35393.	2736.	0.742	1.000
4.599	51.88	3569.	38145.	51094.	45198.	34420.	2720.	0.756	1.000
4.649	54.04	3629.	37085.	49700.	43965.	33481.	2705.	0.771	1.000
4.699	56.24	3688.	36062.	48357.	42777.	32576.	2690.	0.785	1.000
4.749	58.47	3745.	35077.	47064.	41633.	31705.	2675.	0.798	1.000
4.799	60.73	3801.	34128.	45818.	40531.	30866.	2661.	0.812	1.000

CONDITIONS AT:	PHAX	MUZZLE
TIME (MS):	3.729	7.060
TRAVEL (IN):	21.21	187.11
VELOCITY (FT/S):	2218.	5236.
ACCELERATION (G):	56351.	10696.
BREECH PRESS (PSI):	75000.	15129.
MEAN PRESS (PSI):	66345.	13383.
BASE PRESS (PSI):	50525.	10192.
MEAN TEMP (K):	3023.	2147.
Z CHARGE 1 (-):	0.460	0.993
Z CHARGE 2 (-):	0.863	1.000

ENERGY BALANCE SUMMARY	IN-LB	%
TOTAL CHEMICAL:	323663104.	100.00
(1) INTERNAL GAS:	204413888.	63.16
(2) WORK AND LOSSES:	119249216.	36.84
(A) PROJECTILE KINETIC:	79963376.	24.71
(B) GAS KINETIC:	25038928.	7.74
(C) PROJECTILE ROTATIONAL:	40262.	0.01
(D) FRICTIONAL WORK TO TUBE:	0.	0.00
(E) OTHER FRICTIONAL WORK:	391050.	0.12
(F) WORK DONE AGAINST AIR:	1140127.	0.35
(G) HEAT CONVECTED TO BORE:	12675466.	3.92
(H) RECOIL ENERGY:	0.	0.00

LOADING DENSITY (G/CM3):	0.730
CHARGE WT/PROJECTILE WT:	1.023
PIEZOMETRIC EFFICIENCY:	0.325
EXPANSION RATIO:	6.403

PARAMETRIC VARIABLES: / 1/ OUT 1 PMAX
 / 2/ PROP 2 CHWT
 / 3/ PROP 2 DIAM
 / 4/ PROP 2 PO
 / 5/ PROP 2 WEB
 / 6/ OUT 1 VMUZ
 / 7/ OUT 1 ZMUZ(2)
 / 8/ OUT 1 LDEN

/ 1/	/ 2/	/ 3/	/ 4/	/ 5/	/ 6/	/ 7/	/ 8/
75000.	6.0000	0.22731	0.20000E-01	0.41828E-01	5236.5	1.0000	0.72978
75000.	6.5000	0.24653	0.20000E-01	0.46632E-01	5320.0	1.0000	0.75258
75000.	7.0000	0.26551	0.20000E-01	0.51377E-01	5396.4	1.0000	0.77538
75000.	7.5000	0.28584	0.20000E-01	0.56461E-01	545	1.0000	0.79818
75000.	8.0000	0.30781	0.20000E-01	0.61953E-01	550	1.0000	0.82099

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VII. ACKNOWLEDGEMENTS

As stated in the introduction, the intention of this report is to instruct and clarify how to use the IBHVG2 computer code. Although we have worked to improve the computer code in regards to portability and efficiency, Franz Lynn deserves the credit for the creation of IBHVG2. The widespread use of the computer algorithm is a testament to his skill and abilities. His death represents a loss to the interior ballistics community. To be sure, he was sorely missed during the documentation phase of IBHVG2.

We gave considerable thought about including Franz's name on this report. Much of the writing about the input cards and the algorithm comes from his original notes. We decided against it to avoid confusing the readers. Any errors or omissions are solely our own. We are certain that a report with Franz's participation would have been better since he was obviously more knowledgeable about what the code could and could not do.

To thank all the people who helped in writing this documentation or in developing the code would be rather pointless, since it would entail most of the professional staff of Interior Ballistic Division at BRL. However, a few names stand out in particular. A special thanks goes to Fred Robbins for serving as our sublime authority about how to use the code, and to Bob Deas and Paul Baer for motivation about the what and why parts. Stumping these three with a question usually meant some extensive computer experimentation was required. Fortunately, this was an infrequent occurrence.

As a final comment, it is worth mentioning that much of the progress in computer simulations can be directly attributed to experimental developments. From a mathematical standpoint, the equations solved by IBHVG2 are neither original nor particularly complicated. What is new is the data being used to drive these simulations. In-bore measurements, accurate burning rate correlations, and instrumented projectiles have reduced the number of unknowns so that modelers can focus their energies on design and optimization. In this vein, we would like to thank the respective staffs under the direction of Arpad Juhasz for closed bomb firings and Jim Evans for range operations at Sandy Point (Range 18).

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